STFATE
Predominant Currents

MODEL: SHORT-TERM FATE OF DREDGED MATERIAL FROM SPLIT HULL BARGE OR HOPPER DREDGE
(PC Version 5.01 MAY, 1993)

TITLE: Douglas Harbor to Gastineau Channel Current 0.59

FILE: DHGAST07.DUE

AREA: THE PROJECT AREA IS DESCRIBED BY A 32 X 45 GRID.

THERE ARE 32 GRID POINTS (NMAX) IN THE Z-DIRECTION (FROM LEFT TO RIGHT)
AND 45 GRID POINTS (MMAX) IN THE X-DIRECTION (FROM TOP TO BOTTOM).

ZONE: THE MIXING ZONE IS REPRESENTED AS A RECTANGLE ON THE SITE GRID.

THE TOPMOST BOUNDARY IS LOCATED AT POINT # 3 (MDS1) FROM THE TOP OF THE GRID.

THE BOTTOMMOST BOUNDARY IS LOCATED AT POINT #12 (MDS2) FROM THE TOP OF THE GRID.

THE LEFTMOST BOUNDARY IS LOCATED AT POINT #11 (NDS1) FROM THE LEFT OF THE GRID.

THE RIGHTMOST BOUNDARY IS LOCATED AT POINT #22 (NDS2) FROM THE LEFT OF THE GRID.

EXECUTION PARAMETERS:

MODEL COEFFICIENTS SPECIFIED IN INPUT DATA (KEY1 = 1).

PERFORM COMPLETE ANALYSIS INCLUDING DESCENT, COLLAPSE, AND TRANSPORT-DIFFUSION (KEY2 = 0).

PERFORM TIER III INLAND DUMPING INITIAL MIXING EVALUATION
TO COMPARE WITH TOXICITY STANDARD (KEY3 = 6).

MIXING ZONE HAS BEEN DESIGNATED -- NO MIXING ZONE WILL BE COMPUTED.

NO ANALYSIS OF A ZONE OF INITIAL DILUTION REQUESTED.

PRINTING OF CONVECTIVE DESCENT RESULTS NOT REQUESTED (IPCN = 0).

PRINTING OF CONVECTIVE DESCENT RESULTS NOT REQUESTED (IPCN = 0).

PRINTING OF DYNAMIC COLLAPSE RESULTS NOT REQUESTED (IPCL = 0).

QUARTERLY PRINTING OF LONG-TERM TRANSPORT DIFFUSION RESULTS REQUESTED (IPLT = 0).

LONG-TERM TRANSPORT DIFFUSION RESULTS REQUESTED AT THE FOLLOWING 2 DEPTH(S):
60.00 FT
119.00 FT

GRID: NUMBER OF LONG TERM GRID POINTS IN Z-DIRECTION (NMAX) = 32

NUMBER OF LONG TERM GRID POINTS IN X-DIRECTION (MMAX) = 45

GRID SPACING IN Z-DIRECTION (DZ) = 25.00000 FT

GRID SPACING IN X-DIRECTION (DX) = 50.00000 FT

CONSTANT DEPTH GRID SPECIFIED HAVING A DEPTH (DEPC) OF 120.00000 FT.

DEPTH GRID, FEET:

M N = 1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17
1	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.
2	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.
3	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.
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6	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.
7	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.
8	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.
9	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.
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16	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.
17	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.
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36	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.
37	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.
38	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.
39	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.
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M N =	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32
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40	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.
41	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.
42	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.
43	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.
44	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.
45	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.

CODED GRID:

RANGE OF N IS   1 TO 32

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LEGEND FOR CODED GRID: W = WATER POINT

L = LAND POINT
O = OPEN BOUNDARY
B = MIXING ZONE BOUNDARY
Z = ZID BOUNDARY
D = DUMP LOCATION
X = DUMMY POINT

NUMBER OF GRID POINTS WITHIN ESTUARY = 1148

DISPOSAL LOCATION:

THE DUMP LOCATION IS 300.0 FT (XBARGE) OR ABOUT GRID POINT # 7 FROM THE TOP OF THE GRID
AND 450.0 FT (ZBARGE) OR ABOUT GRID POINT #19 FROM THE LEFT EDGE OF THE GRID.

THE BOTTOM SLOPE IN THE X-DIRECTION AT THE DUMP SITE (SLOPEX, POSITIVE IF DEPTH INCREASES
FROM TOP OF GRID TO BOTTOM OF GRID) IS 0.00 DEGREES.

THE BOTTOM SLOPE IN THE Z-DIRECTION AT THE DUMP SITE (SLOPEZ, POSITIVE IF DEPTH INCREASES
FROM LEFT SIDE OF GRID TO RIGHT SIDE OF GRID) IS 0.00 DEGREES.

THE DISPOSAL LOCATION IS NOT AT A HOLE OR DEPRESSION. (DHOLE = 0.0)

AMBIENT DENSITY PROFILE:

DEPTH (FT)	DENSITY (G/CC)
0.0000E+00	1.0200
120.0	1.0200

COMPUTED DEPTH:

THE DEPTH AT THE DUMP LOCATION WAS INTERPOLATED TO BE 120.0 FT.

VELOCITY DISTRIBUTION:

VERTICALLY AVERAGED X-DIRECTION (VAX = 0.590 FPS) AND
Z-DIRECTION (VAZ = 0.000E+00 FPS) VELOCITIES CONSTRUCTED AT EACH GRID POINT
FROM A SINGLE OBSERVATION AT A DEPTH (D) OF 95.0 FT.

VELOCITY GRID: X-DIRECTION, FPS

M N=	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17
1	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467
2	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467
3	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467
4	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467
5	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467
6	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467
7	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467
8	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467
9	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467
10	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467
11	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467
12	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467
13	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467
14	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467
15	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467
16	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467
17	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467
18	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467
19	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467
20	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467
21	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467
22	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467
23	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467
24	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467
25	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467
26	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467
27	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467
28	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467
29	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467
30	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467
31	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467
32	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467
33	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467
34	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467
35	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467
36	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467
37	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467
38	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467
39	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467
40	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467
41	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467
42	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467

43	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467
44	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467
45	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467

M	N= 18	19	20	21	22	23	24	25	26	27	28	29	30	31	32
1	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467
2	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467
3	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467
4	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467
5	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467
6	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467
7	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467
8	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467
9	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467
10	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467
11	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467
12	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467
13	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467
14	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467
15	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467
16	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467
17	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467
18	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467
19	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467
20	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467
21	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467
22	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467
23	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467
24	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467
25	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467
26	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467
27	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467
28	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467
29	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467
30	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467
31	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467
32	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467
33	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467
34	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467
35	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467
36	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467
37	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467
38	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467
39	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467
40	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467
41	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467
42	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467
43	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467
44	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467
45	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467	0.467

VELOCITY GRID: Z-DIRECTION, FPS

M N=	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17
1	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
2	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
3	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
4	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
5	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
6	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
7	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
8	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
9	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
10	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
11	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
12	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
13	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
14	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
15	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
16	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
17	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
18	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
19	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
20	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
21	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
22	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
23	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
24	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
25	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
26	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
27	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
28	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
29	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
30	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
31	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
32	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
33	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
34	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
35	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
36	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
37	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
38	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
39	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
40	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
41	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
42	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
43	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
44	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
45	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000

M	N= 18	19	20	21	22	23	24	25	26	27	28	29	30	31	32
1	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
2	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
3	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
4	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
5	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
6	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
7	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
8	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
9	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
10	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
11	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
12	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
13	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
14	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
15	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
16	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
17	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
18	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
19	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
20	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
21	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
22	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
23	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
24	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
25	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
26	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
27	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
28	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
29	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
30	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
31	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
32	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
33	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
34	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
35	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
36	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
37	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
38	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
39	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
40	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
41	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
42	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
43	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
44	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
45	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000

BOTTOM SHEAR STRESS, LBS/SQ FT:

M N=	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17
1	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
2	0.0000	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007
3	0.0000	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007
4	0.0000	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007
5	0.0000	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007
6	0.0000	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007
7	0.0000	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007
8	0.0000	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007
9	0.0000	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007
10	0.0000	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007
11	0.0000	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007
12	0.0000	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007
13	0.0000	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007
14	0.0000	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007
15	0.0000	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007
16	0.0000	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007
17	0.0000	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007
18	0.0000	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007
19	0.0000	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007
20	0.0000	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007
21	0.0000	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007
22	0.0000	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007
23	0.0000	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007
24	0.0000	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007
25	0.0000	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007
26	0.0000	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007
27	0.0000	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007
28	0.0000	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007
29	0.0000	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007
30	0.0000	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007
31	0.0000	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007
32	0.0000	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007
33	0.0000	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007
34	0.0000	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007
35	0.0000	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007
36	0.0000	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007
37	0.0000	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007
38	0.0000	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007
39	0.0000	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007
40	0.0000	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007
41	0.0000	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007
42	0.0000	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007
43	0.0000	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007
44	0.0000	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007
45	0.0000	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007

M	N= 18	19	20	21	22	23	24	25	26	27	28	29	30	31	32
1	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
2	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007
3	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007
4	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007
5	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007
6	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007
7	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007
8	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007
9	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007
10	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007
11	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007
12	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007
13	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007
14	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007
15	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007
16	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007
17	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007
18	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007
19	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007
20	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007
21	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007
22	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007
23	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007
24	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007
25	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007
26	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007
27	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007
28	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007
29	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007
30	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007
31	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007
32	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007
33	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007
34	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007
35	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007
36	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007
37	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007
38	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007
39	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007
40	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007
41	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007
42	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007
43	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007
44	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007
45	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007

TIME PARAMETERS:

DURATION OF THE DISPOSAL, TREL = 30.00 SECONDS

DURATION OF THE SIMULATION, TSTOP = 3600.00 SECONDS

LONG-TERM TIME STEP USED IN THE SIMULATION, DTL = 300.00 SECONDS

BARGE DESCRIPTION:

LENGTH OF BARGE, BARGL = 60. FT

WIDTH OF BARGE, BARGW = 30. FT

DRAFT OF LOADED BARGE, DREL1 = 6.00 FT

DRAFT OF UNLOADED BARGE, DREL2 = 3.50 FT

MODEL COEFFICIENTS READ FROM INPUT:

TURBULENT THERMAL ENTRAINMENT	ALPHA0	=	0.2350
SETTLING COEFFICIENT	BETA	=	0.0000
APPARENT MASS COEFFICIENT	CM	=	1.0000
DRAG COEFFICIENT FOR A SPHERE	CD	=	0.5000
RATIO--CLOUD/AMBIENT DENSITY GRADIENTS	GAMA	=	0.2500
FORM DRAG FOR COLLAPSING CLOUD	CDRAG	=	1.0000
SKIN FRICTION FOR COLLAPSING CLOUD	CFRIC	=	0.0100
DRAG FOR AN ELLIPSOIDAL WEDGE	CD3	=	0.1000
DRAG FOR A PLATE	CD4	=	1.0000
ENTRAINMENT IN COLLAPSE	ALPHAC	=	0.1000
FRICTION BETWEEN CLOUD AND BOTTOM	FRICTN	=	0.0100
4/3 LAW HORIZ. DIFF. DISSIPATION FACTOR	ALAMDA	=	0.0010
UNSTRATIFIED WATER VERT. DIFF. COEF.	AKY0	=	0.0250
STRIPPING COEF. OF FINES DURING CONVERTIVE DESCENT		=	0.0030

MATERIAL DESCRIPTION: 4 SOLIDS FRACTIONS

L A Y E R 1

DESCRIPTION	SPEC. GRAV. OR DENSITY (GM/CC)	VOLUMETRIC CONCENTRATION (VOL/VOL)	FALL VELOCITY (FPS)	DEPOSITIONAL VOID RATIO	CHARACTER
GRAVEL	2.700	0.1500E-02	1.00000	0.5000	NONCOHESIVE
	CRITICAL SHEAR STRESS FOR DEPOSITION = 99.00 LBS/SQ. FT.				
	SEDIMENT FRACTION WILL NOT BE STRIPPED DURING CONVECTIVE DESCENT.				
SAND	2.700	0.6950E-01	0.10000	0.6000	NONCOHESIVE
	CRITICAL SHEAR STRESS FOR DEPOSITION = 0.2500E-01 LBS/SQ. FT.				
	SEDIMENT FRACTION WILL BE STRIPPED DURING CONVECTIVE DESCENT.				
SILT	2.650	0.4153	0.01000	5.000	COHESIVE
	CRITICAL SHEAR STRESS FOR DEPOSITION = 0.8000E-02 LBS/SQ. FT.				
	SEDIMENT FRACTION WILL BE STRIPPED DURING CONVECTIVE DESCENT.				
CLAY	2.650	0.1384	0.00200	8.000	COHESIVE
	CRITICAL SHEAR STRESS FOR DEPOSITION = 0.1000E-02 LBS/SQ. FT.				
	SEDIMENT FRACTION WILL BE STRIPPED DURING CONVECTIVE DESCENT.				

TOXICITY ANALYSIS DATA:

CONCENTRATIONS OF FLUID IN TERMS OF PERCENT OF THE DREDGED MATERIAL
FOLLOWING INITIAL MIXING ARE COMPUTED FOR WATER QUALITY EVALUATIONS.

THE INITIAL CONCENTRATION OF FLUID IS 100. PERCENT
AND ITS BACKGROUND CONCENTRATION IS 0.000E+00 PERCENT.

THE DILUTION REQUIRED TO MEET TOXICITY STANDARD IS 0.422000 PERCENT.
(TYPICALLY, 1 PERCENT OF THE LC50)

DESCRIPTION	SPEC. GRAV. OR DENSITY (GM/CC)	VOLUMETRIC CONCENTRATION (VOL/VOL)
FLUID	1.020	0.3753

DISCHARGE PARAMETERS:

VOLUME OF LAYER 1 = 500.0 CU YD

INITIAL RADIUS OF CLOUD, RB = 18.61052 FT

INITIAL DEPTH OF CLOUD CENTROID, DREL = 11.73 FT

INITIAL CLOUD VELOCITIES...

X-DIRECTION (FROM TOP TO BOTTOM OF GRID), CU(1) = 1.500 FPS

Y-DIRECTION (FROM SURFACE TO BOTTOM), CV(1) = 0.8333E-01 FPS

Z-DIRECTION (FROM LEFT TO RIGHT OF GRID), CW(1) = 0.0000E+00 FPS

BULK PARAMETERS:

BULK DENSITY, ROO = 2.041811 G/CC

AGGREGATE OR BULK VOIDS RATIO, BVOID = 5.164

CONVECTIVE DESCENT PHASE:

IN TRIAL #1 THE DESCENT PHASE TIME STEP (DT) WAS 0.24027357E-01 SECONDS.

THE TOTAL NUMBER OF INTEGRATION TIME STEPS (ISTEP) WAS 278.

THE BOTTOM WAS ENCOUNTERED DURING CONVECTIVE DESCENT.

THE DISCHARGE DID NOT OBTAIN A NEUTRALLY BUOYANT CONDITION DURING CONVECTIVE DESCENT.

CLOUD COLLAPSE PHASE:

IN TRIAL #1 THE COLLAPSE PHASE TIME STEP (DT) WAS 0.24027357E-01 SECONDS.
THE TOTAL NUMBER OF INTEGRATION TIME STEPS (ISTEP) FOR CONVECTIVE DESCENT AND COLAPSE WAS 1040.
THE INTEGRATION TIME STEP NUMBER WHEN THE BED WAS ENCOUNTERED (IBED) WAS 278.
THE BOTTOM WAS ENCOUNTERED DURING CONVECTIVE DESCENT.
DIFFUSION OF THE DISCHARGE IS GREATER THAN DYNAMIC SPREADING FROM THE COLLAPSE.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID X-LOCATION (FT)	CLOUD CENTROID Z-LOCATION (FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	T O T A L M A S S (CU FT)	ENTRAINED MASS (CU FT)	TIME STEP WHEN THIS CLOUD WAS CREATED	TIME STEP WHEN PREVIOUS CLOUD WAS CREATED
NEW CLOUD CREATED, NTCLD(K) (K = 1) = 1									
37.50	351.5	450.0	93.60	120.0	0.1000E-02	0.7605	0.0000E+00	313	278
NEW CLOUD CREATED, NTCLD(K) (K = 1) = 2									
40.00	352.9	450.0	162.9	120.0	0.1000E-02	4.091	0.0000E+00	417	313
NEW CLOUD CREATED, NTCLD(K) (K = 1) = 3									
42.49	354.1	450.0	217.1	120.0	0.1000E-02	5.131	0.0000E+00	521	417
NEW CLOUD CREATED, NTCLD(K) (K = 1) = 4									
44.99	355.2	450.0	251.2	120.0	0.1000E-02	4.164	0.0000E+00	625	521
NEW CLOUD CREATED, NTCLD(K) (K = 1) = 5									
47.49	356.3	450.0	274.2	120.0	0.1000E-02	2.728	0.0000E+00	729	625
NEW CLOUD CREATED, NTCLD(K) (K = 1) = 6									
49.99	357.3	450.0	292.0	120.0	0.1000E-02	1.602	0.0000E+00	833	729
NEW CLOUD CREATED, NTCLD(K) (K = 1) = 7									
52.49	358.2	450.0	307.0	120.0	0.1000E-02	0.8796	0.0000E+00	937	833
NEW CLOUD CREATED, NTCLD(K) (K = 1) = 8									
54.97	359.1	450.0	320.1	114.9	5.107	0.8944	0.0000E+00	1040	937

NOTE -- When all solid material has settled from a cloud, the cloud is erased and
the remaining clouds for this solids type are renumbered.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID X-LOCATION (FT)	CLOUD CENTROID Z-LOCATION (FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	T O T A L M A S S (CU FT)	ENTRAINED MASS (CU FT)	TIME STEP WHEN THIS CLOUD WAS CREATED	TIME STEP WHEN PREVIOUS CLOUD WAS CREATED
NEW CLOUD CREATED, NTCLD(K) (K = 2) = 1									
32.50	348.1	450.0	46.28	4.750	32.04	12.22	0.0000E+00	105	1
NEW CLOUD CREATED, NTCLD(K) (K = 2) = 2									
35.00	350.0	450.0	62.66	36.79	39.49	10.75	0.0000E+00	209	105
NEW CLOUD CREATED, NTCLD(K) (K = 2) = 3									
37.50	351.5	450.0	93.60	76.28	14.46	14.91	0.0000E+00	313	278
NEW CLOUD CREATED, NTCLD(K) (K = 2) = 4									
40.00	352.9	450.0	162.9	90.74	14.56	18.91	0.0000E+00	417	313
NEW CLOUD CREATED, NTCLD(K) (K = 2) = 5									
42.49	354.1	450.0	217.1	105.3	3.483	8.223	0.0000E+00	521	417
NEW CLOUD CREATED, NTCLD(K) (K = 2) = 6									
44.99	355.2	450.0	251.2	108.8	1.251	3.840	0.0000E+00	625	521
NEW CLOUD CREATED, NTCLD(K) (K = 2) = 7									
47.49	356.3	450.0	274.2	110.0	0.6359	2.223	0.0000E+00	729	625
NEW CLOUD CREATED, NTCLD(K) (K = 2) = 8									
49.99	357.3	450.0	292.0	110.7	0.4108	1.558	0.0000E+00	833	729
NEW CLOUD CREATED, NTCLD(K) (K = 2) = 9									
52.49	358.2	450.0	307.0	111.1	0.3032	1.222	0.0000E+00	937	833
NEW CLOUD CREATED, NTCLD(K) (K = 2) = 10									
54.97	359.1	450.0	320.1	114.9	5.107	864.4	0.0000E+00	1040	937

NOTE -- When all solid material has settled from a cloud, the cloud is erased and
the remaining clouds for this solids type are renumbered.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID X-LOCATION (FT)	CLOUD CENTROID Z-LOCATION (FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	T O T A L M A S S (CU FT)	ENTRAINED MASS (CU FT)	TIME STEP WHEN THIS CLOUD WAS CREATED	TIME STEP WHEN PREVIOUS CLOUD WAS CREATED
NEW CLOUD CREATED, NTCLD(K) (K = 3) = 1									
32.50	348.1	450.0	46.28	4.750	32.04	73.00	0.0000E+00	105	1
NEW CLOUD CREATED, NTCLD(K) (K = 3) = 2									
35.00	350.0	450.0	62.66	36.79	39.49	64.24	0.0000E+00	209	105
NEW CLOUD CREATED, NTCLD(K) (K = 3) = 3									
37.50	351.5	450.0	93.60	76.28	14.46	89.11	0.0000E+00	313	278
NEW CLOUD CREATED, NTCLD(K) (K = 3) = 4									
40.00	352.9	450.0	162.9	90.74	14.56	113.0	0.0000E+00	417	313
NEW CLOUD CREATED, NTCLD(K) (K = 3) = 5									
42.49	354.1	450.0	217.1	105.3	3.483	49.13	0.0000E+00	521	417
NEW CLOUD CREATED, NTCLD(K) (K = 3) = 6									
44.99	355.2	450.0	251.2	108.8	1.251	22.95	0.0000E+00	625	521
NEW CLOUD CREATED, NTCLD(K) (K = 3) = 7									
47.49	356.3	450.0	274.2	110.0	0.6359	13.28	0.0000E+00	729	625
NEW CLOUD CREATED, NTCLD(K) (K = 3) = 8									
49.99	357.3	450.0	292.0	110.7	0.4108	9.309	0.0000E+00	833	729
NEW CLOUD CREATED, NTCLD(K) (K = 3) = 9									
52.49	358.2	450.0	307.0	111.1	0.3032	7.299	0.0000E+00	937	833
NEW CLOUD CREATED, NTCLD(K) (K = 3) = 10									
54.97	359.1	450.0	320.1	114.9	5.107	5165.	0.0000E+00	1040	937

NOTE -- When all solid material has settled from a cloud, the cloud is erased and
the remaining clouds for this solids type are renumbered.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID X-LOCATION (FT)	CLOUD CENTROID Z-LOCATION (FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	T O T A L M A S S (CU FT)	ENTRAINED MASS (CU FT)	TIME STEP WHEN THIS CLOUD WAS CREATED	TIME STEP WHEN PREVIOUS CLOUD WAS CREATED
NEW CLOUD CREATED, NTCLD(K) (K = 4) = 1									
32.50	348.1	450.0	46.28	4.750	32.04	24.33	0.0000E+00	105	1
NEW CLOUD CREATED, NTCLD(K) (K = 4) = 2									
35.00	350.0	450.0	62.66	36.79	39.49	21.41	0.0000E+00	209	105
NEW CLOUD CREATED, NTCLD(K) (K = 4) = 3									
37.50	351.5	450.0	93.60	76.28	14.46	29.70	0.0000E+00	313	278
NEW CLOUD CREATED, NTCLD(K) (K = 4) = 4									
40.00	352.9	450.0	162.9	90.74	14.56	37.66	0.0000E+00	417	313
NEW CLOUD CREATED, NTCLD(K) (K = 4) = 5									
42.49	354.1	450.0	217.1	105.3	3.483	16.37	0.0000E+00	521	417
NEW CLOUD CREATED, NTCLD(K) (K = 4) = 6									
44.99	355.2	450.0	251.2	108.8	1.251	7.647	0.0000E+00	625	521
NEW CLOUD CREATED, NTCLD(K) (K = 4) = 7									
47.49	356.3	450.0	274.2	110.0	0.6359	4.427	0.0000E+00	729	625
NEW CLOUD CREATED, NTCLD(K) (K = 4) = 8									
49.99	357.3	450.0	292.0	110.7	0.4108	3.103	0.0000E+00	833	729
NEW CLOUD CREATED, NTCLD(K) (K = 4) = 9									
52.49	358.2	450.0	307.0	111.1	0.3032	2.433	0.0000E+00	937	833
NEW CLOUD CREATED, NTCLD(K) (K = 4) = 10									
54.97	359.1	450.0	320.1	114.9	5.107	1721.	0.0000E+00	1040	937

NOTE -- When all solid material has settled from a cloud, the cloud is erased and
the remaining clouds for this solids type are renumbered.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID X-LOCATION (FT)	CLOUD CENTROID Z-LOCATION (FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	T O T A L M A S S (CU FT)	ENTRAINED MASS (CU FT)	TIME STEP WHEN THIS CLOUD WAS CREATED	TIME STEP WHEN PREVIOUS CLOUD WAS CREATED
NEW CLOUD CREATED, NTCLD(K) (K = 5) = 1									
54.97	359.1	450.0	320.1	114.9	5.107	5067.	0.0000E+00	1040	1

NOTE -- When all solid material has settled from a cloud, the cloud is erased and the remaining clouds for this solids type are renumbered.

LONG TERM DIFFUSION RESULTS:

BEGIN LONG TERM SIMULATION OF FATE OF GRAVEL

SUMMARY OF GRAVEL DISTRIBUTIONS AFTER 300.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.00000E+00
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 20.250

COMPUTATIONS FOR GRAVEL TERMINATED AT 300.00 SEC. ELAPSED TIME...MATERIAL SETTLED TO BOTTOM

BOTTOM ACCUMULATION OF GRAVEL (CU FT/GRID SQUARE) , 300.00 SECONDS AFTER DUMP

...MULTIPLY DISPLAYED VALUES BY 1.000 (LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)

M N=	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31
2	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O
3	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
4	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
5	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
6	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
7	O	0	0	0	0	0	0	0	0	0	0	0	0	.	+	+	.02	+	+	.	0	0	0	0	0	0	0	0	0	O
8	O	0	0	0	0	0	0	0	0	0	0	0	0	+	.12	3.5	11	3.5	.12	+	0	0	0	0	0	0	0	0	0	O
9	O	0	0	0	0	0	0	0	0	0	0	0	0	.	+	.23	.72	.23	+	.	0	0	0	0	0	0	0	0	0	O
10	O	0	0	0	0	0	0	0	0	0	0	0	0	.	+	.09	.30	.09	+	.	0	0	0	0	0	0	0	0	0	O
11	O	0	0	0	0	0	0	0	0	0	0	0	0	.	+	.07	.23	.07	+	.	0	0	0	0	0	0	0	0	0	O
12	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.	.	.	0	0	0	0	0	0	0	0	0	0	0	O
13	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
14	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
15	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
16	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
17	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
18	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
19	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
20	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
21	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
22	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
23	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
24	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
25	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
26	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
27	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
28	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
29	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
30	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
31	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
32	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
33	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
34	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
35	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
36	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
37	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
38	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
39	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
40	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
41	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
42	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
43	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
44	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O

THICKNESS (FT) OF GRAVEL ACCUMULATED ON BOTTOM, 300.00 SECONDS AFTER DUMP

...MULTIPLY DISPLAYED VALUES BY 0.1000E-01 (LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)

M N=	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31
2	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O
3	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
4	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
5	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
6	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
7	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.	+	+	+	.	0	0	0	0	0	0	0	0	0	O
8	O	0	0	0	0	0	0	0	0	0	0	0	0	0	.	.01	.42	1.2	.42	.01	.	0	0	0	0	0	0	0	0	O
9	O	0	0	0	0	0	0	0	0	0	0	0	0	0	.	+	.02	.08	.02	+	.	0	0	0	0	0	0	0	0	O
10	O	0	0	0	0	0	0	0	0	0	0	0	0	0	.	+	.01	.03	.01	+	.	0	0	0	0	0	0	0	0	O
11	O	0	0	0	0	0	0	0	0	0	0	0	0	0	.	+	+	.02	+	+	.	0	0	0	0	0	0	0	0	O
12	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.	0	0	0	0	0	0	0	0	0	0	0	O
13	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
14	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
15	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
16	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
17	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
18	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
19	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
20	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
21	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
22	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
23	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
24	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
25	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
26	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
27	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
28	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
29	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
30	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
31	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
32	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
33	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
34	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
35	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
36	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
37	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
38	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
39	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
40	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
41	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
42	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
43	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
44	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O

BEGIN LONG TERM SIMULATION OF FATE OF SAND

SUMMARY OF SAND DISTRIBUTIONS AFTER 300.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 35.655
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 901.81

SUMMARY OF SAND DISTRIBUTIONS AFTER 600.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 15.460
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 922.01

SUMMARY OF SAND DISTRIBUTIONS AFTER 900.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 7.8324
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 929.63

CONCENTRATIONS ABOVE BACKGROUND OF SAND (MG/L) IN THE CLOUD 900.00 SECONDS AFTER DUMP

60.00 FT BELOW THE WATER SURFACE

...MULTIPLY DISPLAYED VALUES BY 1.000 (LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)

M N=	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31
2	OOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOO																													
3	OOOO	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		00000
4	OOOO	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		00000
5	OOOO	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		00000
6	OOOO	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		00000
7	OOOO	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		00000
8	OOOO	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		00000
9	OOOO	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		00000
10	OOOO	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		00000
11	OOOO	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		00000
12	OOOO	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		00000
13	OOOO	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		00000
14	OOOO	0	0	0	0	0	0	0	0	0	0	0	0	0	.	.	+	+	+	.	.	0	0	0	0	0	0	0		00000
15	OOOO	0	0	0	0	0	0	0	0	0	0	0	.	.	+	+	.03	.04	.03	+	+	.	.	0	0	0	0	0		00000
16	OOOO	0	0	0	0	0	0	0	0	0	0	0	.	+	+	.05	.20	.31	.20	.05	+	+	.	0	0	0	0	0		00000
17	OOOO	0	0	0	0	0	0	0	0	0	0	0	.	.	+	.01	.04	.07	.04	.01	+	.	.	0	0	0	0	0		00000
18	OOOO	0	0	0	0	0	0	0	0	0	0	0	0	0	.	+	+	+	+	+	.	0	0	0	0	0	0	0		00000
19	OOOO	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		00000
20	OOOO	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		00000
21	OOOO	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		00000
22	OOOO	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		00000
23	OOOO	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		00000
24	OOOO	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		00000
25	OOOO	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		00000
26	OOOO	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		00000
27	OOOO	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		00000
28	OOOO	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		00000
29	OOOO	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		00000
30	OOOO	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		00000
31	OOOO	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		00000
32	OOOO	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		00000
33	OOOO	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		00000
34	OOOO	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		00000
35	OOOO	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		00000
36	OOOO	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		00000
37	OOOO	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		00000
38	OOOO	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		00000
39	OOOO	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		00000
40	OOOO	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		00000
41	OOOO	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		00000
42	OOOO	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		00000
43	OOOO	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		00000
44	OOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOO																													

CONCENTRATIONS ABOVE BACKGROUND OF SAND (MG/L) IN THE CLOUD 900.00 SECONDS AFTER DUMP

119.00 FT BELOW THE WATER SURFACE

...MULTIPLY DISPLAYED VALUES BY 1.000 (LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)

M N=	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	0	0	0	0	0	0	0	0	0	0	0	0	.	.	.	+	+	+	.	.	.	0	0	0	0	0	0	0	0	0
14	0	0	0	0	0	0	0	0	0	0	.	.	+	+	.02	.05	.06	.05	.02	+	+	.	.	0	0	0	0	0	0	0
15	0	0	0	0	0	0	0	0	0	.	.	+	.02	.21	1.1	3.2	4.7	3.2	1.1	.21	.02	+	.	.	0	0	0	0	0	0
16	0	0	0	0	0	0	0	0	0	.	+	+	.10	.99	5.7	18	26	18	5.7	.99	.10	+	+	.	0	0	0	0	0	0
17	0	0	0	0	0	0	0	0	0	.	+	+	.03	.32	1.7	4.9	7.1	4.9	1.7	.32	.03	+	+	.	0	0	0	0	0	0
18	0	0	0	0	0	0	0	0	0	0	.	+	+	+	.04	.10	.14	.10	.04	+	+	+	.	0	0	0	0	0	0	0
19	0	0	0	0	0	0	0	0	0	0	0	0	.	.	+	+	+	+	+	.	.	0	0	0	0	0	0	0	0	0
20	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
21	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
22	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
23	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
24	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
25	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
26	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
27	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
28	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
29	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
30	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
31	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
32	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
33	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
34	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
35	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
36	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
37	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
38	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
39	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
40	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
41	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
42	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
43	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
44	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0

BOTTOM ACCUMULATION OF SAND (CU FT/GRID SQUARE) , 900.00 SECONDS AFTER DUMP

...MULTIPLY DISPLAYED VALUES BY 1.000 (LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)

M N=	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31
2	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O
3	O	.	.	.	.	.	+	+	+	+	+	+	+	+	+	.01	.01	.01	.01	.01	+	+	+	+	+	+	+	+	+	O
4	O	.	.	+	+	+	+	+	+	+	.01	.02	.03	.04	.05	.06	.06	.07	.06	.06	.05	.04	.03	.02	.01	+	+	+	+	O
5	O	.	+	+	+	+	+	.01	.02	.04	.06	.10	.15	.20	.26	.30	.33	.35	.33	.30	.26	.20	.15	.10	.06	.04	.02	.01	+	O
6	O	+	+	+	+	.01	.02	.04	.08	.15	.25	.39	.57	.76	.96	1.1	1.2	1.3	1.2	1.1	.96	.76	.57	.39	.25	.15	.08	.04	.02	O
7	O	+	+	+	.01	.03	.06	.13	.25	.44	.73	1.1	1.6	2.2	2.7	3.2	3.6	3.7	3.6	3.2	2.7	2.2	1.6	1.1	.73	.44	.25	.13	.06	O
8	O	+	+	.01	.03	.07	.14	.29	.56	.98	1.6	2.4	3.5	4.8	6.1	7.2	8.0	8.3	8.0	7.2	6.1	4.8	3.5	2.4	1.6	.98	.56	.29	.14	O
9	O	+	+	.02	.05	.11	.25	.50	.94	1.6	2.7	4.2	6.0	8.2	11	13	14	14	14	13	11	8.2	6.0	4.2	2.7	1.6	.94	.50	.25	O
10	O	+	.01	.02	.06	.15	.32	.65	1.2	2.1	3.5	5.4	7.9	11	14	17	19	20	19	17	14	11	7.9	5.4	3.5	2.1	1.2	.65	.32	O
11	O	+	.01	.02	.06	.15	.32	.64	1.2	2.1	3.5	5.4	7.8	11	14	17	19	20	19	17	14	11	7.8	5.4	3.5	2.1	1.2	.64	.32	O
12	O	+	+	.02	.05	.11	.24	.49	.92	1.6	2.6	4.1	5.9	8.1	10	12	14	15	14	12	10	8.1	5.9	4.1	2.6	1.6	.92	.49	.24	O
13	O	+	+	.01	.02	.06	.14	.28	.54	.94	1.5	2.4	3.4	4.7	6.2	7.9	10	11	10	7.9	6.2	4.7	3.4	2.4	1.5	.94	.54	.28	.14	O
14	O	+	+	+	.01	.03	.06	.12	.24	.42	.70	1.0	1.5	2.1	2.8	3.6	4.7	5.3	4.7	3.6	2.8	2.1	1.5	1.0	.70	.42	.24	.12	.06	O
15	O	+	+	+	+	.01	.02	.04	.08	.14	.24	.37	.54	.74	.97	1.2	1.5	1.7	1.5	1.2	.97	.74	.54	.37	.24	.14	.08	.04	.02	O
16	O	.	+	+	+	+	+	.01	.02	.03	.06	.09	.14	.20	.32	.69	1.5	2.0	1.5	.69	.32	.20	.14	.09	.06	.03	.02	.01	+	O
17	O	.	.	+	+	+	+	+	+	+	.01	.02	.02	.04	.07	.18	.41	.55	.41	.18	.07	.04	.02	.02	.01	+	+	+	+	O
18	O	.	.	.	.	.	+	+	+	+	+	+	+	+	+	.01	.01	.02	.01	.01	+	+	+	+	+	+	+	+	+	O
19	O	0	0	.	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	O
20	O	0	0	0	0	0	.	.	.	.	.	.	.	.	.	+	+	+	+	+	.	.	.	.	.	.	.	.	.	O
21	O	0	0	0	0	0	0	0	0	0	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0	O
22	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
23	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
24	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
25	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
26	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
27	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
28	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
29	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
30	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
31	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
32	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
33	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
34	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
35	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
36	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
37	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
38	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
39	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
40	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
41	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
42	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
43	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
44	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O

SMALL CLOUDS AT 900.00 SECONDS ELAPSED TIME FOR SAND

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID	LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	753.3	450.0	5.460	0.0000E+00	96.88	75.77	44.23	0.100000
2	754.0	450.0	2.373	0.0000E+00	117.6	86.17	33.83	0.100000
3	754.4	450.0	0.4771E-04	0.0000E+00	155.1	117.3	2.729	0.100000
4	754.6	450.0	0.4942E-09	0.0000E+00	235.4	118.9	1.099	0.100000
5	754.5	450.0	0.0000E+00	0.0000E+00	358.6	119.0	1.007	0.100000
6	754.1	450.0	0.0000E+00	0.0000E+00	393.9	119.3	0.7279	0.100000

SUMMARY OF SAND DISTRIBUTIONS AFTER 1200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 3.4781
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 933.99

SUMMARY OF SAND DISTRIBUTIONS AFTER 1500.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 1.3740
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 936.09

SUMMARY OF SAND DISTRIBUTIONS AFTER 1800.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.48995
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 936.97

MAX CONC IS 0.00000000 OUTPUT SUPPRESSED AT 60.00 FT

CONCENTRATIONS ABOVE BACKGROUND OF SAND (MG/L) IN THE CLOUD 1800.00 SECONDS AFTER DUMP

119.00 FT BELOW THE WATER SURFACE

...MULTIPLY DISPLAYED VALUES BY 1.000 (LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)

M N=	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
18	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
19	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
20	0	0	0	0	0	0	0	0	0	0	0	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0	0	0	0
21	0	0	0	0	0	0	0	0	0	0	.	.	.	+	+	+	+	+	+	+	+	+	.	0	0	0	0	0	0	0
22	0	0	0	0	0	0	0	0	0	.	.	+	+	+	+	.01	.02	.03	.02	.01	+	+	+	0	0	0	0	0	0	0
23	0	0	0	0	0	0	0	0	.	+	+	+	.03	.07	.15	.24	.28	.24	.15	.07	.03	+	0	0	0	0	0	0	0	0
24	0	0	0	0	0	0	0	0	+	+	+	.02	.08	.23	.48	.73	.85	.73	.48	.23	.08	.02	0	0	0	0	0	0	0	0
25	0	0	0	0	0	0	0	0	+	+	+	.02	.08	.23	.46	.71	.82	.71	.46	.23	.08	.02	0	0	0	0	0	0	0	0
26	0	0	0	0	0	0	0	0	.	+	+	+	.02	.07	.14	.22	.25	.22	.14	.07	.02	+	0	0	0	0	0	0	0	0
27	0	0	0	0	0	0	0	0	.	.	+	+	+	+	.01	.02	.02	.02	.01	+	+	+	0	0	0	0	0	0	0	0
28	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
29	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
30	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
31	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
32	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
33	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
34	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
35	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
36	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
37	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
38	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
39	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
40	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
41	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
42	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
43	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
44	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0

BOTTOM ACCUMULATION OF SAND (CU FT/GRID SQUARE) , 1800.00 SECONDS AFTER DUMP

...MULTIPLY DISPLAYED VALUES BY 1.000 (LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)

M N=	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31
2	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O
3	O	O	O	.	.	.	.	.	+	+	+	+	+	+	+	+	+	.01	.01	.01	.01	.01	+	+	+	+	+	+	+	+	+0	O
4	O	O	O	.	.	+	+	+	+	+	.01	.02	.03	.04	.05	.06	.06	.07	.06	.06	.05	.04	.03	.02	.01	+	+	+	+0	O
5	O	O	O	.	+	+	+	+	+	.01	.02	.04	.06	.10	.15	.20	.26	.30	.33	.35	.33	.30	.26	.20	.15	.10	.06	.04	.02	.01	+0	O
6	O	O	O	+	+	+	+	.01	.02	.04	.08	.15	.25	.39	.57	.76	.96	1.1	1.2	1.3	1.2	1.1	.96	.76	.57	.39	.25	.15	.08	.04	.02	O
7	O	O	O	+	+	+	.01	.03	.06	.13	.25	.44	.73	1.1	1.6	2.2	2.7	3.2	3.6	3.7	3.6	3.2	2.7	2.2	1.6	1.1	.73	.44	.25	.13	.06	O
8	O	O	O	+	+	.01	.03	.07	.14	.29	.56	.98	1.6	2.4	3.5	4.8	6.1	7.2	8.0	8.3	8.0	7.2	6.1	4.8	3.5	2.4	1.6	.98	.56	.29	.14	O
9	O	O	O	+	+	.02	.05	.11	.25	.50	.94	1.6	2.7	4.2	6.0	8.2	11	13	14	14	14	13	11	8.2	6.0	4.2	2.7	1.6	.94	.50	.25	O
10	O	O	O	+	.01	.02	.06	.15	.32	.65	1.2	2.1	3.5	5.4	7.9	11	14	17	19	20	19	17	14	11	7.9	5.4	3.5	2.1	1.2	.65	.32	O
11	O	O	O	+	.01	.02	.06	.15	.32	.64	1.2	2.1	3.5	5.4	7.8	11	14	17	19	20	19	17	14	11	7.8	5.4	3.5	2.1	1.2	.64	.32	O
12	O	O	O	+	+	.02	.05	.11	.24	.49	.92	1.6	2.6	4.1	5.9	8.1	10	12	14	15	14	12	10	8.1	5.9	4.1	2.6	1.6	.92	.49	.24	O
13	O	O	O	+	+	.01	.02	.06	.14	.28	.54	.94	1.5	2.4	3.4	4.7	6.2	7.9	10	11	10	7.9	6.2	4.7	3.4	2.4	1.5	.94	.54	.28	.14	O
14	O	O	O	+	+	+	.01	.03	.06	.12	.24	.42	.70	1.0	1.5	2.1	2.8	3.6	4.7	5.3	4.7	3.6	2.8	2.1	1.5	1.0	.70	.42	.24	.12	.06	O
15	O	O	O	+	+	+	+	.01	.02	.04	.08	.14	.24	.37	.54	.74	.97	1.2	1.5	1.7	1.5	1.2	.97	.74	.54	.37	.24	.14	.08	.04	.02	O
16	O	O	O	.	+	+	+	+	+	.01	.02	.03	.06	.09	.14	.20	.32	.69	1.5	2.0	1.5	.69	.32	.20	.14	.09	.06	.03	.02	.01	+0	O
17	O	O	O	.	.	+	+	+	+	+	.01	.02	.02	.04	.07	.19	.42	.57	.42	.19	.07	.04	.02	.02	.01	+	+	+	+0	O
18	O	O	O	.	.	.	.	.	+	+	+	+	+	.01	.04	.12	.26	.34	.26	.12	.04	.01	+	+	+	+	+	+	+0	O
19	O	O	0	0	.	.	.	.	.	+	+	+	+	.01	.07	.24	.54	.70	.54	.24	.07	.01	+	+	+	+	+	.	.	.0	O
20	O	O	0	0	0	0	.	.	.	.	.	+	+	+	+	.02	.08	.17	.22	.17	.08	.02	+	+	+	.	.	.	.	.0	O
21	O	O	0	0	0	0	0	0	0	.	.	+	+	+	+	.03	.08	.15	.18	.15	.08	.03	+	+	+	.	.	0	0	00	O
22	O	O	0	0	0	0	0	0	0	.	.	+	+	.01	.04	.11	.19	.23	.19	.11	.04	.01	+	+	.	.	0	0	00	O
23	O	O	0	0	0	0	0	0	0	.	.	+	+	+	.01	.04	.07	.08	.07	.04	.01	+	+	+	.	.	0	0	00	O
24	O	O	0	0	0	0	0	0	.	.	.	+	+	+	.02	.04	.06	.07	.06	.04	.02	+	+	+	.	.	.	0	00	O
25	O	O	0	0	0	0	0	0	.	.	.	+	+	+	.01	.03	.05	.06	.05	.03	.01	+	+	+	.	.	.	0	00	O
26	O	O	0	0	0	0	0	0	0	.	.	+	+	+	+	.01	.01	.02	.01	.01	+	+	+	+	.	.	0	0	00	O
27	O	O	0	0	0	0	0	0	0	0	.	.	.	+	+	+	+	+	+	+	+	+	.	.	.	0	0	0	00	O
28	O	O	0	0	0	0	0	0	0	0	0	.	.	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0	00	O
29	O	O	0	0	0	0	0	0	0	0	0	0	0	0	0	.	.	.	.	.	0	0	0	0	0	0	0	0	0	00	O
30	O	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00	O
31	O	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00	O
32	O	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00	O
33	O	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00	O
34	O	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00	O
35	O	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00	O
36	O	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00	O
37	O	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00	O
38	O	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00	O
39	O	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00	O
40	O	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00	O
41	O	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00	O
42	O	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00	O
43	O	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00	O
44	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O

SMALL CLOUDS AT 1800.00 SECONDS ELAPSED TIME FOR SAND

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID	LOCATION OF CLOUD CENTROID DISTANCE FROM LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	1174.	450.0	0.3984	0.0000E+00	161.8	90.80	29.20	0.100000
2	1174.	450.0	0.9152E-01	0.0000E+00	186.4	96.22	23.78	0.100000

SUMMARY OF SAND DISTRIBUTIONS AFTER 2100.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.15762
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 937.31

SUMMARY OF SAND DISTRIBUTIONS AFTER 2400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.45255E-01
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 937.42

SUMMARY OF SAND DISTRIBUTIONS AFTER 2700.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.11316E-01
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 937.45

MAX CONC IS 0.00000000 OUTPUT SUPPRESSED AT 60.00 FT

MAX CONC IS 0.00000001 OUTPUT SUPPRESSED AT 119.00 FT

BOTTOM ACCUMULATION OF SAND (CU FT/GRID SQUARE) , 2700.00 SECONDS AFTER DUMP

...MULTIPLY DISPLAYED VALUES BY 1.000 (LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)

M N=	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31
2	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O
3	O	O	O	.	.	.	.	.	+	+	+	+	+	+	+	+	+	.01	.01	.01	.01	.01	+	+	+	+	+	+	+	+	+0	O
4	O	O	O	.	.	+	+	+	+	+	+	.01	.02	.03	.04	.05	.06	.06	.07	.06	.06	.05	.04	.03	.02	.01	+	+	+	+0	O
5	O	O	O	.	+	+	+	+	+	.01	.02	.04	.06	.10	.15	.20	.26	.30	.33	.35	.33	.30	.26	.20	.15	.10	.06	.04	.02	.01	+0	O
6	O	O	O	+	+	+	+	.01	.02	.04	.08	.15	.25	.39	.57	.76	.96	1.1	1.2	1.3	1.2	1.1	.96	.76	.57	.39	.25	.15	.08	.04	.02	O
7	O	O	O	+	+	+	.01	.03	.06	.13	.25	.44	.73	1.1	1.6	2.2	2.7	3.2	3.6	3.7	3.6	3.2	2.7	2.2	1.6	1.1	.73	.44	.25	.13	.06	O
8	O	O	O	+	+	.01	.03	.07	.14	.29	.56	.98	1.6	2.4	3.5	4.8	6.1	7.2	8.0	8.3	8.0	7.2	6.1	4.8	3.5	2.4	1.6	.98	.56	.29	.14	O
9	O	O	O	+	+	.02	.05	.11	.25	.50	.94	1.6	2.7	4.2	6.0	8.2	11	13	14	14	14	13	11	8.2	6.0	4.2	2.7	1.6	.94	.50	.25	O
10	O	O	O	+	.01	.02	.06	.15	.32	.65	1.2	2.1	3.5	5.4	7.9	11	14	17	19	20	19	17	14	11	7.9	5.4	3.5	2.1	1.2	.65	.32	O
11	O	O	O	+	.01	.02	.06	.15	.32	.64	1.2	2.1	3.5	5.4	7.8	11	14	17	19	20	19	17	14	11	7.8	5.4	3.5	2.1	1.2	.64	.32	O
12	O	O	O	+	+	.02	.05	.11	.24	.49	.92	1.6	2.6	4.1	5.9	8.1	10	12	14	15	14	12	10	8.1	5.9	4.1	2.6	1.6	.92	.49	.24	O
13	O	O	O	+	+	.01	.02	.06	.14	.28	.54	.94	1.5	2.4	3.4	4.7	6.2	7.9	10	11	10	7.9	6.2	4.7	3.4	2.4	1.5	.94	.54	.28	.14	O
14	O	O	O	+	+	+	.01	.03	.06	.12	.24	.42	.70	1.0	1.5	2.1	2.8	3.6	4.7	5.3	4.7	3.6	2.8	2.1	1.5	1.0	.70	.42	.24	.12	.06	O
15	O	O	O	+	+	+	+	.01	.02	.04	.08	.14	.24	.37	.54	.74	.97	1.2	1.5	1.7	1.5	1.2	.97	.74	.54	.37	.24	.14	.08	.04	.02	O
16	O	O	.	+	+	+	+	+	.01	.02	.03	.06	.09	.14	.20	.32	.69	1.5	2.0	1.5	.69	.32	.20	.14	.09	.06	.03	.02	.01	+0	O
17	O	O	O	.	.	+	+	+	+	+	.01	.02	.02	.04	.07	.19	.42	.57	.42	.19	.07	.04	.02	.02	.01	+	+	+	+0	O
18	O	O	O	.	.	.	.	.	+	+	+	+	.01	.04	.12	.26	.34	.26	.12	.04	.01	+	+	+	+	+	+	+	+0	O
19	O	O	0	0	.	.	.	.	.	+	+	+	+	.01	.07	.24	.54	.70	.54	.24	.07	.01	+	+	+	+	+	.	.	.0	O
20	O	O	0	0	0	0	.	.	.	.	.	+	+	+	.02	.08	.17	.22	.17	.08	.02	+	+	+	.	.	.	.	.0	O
21	O	O	0	0	0	0	0	0	0	.	.	+	+	+	.03	.08	.15	.18	.15	.08	.03	+	+	+	.	.	0	0	00	O
22	O	O	0	0	0	0	0	0	0	.	.	+	+	.01	.04	.11	.19	.23	.19	.11	.04	.01	+	+	.	.	0	0	00	O
23	O	O	0	0	0	0	0	0	0	.	.	+	+	+	.01	.04	.07	.08	.07	.04	.01	+	+	+	.	.	0	0	00	O
24	O	O	0	0	0	0	0	0	.	.	.	+	+	+	.02	.04	.06	.07	.06	.04	.02	+	+	+	.	.	.	0	00	O
25	O	O	0	0	0	0	0	0	.	.	+	+	+	+	.01	.04	.06	.07	.06	.04	.01	+	+	+	+	.	.	0	00	O
26	O	O	0	0	0	0	0	0	.	.	.	+	+	+	.01	.01	.02	.03	.02	.01	.01	+	+	+	.	.	.	0	00	O
27	O	O	0	0	0	0	0	0	.	.	+	+	+	+	+	.01	.02	.02	.02	.01	+	+	+	+	+	.	.	0	00	O
28	O	O	0	0	0	0	0	.	.	.	+	+	+	+	+	.01	.01	.01	.01	.01	+	+	+	+	+	.	.	.	00	O
29	O	O	0	0	0	0	0	.	.	.	+	+	+	+	+	+	+	.01	+	+	+	+	+	+	+	.	.	.	00	O
30	O	O	0	0	0	0	0	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	00	O
31	O	O	0	0	0	0	0	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	00	O
32	O	O	0	0	0	0	0	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	00	O
33	O	O	0	0	0	0	0	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	00	O
34	O	O	0	0	0	0	0	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	00	O
35	O	O	0	0	0	0	0	0	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	0	00	O
36	O	O	0	0	0	0	0	0	0	.	.	.	.	.	.	.	.	+	.	.	.	.	.	.	.	.	0	0	00	O
37	O	O	0	0	0	0	0	0	0	0	0	.	.	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0	00	O
38	O	O	0	0	0	0	0	0	0	0	0	0	0	0	0	.	.	.	.	.	0	0	0	0	0	0	0	0	0	00	O
39	O	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00	O
40	O	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00	O
41	O	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00	O
42	O	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00	O
43	O	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00	O
44	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O

SMALL CLOUDS AT 2700.00 SECONDS ELAPSED TIME FOR SAND

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID	LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	1594.	450.0	0.1045E-01	0.0000E+00	237.6	98.72	21.28	0.100000
2	1595.	450.0	0.8684E-03	0.0000E+00	265.5	104.1	15.94	0.100000

SUMMARY OF SAND DISTRIBUTIONS AFTER 3000.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.23792E-02
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 937.46

SUMMARY OF SAND DISTRIBUTIONS AFTER 3300.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.39921E-03
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 937.46

SUMMARY OF SAND DISTRIBUTIONS AFTER 3600.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.49171E-04
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 937.46

MAX CONC IS 0.00000000 OUTPUT SUPPRESSED AT 60.00 FT

MAX CONC IS 0.00000000 OUTPUT SUPPRESSED AT 119.00 FT

BOTTOM ACCUMULATION OF SAND (CU FT/GRID SQUARE) , 3600.00 SECONDS AFTER DUMP

...MULTIPLY DISPLAYED VALUES BY 1.000 (LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)

M N=	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31
2	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O
3	O	O	O	.	.	.	.	.	+	+	+	+	+	+	+	+	+	.01	.01	.01	.01	.01	+	+	+	+	+	+	+	+	+0	O
4	O	O	O	.	.	+	+	+	+	+	+	.01	.02	.03	.04	.05	.06	.06	.07	.06	.06	.05	.04	.03	.02	.01	+	+	+	+0	O
5	O	O	O	.	+	+	+	+	+	.01	.02	.04	.06	.10	.15	.20	.26	.30	.33	.35	.33	.30	.26	.20	.15	.10	.06	.04	.02	.01	+0	O
6	O	O	O	+	+	+	+	.01	.02	.04	.08	.15	.25	.39	.57	.76	.96	1.1	1.2	1.3	1.2	1.1	.96	.76	.57	.39	.25	.15	.08	.04	.02	O
7	O	O	O	+	+	+	.01	.03	.06	.13	.25	.44	.73	1.1	1.6	2.2	2.7	3.2	3.6	3.7	3.6	3.2	2.7	2.2	1.6	1.1	.73	.44	.25	.13	.06	O
8	O	O	O	+	+	.01	.03	.07	.14	.29	.56	.98	1.6	2.4	3.5	4.8	6.1	7.2	8.0	8.3	8.0	7.2	6.1	4.8	3.5	2.4	1.6	.98	.56	.29	.14	O
9	O	O	O	+	+	.02	.05	.11	.25	.50	.94	1.6	2.7	4.2	6.0	8.2	11	13	14	14	14	13	11	8.2	6.0	4.2	2.7	1.6	.94	.50	.25	O
10	O	O	O	+	.01	.02	.06	.15	.32	.65	1.2	2.1	3.5	5.4	7.9	11	14	17	19	20	19	17	14	11	7.9	5.4	3.5	2.1	1.2	.65	.32	O
11	O	O	O	+	.01	.02	.06	.15	.32	.64	1.2	2.1	3.5	5.4	7.8	11	14	17	19	20	19	17	14	11	7.8	5.4	3.5	2.1	1.2	.64	.32	O
12	O	O	O	+	+	.02	.05	.11	.24	.49	.92	1.6	2.6	4.1	5.9	8.1	10	12	14	15	14	12	10	8.1	5.9	4.1	2.6	1.6	.92	.49	.24	O
13	O	O	O	+	+	.01	.02	.06	.14	.28	.54	.94	1.5	2.4	3.4	4.7	6.2	7.9	10	11	10	7.9	6.2	4.7	3.4	2.4	1.5	.94	.54	.28	.14	O
14	O	O	O	+	+	+	.01	.03	.06	.12	.24	.42	.70	1.0	1.5	2.1	2.8	3.6	4.7	5.3	4.7	3.6	2.8	2.1	1.5	1.0	.70	.42	.24	.12	.06	O
15	O	O	O	+	+	+	+	.01	.02	.04	.08	.14	.24	.37	.54	.74	.97	1.2	1.5	1.7	1.5	1.2	.97	.74	.54	.37	.24	.14	.08	.04	.02	O
16	O	O	O	.	+	+	+	+	+	.01	.02	.03	.06	.09	.14	.20	.32	.69	1.5	2.0	1.5	.69	.32	.20	.14	.09	.06	.03	.02	.01	+0	O
17	O	O	O	.	.	+	+	+	+	+	.01	.02	.02	.04	.07	.19	.42	.57	.42	.19	.07	.04	.02	.02	.01	+	+	+	+	+	+0	O
18	O	O	O	.	.	.	.	.	+	+	+	+	+	.01	.04	.12	.26	.34	.26	.12	.04	.01	+	+	+	+	+	+	+	+	+0	O
19	O	O	0	0	.	.	.	.	.	.	+	+	+	.01	.07	.24	.54	.70	.54	.24	.07	.01	+	+	+	+	.	.	.	.	.0	O
20	O	O	0	0	0	0	.	.	.	.	.	+	+	+	.02	.08	.17	.22	.17	.08	.02	+	+	+	.	.	.	.	.	.0	O
21	O	O	0	0	0	0	0	0	0	.	.	+	+	+	.03	.08	.15	.18	.15	.08	.03	+	+	+	.	.	0	0	0	00	O
22	O	O	0	0	0	0	0	0	0	.	.	+	+	.01	.04	.11	.19	.23	.19	.11	.04	.01	+	+	.	.	0	0	0	00	O
23	O	O	0	0	0	0	0	0	0	.	.	+	+	+	.01	.04	.07	.08	.07	.04	.01	+	+	+	.	.	0	0	0	00	O
24	O	O	0	0	0	0	0	0	.	.	.	+	+	+	.02	.04	.06	.07	.06	.04	.02	+	+	+	.	.	.	0	0	00	O
25	O	O	0	0	0	0	0	0	.	.	+	+	+	+	.01	.04	.06	.07	.06	.04	.01	+	+	+	+	.	.	0	0	00	O
26	O	O	0	0	0	0	0	0	.	.	.	+	+	+	.01	.01	.02	.03	.02	.01	.01	+	+	+	.	.	.	0	0	00	O
27	O	O	0	0	0	0	0	0	.	.	+	+	+	+	+	.01	.02	.02	.02	.01	+	+	+	+	+	.	.	0	0	00	O
28	O	O	0	0	0	0	0	.	.	.	+	+	+	+	+	.01	.01	.01	.01	.01	+	+	+	+	+	.	.	.	0	0	O
29	O	O	0	0	0	0	0	.	.	.	+	+	+	+	+	+	+	.01	+	+	+	+	+	+	+	.	.	.	0	0	O
30	O	O	0	0	0	0	0	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	0	0	O
31	O	O	0	0	0	0	0	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	0	O
32	O	O	0	0	0	0	0	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	0	O
33	O	O	0	0	0	0	0	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	0	O
34	O	O	0	0	0	0	0	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	0	O
35	O	O	0	0	0	0	0	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	0	O
36	O	O	0	0	0	0	0	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	0	O
37	O	O	0	0	0	0	0	.	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	0	O
38	O	O	0	0	0	0	0	.	.	.	.	.	.	.	.	+	+	+	+	+	.	.	.	.	.	.	.	.	.	0	O
39	O	O	0	0	0	0	0	0	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	0	0	O
40	O	O	0	0	0	0	0	0	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	0	0	O
41	O	O	0	0	0	0	0	0	0	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	O
42	O	O	0	0	0	0	0	0	0	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	O
43	O	O	0	0	0	0	0	0	0	0	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0	O
44	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O

SMALL CLOUDS AT 3600.00 SECONDS ELAPSED TIME FOR SAND

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID	LOCATION OF CLOUD CENTROID DISTANCE FROM LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	2014.	450.0	0.4887E-04	0.0000E+00	322.9	106.6	13.43	0.100000
2	2015.	450.0	0.3007E-06	0.0000E+00	353.9	111.9	8.101	0.100000

BOTTOM ACCUMULATION OF SAND (CU FT/GRID SQUARE) , 3600.00 SECONDS AFTER DUMP

...MULTIPLY DISPLAYED VALUES BY 1.000 (LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)

M N=	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31
2	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O
3	O	O	O	.	.	.	.	.	+	+	+	+	+	+	+	+	+	.01	.01	.01	.01	.01	+	+	+	+	+	+	+	+	+0	O
4	O	O	O	.	.	+	+	+	+	+	+	.01	.02	.03	.04	.05	.06	.06	.07	.06	.06	.05	.04	.03	.02	.01	+	+	+	+0	O
5	O	O	O	.	+	+	+	+	+	.01	.02	.04	.06	.10	.15	.20	.26	.30	.33	.35	.33	.30	.26	.20	.15	.10	.06	.04	.02	.01	+0	O
6	O	O	O	+	+	+	+	.01	.02	.04	.08	.15	.25	.39	.57	.76	.96	1.1	1.2	1.3	1.2	1.1	.96	.76	.57	.39	.25	.15	.08	.04	.02	O
7	O	O	O	+	+	+	.01	.03	.06	.13	.25	.44	.73	1.1	1.6	2.2	2.7	3.2	3.6	3.7	3.6	3.2	2.7	2.2	1.6	1.1	.73	.44	.25	.13	.06	O
8	O	O	O	+	+	.01	.03	.07	.14	.29	.56	.98	1.6	2.4	3.5	4.8	6.1	7.2	8.0	8.3	8.0	7.2	6.1	4.8	3.5	2.4	1.6	.98	.56	.29	.14	O
9	O	O	O	+	+	.02	.05	.11	.25	.50	.94	1.6	2.7	4.2	6.0	8.2	11	13	14	14	14	13	11	8.2	6.0	4.2	2.7	1.6	.94	.50	.25	O
10	O	O	O	+	.01	.02	.06	.15	.32	.65	1.2	2.1	3.5	5.4	7.9	11	14	17	19	20	19	17	14	11	7.9	5.4	3.5	2.1	1.2	.65	.32	O
11	O	O	O	+	.01	.02	.06	.15	.32	.64	1.2	2.1	3.5	5.4	7.8	11	14	17	19	20	19	17	14	11	7.8	5.4	3.5	2.1	1.2	.64	.32	O
12	O	O	O	+	+	.02	.05	.11	.24	.49	.92	1.6	2.6	4.1	5.9	8.1	10	12	14	15	14	12	10	8.1	5.9	4.1	2.6	1.6	.92	.49	.24	O
13	O	O	O	+	+	.01	.02	.06	.14	.28	.54	.94	1.5	2.4	3.4	4.7	6.2	7.9	10	11	10	7.9	6.2	4.7	3.4	2.4	1.5	.94	.54	.28	.14	O
14	O	O	O	+	+	+	.01	.03	.06	.12	.24	.42	.70	1.0	1.5	2.1	2.8	3.6	4.7	5.3	4.7	3.6	2.8	2.1	1.5	1.0	.70	.42	.24	.12	.06	O
15	O	O	O	+	+	+	+	.01	.02	.04	.08	.14	.24	.37	.54	.74	.97	1.2	1.5	1.7	1.5	1.2	.97	.74	.54	.37	.24	.14	.08	.04	.02	O
16	O	O	O	.	+	+	+	+	+	.01	.02	.03	.06	.09	.14	.20	.32	.69	1.5	2.0	1.5	.69	.32	.20	.14	.09	.06	.03	.02	.01	+0	O
17	O	O	O	.	.	+	+	+	+	+	.01	.02	.02	.04	.07	.19	.42	.57	.42	.19	.07	.04	.02	.02	.01	+	+	+	+	+	+0	O
18	O	O	O	.	.	.	.	.	+	+	+	+	+	.01	.04	.12	.26	.34	.26	.12	.04	.01	+	+	+	+	+	+	+	+	+0	O
19	O	O	0	0	.	.	.	.	.	.	+	+	+	.01	.07	.24	.54	.70	.54	.24	.07	.01	+	+	+	+	.	.	.	.	.0	O
20	O	O	0	0	0	0	.	.	.	.	.	+	+	+	.02	.08	.17	.22	.17	.08	.02	+	+	+	.	.	.	.	.	.0	O
21	O	O	0	0	0	0	0	0	0	.	.	+	+	+	.03	.08	.15	.18	.15	.08	.03	+	+	+	.	.	0	0	0	00	O
22	O	O	0	0	0	0	0	0	0	.	.	+	+	.01	.04	.11	.19	.23	.19	.11	.04	.01	+	+	.	.	0	0	0	00	O
23	O	O	0	0	0	0	0	0	0	.	.	+	+	+	.01	.04	.07	.08	.07	.04	.01	+	+	+	.	.	0	0	0	00	O
24	O	O	0	0	0	0	0	0	.	.	.	+	+	+	.02	.04	.06	.07	.06	.04	.02	+	+	+	.	.	.	0	0	00	O
25	O	O	0	0	0	0	0	0	.	.	+	+	+	+	.01	.04	.06	.07	.06	.04	.01	+	+	+	+	.	.	0	0	00	O
26	O	O	0	0	0	0	0	0	.	.	.	+	+	+	.01	.01	.02	.03	.02	.01	.01	+	+	+	.	.	.	0	0	00	O
27	O	O	0	0	0	0	0	0	.	.	+	+	+	+	+	.01	.02	.02	.02	.01	+	+	+	+	+	.	.	0	0	00	O
28	O	O	0	0	0	0	0	.	.	.	+	+	+	+	+	.01	.01	.01	.01	.01	+	+	+	+	+	.	.	.	0	0	O
29	O	O	0	0	0	0	0	.	.	.	+	+	+	+	+	+	+	.01	+	+	+	+	+	+	+	.	.	.	0	0	O
30	O	O	0	0	0	0	0	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	0	0	O
31	O	O	0	0	0	0	0	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	0	O
32	O	O	0	0	0	0	0	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	0	O
33	O	O	0	0	0	0	0	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	0	O
34	O	O	0	0	0	0	0	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	0	O
35	O	O	0	0	0	0	0	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	0	O
36	O	O	0	0	0	0	0	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	0	O
37	O	O	0	0	0	0	0	.	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	0	O
38	O	O	0	0	0	0	0	.	.	.	.	.	.	.	.	+	+	+	+	+	.	.	.	.	.	.	.	.	.	0	O
39	O	O	0	0	0	0	0	0	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	0	0	O
40	O	O	0	0	0	0	0	0	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	0	0	O
41	O	O	0	0	0	0	0	0	0	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	O
42	O	O	0	0	0	0	0	0	0	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	O
43	O	O	0	0	0	0	0	0	0	0	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0	O
44	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O

THICKNESS (FT) OF SAND ACCUMULATED ON BOTTOM, 3600.00 SECONDS AFTER DUMP
...MULTIPLY DISPLAYED VALUES BY 0.1000E-01 (LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)

M N=	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31
2	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O
3	O	0	0	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.0	0
4	O	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+0	0
5	O	.	.	.	+	+	+	+	+	+	+	.01	.01	.02	.03	.03	.04	.04	.04	.03	.03	.02	.01	.01	+	+	+	+	+0	0
6	O	.	.	+	+	+	+	+	.01	.02	.03	.05	.07	.09	.12	.14	.16	.16	.16	.14	.12	.09	.07	.05	.03	.02	.01	+	+0	0
7	O	+	+	+	+	+	+	.01	.03	.05	.09	.14	.20	.28	.35	.41	.46	.47	.46	.41	.35	.28	.20	.14	.09	.05	.03	.01	+0	0
8	O	+	+	+	+	+	.01	.03	.07	.12	.20	.31	.46	.62	.78	.93	1.0	1.0	1.0	.93	.78	.62	.46	.31	.20	.12	.07	.03	.01	0
9	O	+	+	+	+	.01	.03	.06	.12	.21	.35	.53	.78	1.0	1.3	1.6	1.7	1.8	1.7	1.6	1.3	1.0	.78	.53	.35	.21	.12	.06	.03	0
10	O	+	+	+	+	.01	.04	.08	.15	.27	.45	.70	1.0	1.3	1.7	2.1	2.4	2.5	2.4	2.1	1.7	1.3	1.0	.70	.45	.27	.15	.08	.04	0
11	O	+	+	+	+	.01	.04	.08	.15	.27	.45	.69	1.0	1.3	1.7	2.1	2.4	2.5	2.4	2.1	1.7	1.3	1.0	.69	.45	.27	.15	.08	.04	0
12	O	+	+	+	+	.01	.03	.06	.11	.20	.34	.52	.76	1.0	1.3	1.5	1.7	1.8	1.7	1.5	1.3	1.0	.76	.52	.34	.20	.11	.06	.03	0
13	O	+	+	+	+	+	.01	.03	.06	.12	.20	.30	.44	.60	.79	1.0	1.2	1.4	1.2	1.0	.79	.60	.44	.30	.20	.12	.06	.03	.01	0
14	O	.	+	+	+	+	+	.01	.03	.05	.08	.13	.20	.27	.36	.47	.60	.68	.60	.47	.36	.27	.20	.13	.08	.05	.03	.01	+0	0
15	O	.	.	+	+	+	+	+	.01	.01	.03	.04	.06	.09	.12	.15	.20	.22	.20	.15	.12	.09	.06	.04	.03	.01	.01	+	+0	0
16	O	.	.	.	+	+	+	+	+	+	+	.01	.01	.02	.04	.08	.19	.26	.19	.08	.04	.02	.01	.01	+	+	+	+	+0	0
17	O	.	.	.	.	.	+	+	+	+	+	+	+	+	+	.02	.05	.07	.05	.02	+	+	+	+	+	+	+	+	+0	0
18	O	0	0	.	.	.	.	.	.	+	+	+	+	+	+	.01	.03	.04	.03	.01	+	+	+	+	+	+	+	.	.0	0
19	O	0	0	0	0	.	.	.	.	.	.	.	+	+	+	.03	.06	.09	.06	.03	+	+	+	.	.	.	.	.	.0	0
20	O	0	0	0	0	0	0	0	.	.	.	.	+	+	+	.01	.02	.02	.02	.01	+	+	+	.	.	.	.	0	0	0
21	O	0	0	0	0	0	0	0	0	0	.	.	+	+	+	.01	.01	.02	.01	.01	+	+	+	.	.	0	0	0	0	0
22	O	0	0	0	0	0	0	0	0	0	.	.	+	+	+	.01	.02	.03	.02	.01	+	+	+	.	.	0	0	0	0	0
23	O	0	0	0	0	0	0	0	0	0	.	.	+	+	+	+	+	.01	+	+	+	+	+	.	.	0	0	0	0	0
24	O	0	0	0	0	0	0	0	0	.	.	.	+	+	+	+	+	+	+	+	+	+	+	.	.	.	0	0	0	0
25	O	0	0	0	0	0	0	0	0	.	.	.	+	+	+	+	+	+	+	+	+	+	+	.	.	.	0	0	0	0
26	O	0	0	0	0	0	0	0	0	.	.	.	+	+	+	+	+	+	+	+	+	+	+	.	.	.	0	0	0	0
27	O	0	0	0	0	0	0	0	0	.	.	.	+	+	+	+	+	+	+	+	+	+	+	.	.	.	0	0	0	0
28	O	0	0	0	0	0	0	0	0	.	.	.	+	+	+	+	+	+	+	+	+	+	+	.	.	.	0	0	0	0
29	O	0	0	0	0	0	0	0	0	.	.	.	+	+	+	+	+	+	+	+	+	+	+	.	.	.	0	0	0	0
30	O	0	0	0	0	0	0	0	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	0	0	0
31	O	0	0	0	0	0	0	0	.	.	.	.	.	+	+	+	+	+	+	+	+	+	.	.	.	.	.	0	0	0
32	O	0	0	0	0	0	0	0	0	.	.	.	.	+	+	+	+	+	+	+	+	+	.	.	.	.	0	0	0	0
33	O	0	0	0	0	0	0	0	0	.	.	.	.	.	+	+	+	+	+	+	+	.	.	.	.	.	0	0	0	0
34	O	0	0	0	0	0	0	0	0	.	.	.	.	.	.	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0
35	O	0	0	0	0	0	0	0	0	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0
36	O	0	0	0	0	0	0	0	0	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0
37	O	0	0	0	0	0	0	0	0	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0
38	O	0	0	0	0	0	0	0	0	0	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0
39	O	0	0	0	0	0	0	0	0	0	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0
40	O	0	0	0	0	0	0	0	0	0	0	.	.	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0	0
41	O	0	0	0	0	0	0	0	0	0	0	0	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0	0	0
42	O	0	0	0	0	0	0	0	0	0	0	0	0	0	.	.	.	.	.	.	.	.	0	0	0	0	0	0	0	0
43	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
44	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O

BEGIN LONG TERM SIMULATION OF FATE OF SILT

SUMMARY OF SILT DISTRIBUTIONS AFTER 300.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 3957.5
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 1647.6

SUMMARY OF SILT DISTRIBUTIONS AFTER 600.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 2135.7
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 3466.2

SUMMARY OF SILT DISTRIBUTIONS AFTER 900.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 660.02
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 4937.4

CONCENTRATIONS ABOVE BACKGROUND OF SILT (MG/L) IN THE CLOUD 900.00 SECONDS AFTER DUMP

60.00 FT BELOW THE WATER SURFACE

...MULTIPLY DISPLAYED VALUES BY 1.000 (LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)

M N=	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	0
9	0	0	0	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	0
10	0	0	0	+	+	+	+	+	+	.01	.01	.01	.02	.02	.03	.03	.03	.03	.03	.02	.02	.01	.01	.01	+	+	+	+	+	0
11	0	0	0	+	+	+	+	.01	.02	.03	.04	.06	.08	.10	.11	.12	.12	.12	.11	.10	.08	.06	.04	.03	.02	.01	+	+	+	0
12	0	0	0	+	+	.01	.02	.03	.06	.09	.13	.17	.22	.27	.31	.33	.34	.33	.31	.27	.22	.17	.13	.09	.06	.03	.02	+	+	0
13	0	0	0	+	.01	.02	.05	.08	.13	.19	.28	.38	.49	.59	.68	.74	.77	.74	.68	.59	.49	.38	.28	.19	.13	.08	.05	+	+	0
14	0	0	0	.01	.02	.04	.08	.14	.23	.35	.50	.67	.89	1.2	2.0	3.4	4.2	3.4	2.0	1.2	.89	.67	.50	.35	.23	.14	.08	+	+	0
15	0	0	0	.01	.03	.06	.12	.20	.32	.49	.71	1.0	2.2	10	46	123	174	123	46	10	2.2	1.0	.71	.49	.32	.20	.12	+	+	0
16	0	0	0	.02	.04	.07	.14	.23	.37	.56	.82	1.3	5.6	40	212	620	894	620	212	40	5.6	1.3	.82	.56	.37	.23	.14	+	+	0
17	0	0	0	.01	.03	.07	.12	.21	.34	.51	.74	1.1	2.8	14	67	183	260	183	67	14	2.8	1.1	.74	.51	.34	.21	.12	+	+	0
18	0	0	0	.01	.02	.05	.09	.15	.25	.37	.53	.73	.99	1.5	3.1	5.9	7.5	5.9	3.1	1.5	.99	.73	.53	.37	.25	.15	.09	+	+	0
19	0	0	0	+	.01	.03	.05	.09	.14	.22	.31	.42	.54	.66	.77	.84	.87	.84	.77	.66	.54	.42	.31	.22	.14	.09	.05	+	+	0
20	0	0	0	+	+	.01	.02	.04	.07	.10	.15	.20	.26	.31	.36	.39	.40	.39	.36	.31	.26	.20	.15	.10	.07	.04	.02	+	+	0
21	0	0	0	+	+	+	.01	.01	.02	.04	.05	.07	.09	.12	.13	.14	.15	.14	.13	.12	.09	.07	.05	.04	.02	.01	.01	+	+	0
22	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
23	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
24	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
25	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
26	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
27	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
28	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
29	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
30	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
31	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
32	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
33	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
34	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
35	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
36	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
37	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
38	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
39	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
40	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
41	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
42	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
43	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
44	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0

CONCENTRATIONS ABOVE BACKGROUND OF SILT (MG/L) IN THE CLOUD 900.00 SECONDS AFTER DUMP

119.00 FT BELOW THE WATER SURFACE

...MULTIPLY DISPLAYED VALUES BY 1.000 (LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)

M N=	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31
2	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O
3	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
4	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
5	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
6	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
7	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
8	O	0	0	0	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	O
9	O	0	0	0	+	+	+	+	+	+	+	.01	.01	.02	.02	.03	.03	.03	.03	.03	.02	.02	.01	.01	+	+	+	+	+	O
10	O	0	0	0	+	+	+	+	.01	.02	.04	.06	.09	.13	.17	.21	.23	.24	.23	.21	.17	.13	.09	.06	.04	.02	.01	+	+	O
11	O	0	0	0	+	+	.01	.03	.06	.12	.20	.33	.50	.71	.94	1.1	1.2	1.3	1.2	1.1	.94	.71	.50	.33	.20	.12	.06	.03	+	O
12	O	0	0	0	.01	.02	.05	.12	.24	.46	.82	1.3	2.1	3.1	4.2	5.2	6.0	6.2	6.0	5.2	4.2	3.1	2.1	1.3	.82	.46	.24	.12	+	O
13	O	0	0	0	.03	.07	.16	.35	.73	1.4	2.6	4.5	7.4	11	16	20	23	24	23	20	16	11	7.4	4.5	2.6	1.4	.73	.35	+	O
14	O	0	0	0	.06	.15	.35	.78	1.6	3.3	6.4	12	20	31	45	60	73	77	73	60	45	31	20	12	6.4	3.3	1.6	.78	+	O
15	O	0	0	0	.09	.24	.56	1.2	2.8	5.8	11	21	38	63	100	149	201	226	201	149	100	63	38	21	11	5.8	2.8	1.2	+	O
16	O	0	0	0	.11	.28	.68	1.5	3.4	7.1	14	27	49	85	145	245	378	450	378	245	145	85	49	27	14	7.1	3.4	1.5	+	O
17	O	0	0	0	.10	.25	.60	1.3	2.9	6.2	12	23	41	69	111	170	235	266	235	170	111	69	41	23	12	6.2	2.9	1.3	+	O
18	O	0	0	0	.06	.16	.39	.87	1.8	3.8	7.3	13	23	36	53	72	88	94	88	72	53	36	23	13	7.3	3.8	1.8	.87	+	O
19	O	0	0	0	.03	.08	.19	.41	.86	1.7	3.1	5.5	9.0	14	19	25	29	30	29	25	19	14	9.0	5.5	3.1	1.7	.86	.41	+	O
20	O	0	0	0	.01	.03	.07	.15	.30	.58	1.0	1.7	2.7	4.0	5.4	6.8	7.8	8.1	7.8	6.8	5.4	4.0	2.7	1.7	1.0	.58	.30	.15	+	O
21	O	0	0	0	+	.01	.02	.04	.08	.15	.27	.44	.67	.95	1.2	1.5	1.7	1.8	1.7	1.5	1.2	.95	.67	.44	.27	.15	.08	.04	+	O
22	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
23	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
24	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
25	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
26	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
27	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
28	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
29	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
30	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
31	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
32	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
33	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
34	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
35	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
36	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
37	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
38	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
39	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
40	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
41	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
42	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
43	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
44	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O

BOTTOM ACCUMULATION OF SILT (CU FT/GRID SQUARE) , 900.00 SECONDS AFTER DUMP

...MULTIPLY DISPLAYED VALUES BY 1.000 (LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)

M N=	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31
2	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O
3	O	O	O	.	.	.	.	+	+	+	+	+	+	+	.01	.01	.01	.02	.02	.02	.01	.01	.01	+	+	+	+	+	+	+0
4	O	O	.	.	+	+	+	+	+	.01	.02	.04	.06	.08	.10	.12	.13	.13	.13	.12	.10	.08	.06	.04	.02	.01	+	+	+	+0
5	O	O	+	+	+	+	+	.01	.02	.04	.08	.13	.20	.29	.40	.50	.59	.65	.68	.65	.59	.50	.40	.29	.20	.13	.08	.04	.02	.01
6	O	O	+	+	+	.01	.02	.04	.09	.18	.31	.51	.78	1.1	1.5	1.9	2.2	2.4	2.5	2.4	2.2	1.9	1.5	1.1	.78	.51	.31	.18	.09	.04
7	O	O	+	+	.01	.03	.06	.14	.28	.53	.92	1.5	2.3	3.3	4.4	5.5	6.5	7.2	7.4	7.2	6.5	5.5	4.4	3.3	2.3	1.5	.92	.53	.28	.14
8	O	O	+	.01	.03	.07	.16	.33	.66	1.2	2.1	3.4	5.2	7.5	10	13	15	16	17	16	15	13	10	7.5	5.2	3.4	2.1	1.2	.66	.33
9	O	O	+	.02	.06	.14	.30	.63	1.2	2.2	3.9	6.3	10	14	18	23	27	30	31	30	27	23	18	14	10	6.3	3.9	2.2	1.2	.63
10	O	O	.01	.04	.10	.22	.49	.99	1.9	3.4	5.8	9.4	14	20	27	33	39	43	44	43	39	33	27	20	14	9.4	5.8	3.4	1.9	.99
11	O	O	.02	.06	.14	.32	.68	1.3	2.5	4.5	7.5	12	18	25	33	41	47	52	54	52	47	41	33	25	18	12	7.5	4.5	2.5	1.3
12	O	O	.03	.08	.20	.42	.86	1.6	3.0	5.2	8.6	13	20	27	35	44	51	55	57	55	51	44	35	27	20	13	8.6	5.2	3.0	1.6
13	O	O	.05	.11	.24	.51	1.0	1.9	3.3	5.7	9.2	14	20	28	36	43	50	55	56	55	50	43	36	28	20	14	9.2	5.7	3.3	1.9
14	O	O	.06	.13	.28	.57	1.1	2.0	3.5	5.8	9.2	14	20	26	34	41	47	51	52	51	47	41	34	26	20	14	9.2	5.8	3.5	2.0
15	O	O	.06	.14	.29	.58	1.1	1.9	3.4	5.5	8.5	13	18	24	30	36	41	44	45	44	41	36	30	24	18	13	8.5	5.5	3.4	1.9
16	O	O	.06	.13	.27	.54	1.0	1.7	2.9	4.8	7.3	11	15	20	25	29	33	36	37	36	33	29	25	20	15	11	7.3	4.8	2.9	1.7
17	O	O	.05	.11	.23	.44	.81	1.4	2.3	3.7	5.7	8.2	11	15	19	22	25	27	28	27	25	22	19	15	11	8.2	5.7	3.7	2.3	1.4
18	O	O	.03	.08	.16	.31	.57	.99	1.6	2.6	3.9	5.6	7.6	10	12	15	17	18	18	18	17	15	12	10	7.6	5.6	3.9	2.6	1.6	.99
19	O	O	.02	.05	.10	.19	.34	.59	.98	1.5	2.3	3.3	4.5	5.9	7.3	8.6	10	11	11	11	10	8.6	7.3	5.9	4.5	3.3	2.3	1.5	.98	.59
20	O	O	.01	.02	.05	.09	.17	.30	.50	.78	1.1	1.6	2.2	2.9	3.6	4.3	4.9	5.2	5.4	5.2	4.9	4.3	3.6	2.9	2.2	1.6	1.1	.78	.50	.30
21	O	O	+	.01	.02	.04	.07	.13	.21	.33	.50	.71	.97	1.2	1.5	1.8	2.0	2.2	2.2	2.2	2.0	1.8	1.5	1.2	.97	.71	.50	.33	.21	.13
22	O	O	+	+	+	.01	.02	.04	.07	.12	.17	.25	.34	.45	.55	.65	.74	.79	.81	.79	.74	.65	.55	.45	.34	.25	.17	.12	.07	.04
23	O	O	+	+	+	+	+	.01	.02	.03	.05	.07	.10	.13	.16	.19	.21	.23	.24	.23	.21	.19	.16	.13	.10	.07	.05	.03	.02	.01
24	O	O	+	+	+	+	+	+	+	+	.01	.01	.02	.03	.04	.04	.05	.05	.05	.05	.05	.04	.04	.03	.02	.01	.01	+	+	+0
25	O	O	.	.	+	+	+	+	+	+	+	+	+	+	+	.01	.01	.01	.01	.01	+	+	+	+	+	+	+	+	+	+0
26	O	O	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+0
27	O	O	0	.	.	.	.	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.0
28	O	O	0	0	0	0	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.0
29	O	O	0	0	0	0	0	0	0	0	0	.	.	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0	00
30	O	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00
31	O	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00
32	O	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00
33	O	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00
34	O	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00
35	O	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00
36	O	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00
37	O	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00
38	O	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00
39	O	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00
40	O	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00
41	O	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00
42	O	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00
43	O	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00
44	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O

SMALL CLOUDS AT 900.00 SECONDS ELAPSED TIME FOR SILT

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID	LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	753.3	450.0	73.00	0.0000E+00	96.88	5.816	113.8	0.447787E-03
2	754.0	450.0	64.14	0.0000E+00	117.6	36.35	83.65	0.229788E-03
3	754.4	450.0	88.56	0.0000E+00	155.1	76.33	43.67	0.356073E-03
4	754.6	450.0	111.9	0.0000E+00	235.4	90.07	29.93	0.247456E-03
5	754.6	450.0	48.45	0.0000E+00	296.0	104.5	15.52	0.115698E-03
6	754.6	450.0	22.69	0.0000E+00	333.5	97.61	22.39	0.562804E-04
7	754.5	450.0	13.18	0.0000E+00	358.6	67.68	52.32	0.340000E-04
8	754.3	450.0	9.244	0.0000E+00	377.8	63.06	56.94	0.340000E-04
9	754.1	450.0	7.247	0.0000E+00	393.9	61.35	58.65	0.340000E-04
10	753.8	450.0	221.6	0.0000E+00	407.8	119.6	0.4016	0.690000E-02

SUMMARY OF SILT DISTRIBUTIONS AFTER 1200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 437.89
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 5158.5

SUMMARY OF SILT DISTRIBUTIONS AFTER 1500.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 437.51
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 5158.9

SUMMARY OF SILT DISTRIBUTIONS AFTER 1800.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 437.23
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 5159.2

CONCENTRATIONS ABOVE BACKGROUND OF SILT (MG/L) IN THE CLOUD 1800.00 SECONDS AFTER DUMP

60.00 FT BELOW THE WATER SURFACE

...MULTIPLY DISPLAYED VALUES BY 1.000 (LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)

M N=	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31
2	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	0	+	+	+	+	+	+	+	+	+	.01	.01	.01	.01	.01	.02	.02	.02	.01	.01	.01	.01	.01	+	+	+	+	+	0	0
16	0	+	+	+	+	+	.01	.01	.02	.03	.04	.04	.05	.06	.07	.07	.07	.07	.07	.06	.05	.04	.04	.03	.02	.01	.01	+	0	0
17	0	+	+	.01	.01	.02	.04	.05	.07	.10	.13	.16	.19	.21	.23	.25	.25	.25	.23	.21	.19	.16	.13	.10	.07	.05	.04	.02	0	0
18	0	.01	.01	.03	.05	.07	.11	.16	.22	.29	.37	.45	.54	.62	.68	.72	.73	.72	.68	.62	.54	.45	.37	.29	.22	.16	.11	.07	0	0
19	0	.02	.04	.07	.12	.18	.27	.39	.54	.72	.92	1.1	1.3	1.5	1.6	1.7	1.8	1.7	1.6	1.5	1.3	1.1	.92	.72	.54	.39	.27	.18	0	0
20	0	.05	.09	.16	.25	.39	.58	.83	1.1	1.5	1.9	2.4	2.8	3.3	3.6	3.8	3.9	3.8	3.6	3.3	2.8	2.4	1.9	1.5	1.1	.83	.58	.39	0	0
21	0	.10	.17	.29	.46	.71	1.0	1.5	2.1	2.8	3.6	4.5	5.4	6.3	7.2	7.8	8.0	7.8	7.2	6.3	5.4	4.5	3.6	2.8	2.1	1.5	1.0	.71	0	0
22	0	.16	.27	.45	.73	1.1	1.6	2.4	3.3	4.5	5.9	7.7	10	14	19	23	25	23	19	14	10	7.7	5.9	4.5	3.3	2.4	1.6	1.1	0	0
23	0	.21	.37	.61	.99	1.5	2.2	3.3	4.6	6.3	9.0	14	25	45	76	106	120	106	76	45	25	14	9.0	6.3	4.6	3.3	2.2	1.5	0	0
24	0	.25	.43	.71	1.1	1.7	2.6	3.8	5.4	7.7	12	23	49	105	190	277	315	277	190	105	49	23	12	7.7	5.4	3.8	2.6	1.7	0	0
25	0	.25	.43	.71	1.1	1.7	2.6	3.8	5.4	7.7	12	22	49	103	186	271	308	271	186	103	49	22	12	7.7	5.4	3.8	2.6	1.7	0	0
26	0	.21	.37	.61	.99	1.5	2.2	3.3	4.6	6.3	8.9	14	24	43	72	101	113	101	72	43	24	14	8.9	6.3	4.6	3.3	2.2	1.5	0	0
27	0	.16	.27	.45	.73	1.1	1.6	2.4	3.3	4.5	5.9	7.7	10	14	18	22	24	22	18	14	10	7.7	5.9	4.5	3.3	2.4	1.6	1.1	0	0
28	0	.10	.17	.29	.46	.71	1.0	1.5	2.1	2.8	3.6	4.5	5.4	6.3	7.1	7.7	7.9	7.7	7.1	6.3	5.4	4.5	3.6	2.8	2.1	1.5	1.0	.71	0	0
29	0	.05	.09	.15	.25	.39	.58	.83	1.1	1.5	1.9	2.4	2.8	3.3	3.6	3.8	3.9	3.8	3.6	3.3	2.8	2.4	1.9	1.5	1.1	.83	.58	.39	0	0
30	0	.02	.04	.07	.12	.18	.27	.39	.53	.71	.91	1.1	1.3	1.5	1.6	1.7	1.8	1.7	1.6	1.5	1.3	1.1	.91	.71	.53	.39	.27	.18	0	0
31	0	.01	.01	.03	.04	.07	.11	.15	.21	.29	.37	.45	.53	.61	.67	.71	.72	.71	.67	.61	.53	.45	.37	.29	.21	.15	.11	.07	0	0
32	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
33	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
34	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
35	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
36	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
37	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
38	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
39	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
40	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
41	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
42	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
43	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
44	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O

CONCENTRATIONS ABOVE BACKGROUND OF SILT (MG/L) IN THE CLOUD 1800.00 SECONDS AFTER DUMP

119.00 FT BELOW THE WATER SURFACE

...MULTIPLY DISPLAYED VALUES BY 1.000 (LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)

M N=	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	0	0	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+
16	0	0	+	+	+	+	+	+	+	+	+	.01	.01	.01	.02	.02	.02	.02	.02	.02	.02	.01	.01	.01	+	+	+	+	+	+
17	0	0	+	+	+	+	+	+	.01	.01	.02	.03	.05	.06	.08	.09	.11	.11	.12	.11	.11	.09	.08	.06	.05	.03	.02	.01	.01	+
18	0	0	+	+	+	.01	.02	.04	.06	.10	.14	.20	.26	.33	.40	.46	.50	.51	.50	.46	.40	.33	.26	.20	.14	.10	.06	.04	.02	0
19	0	0	+	.01	.02	.04	.08	.13	.21	.33	.50	.70	.95	1.2	1.4	1.7	1.8	1.9	1.8	1.7	1.4	1.2	.95	.70	.50	.33	.21	.13	.08	0
20	0	0	.01	.03	.06	.12	.21	.37	.61	.98	1.4	2.1	2.9	3.8	4.7	5.5	6.0	6.2	6.0	5.5	4.7	3.8	2.9	2.1	1.4	.98	.61	.37	.21	0
21	0	0	.03	.07	.14	.27	.50	.87	1.4	2.4	3.7	5.5	7.8	10	13	16	17	18	17	16	13	10	7.8	5.5	3.7	2.4	1.4	.87	.50	0
22	0	0	.06	.13	.26	.51	.95	1.7	2.9	4.9	7.8	12	17	24	31	39	44	46	44	39	31	24	17	12	7.8	4.9	2.9	1.7	.95	0
23	0	0	.09	.20	.40	.78	1.4	2.7	4.7	8.0	13	21	31	46	64	83	98	104	98	83	64	46	31	21	13	8.0	4.7	2.7	1.4	0
24	0	0	.11	.24	.50	.98	1.8	3.4	6.0	10	17	28	44	67	98	134	164	176	164	134	98	67	44	28	17	10	6.0	3.4	1.8	0
25	0	0	.11	.24	.50	.98	1.8	3.4	6.0	10	17	28	44	67	98	133	163	175	163	133	98	67	44	28	17	10	6.0	3.4	1.8	0
26	0	0	.09	.20	.40	.78	1.4	2.7	4.7	8.0	13	21	31	46	63	82	97	103	97	82	63	46	31	21	13	8.0	4.7	2.7	1.4	0
27	0	0	.06	.13	.26	.51	.95	1.7	2.9	4.9	7.7	12	17	24	31	38	44	46	44	38	31	24	17	12	7.7	4.9	2.9	1.7	.95	0
28	0	0	.03	.07	.14	.27	.49	.87	1.4	2.4	3.7	5.5	7.7	10	13	16	17	18	17	16	13	10	7.7	5.5	3.7	2.4	1.4	.87	.49	0
29	0	0	.01	.03	.06	.12	.21	.37	.61	.97	1.4	2.1	2.9	3.8	4.7	5.5	6.0	6.2	6.0	5.5	4.7	3.8	2.9	2.1	1.4	.97	.61	.37	.21	0
30	0	0	+	.01	.02	.04	.08	.13	.21	.33	.49	.70	.95	1.2	1.4	1.7	1.8	1.9	1.8	1.7	1.4	1.2	.95	.70	.49	.33	.21	.13	.08	0
31	0	0	+	+	+	.01	.02	.04	.06	.10	.14	.20	.26	.33	.40	.46	.49	.51	.49	.46	.40	.33	.26	.20	.14	.10	.06	.04	.02	0
32	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
33	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
34	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
35	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
36	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
37	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
38	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
39	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
40	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
41	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
42	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
43	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
44	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0

BOTTOM ACCUMULATION OF SILT (CU FT/GRID SQUARE) , 1800.00 SECONDS AFTER DUMP

...MULTIPLY DISPLAYED VALUES BY 1.000 (LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)

M N=	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31
2	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O
3	O	O	O	.	.	.	.	+	+	+	+	+	+	+	.01	.01	.01	.02	.02	.02	.01	.01	.01	+	+	+	+	+	+	+0	O
4	O	O	O	.	.	+	+	+	+	+	.01	.02	.04	.06	.08	.10	.12	.13	.13	.13	.12	.10	.08	.06	.04	.02	.01	+	+	+0	O
5	O	O	O	+	+	+	+	+	.01	.02	.04	.08	.13	.20	.29	.40	.50	.59	.65	.68	.65	.59	.50	.40	.29	.20	.13	.08	.04	.02	.01	O
6	O	O	O	+	+	+	.01	.02	.04	.09	.18	.31	.51	.78	1.1	1.5	1.9	2.2	2.4	2.5	2.4	2.2	1.9	1.5	1.1	.78	.51	.31	.18	.09	.04	O
7	O	O	O	+	+	.01	.03	.06	.14	.28	.53	.92	1.5	2.3	3.3	4.4	5.5	6.5	7.2	7.4	7.2	6.5	5.5	4.4	3.3	2.3	1.5	.92	.53	.28	.14	O
8	O	O	O	+	.01	.03	.07	.16	.33	.66	1.2	2.1	3.4	5.2	7.5	10	13	15	16	17	16	15	13	10	7.5	5.2	3.4	2.1	1.2	.66	.33	O
9	O	O	O	+	.02	.06	.14	.30	.63	1.2	2.2	3.9	6.3	10	14	18	23	27	30	31	30	27	23	18	14	10	6.3	3.9	2.2	1.2	.63	O
10	O	O	O	.01	.04	.10	.22	.49	.99	1.9	3.4	5.8	9.4	14	20	27	33	39	43	44	43	39	33	27	20	14	9.4	5.8	3.4	1.9	.99	O
11	O	O	O	.02	.06	.14	.32	.68	1.3	2.5	4.5	7.5	12	18	25	33	41	47	52	54	52	47	41	33	25	18	12	7.5	4.5	2.5	1.3	O
12	O	O	O	.03	.09	.20	.42	.86	1.6	3.0	5.2	8.6	13	20	27	36	44	51	55	57	55	51	44	36	27	20	13	8.6	5.2	3.0	1.6	O
13	O	O	O	.05	.11	.25	.52	1.0	1.9	3.4	5.7	9.2	14	20	28	36	44	50	55	56	55	50	44	36	28	20	14	9.2	5.7	3.4	1.9	O
14	O	O	O	.06	.13	.29	.59	1.1	2.0	3.5	5.9	9.3	14	20	27	34	41	47	51	52	51	47	41	34	27	20	14	9.3	5.9	3.5	2.0	O
15	O	O	O	.07	.15	.31	.61	1.1	2.0	3.5	5.7	8.8	13	18	24	31	37	42	45	46	45	42	37	31	24	18	13	8.8	5.7	3.5	2.0	O
16	O	O	O	.07	.15	.30	.59	1.0	1.9	3.1	5.0	7.7	11	16	21	26	31	35	38	38	38	35	31	26	21	16	11	7.7	5.0	3.1	1.9	O
17	O	O	O	.06	.13	.27	.51	.92	1.6	2.6	4.1	6.2	9.0	12	16	20	24	27	29	30	29	27	24	20	16	12	9.0	6.2	4.1	2.6	1.6	O
18	O	O	O	.05	.11	.21	.40	.71	1.2	2.0	3.1	4.6	6.6	9.0	12	14	17	19	21	21	21	19	17	14	12	9.0	6.6	4.6	3.1	2.0	1.2	O
19	O	O	O	.04	.08	.15	.28	.50	.84	1.3	2.1	3.1	4.4	5.9	7.6	9.4	11	12	13	14	13	12	11	9.4	7.6	5.9	4.4	3.1	2.1	1.3	.84	O
20	O	O	O	.02	.05	.10	.18	.31	.53	.84	1.2	1.8	2.6	3.5	4.5	5.5	6.5	7.3	7.8	8.0	7.8	7.3	6.5	5.5	4.5	3.5	2.6	1.8	1.2	.84	.53	O
21	O	O	O	.01	.03	.06	.10	.18	.30	.47	.72	1.0	1.4	1.9	2.4	3.0	3.5	3.9	4.2	4.3	4.2	3.9	3.5	3.0	2.4	1.9	1.4	1.0	.72	.47	.30	O
22	O	O	O	+	.01	.03	.05	.09	.15	.24	.37	.53	.74	.98	1.2	1.5	1.7	1.9	2.0	2.1	2.0	1.9	1.7	1.5	1.2	.98	.74	.53	.37	.24	.15	O
23	O	O	O	+	+	.01	.02	.04	.07	.11	.17	.25	.34	.45	.57	.69	.80	.90	.96	.98	.96	.90	.80	.69	.57	.45	.34	.25	.17	.11	.07	O
24	O	O	O	+	+	+	.01	.02	.03	.05	.07	.10	.14	.19	.24	.29	.34	.38	.40	.41	.40	.38	.34	.29	.24	.19	.14	.10	.07	.05	.03	O
25	O	O	O	+	+	+	+	+	.01	.01	.02	.04	.05	.07	.09	.11	.13	.14	.15	.16	.15	.14	.13	.11	.09	.07	.05	.04	.02	.01	.01	O
26	O	O	O	+	+	+	+	+	+	+	+	.01	.01	.02	.03	.03	.04	.05	.05	.05	.05	.05	.04	.03	.03	.02	.01	.01	+	+	+0	O
27	O	O	O	.	+	+	+	+	+	+	+	+	+	.01	.01	.01	.01	.01	.01	.01	.01	.01	+	+	+	+	+	+	+	+0	O
28	O	O	O	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+0	O
29	O	O	O	.	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.0	O
30	O	O	0	.	.	.	.	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.0	O
31	O	O	0	0	0	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.0	O
32	O	O	0	0	0	0	0	0	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0	O
33	O	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.	.	.	0	0	0	0	0	0	0	0	0	0	0	O
34	O	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
35	O	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
36	O	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
37	O	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
38	O	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
39	O	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
40	O	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
41	O	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
42	O	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
43	O	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
44	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O

SMALL CLOUDS AT 1800.00 SECONDS ELAPSED TIME FOR SILT

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID	LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	1174.	450.0	72.93	0.0000E+00	161.8	4.771	115.2	0.844027E-04
2	1174.	450.0	64.07	0.0000E+00	186.4	35.28	84.72	0.744429E-04
3	1175.	450.0	88.24	0.0000E+00	230.0	75.33	44.67	0.124642E-03
4	1175.	450.0	111.4	0.0000E+00	320.4	89.03	30.97	0.110923E-03
5	1175.	450.0	48.24	0.0000E+00	387.4	99.89	20.11	0.618988E-04
6	1175.	450.0	22.67	0.0000E+00	428.4	25.22	94.78	0.340000E-04
7	1175.	450.0	13.17	0.0000E+00	455.7	0.0000E+00	120.0	0.340000E-04
8	1175.	450.0	9.240	0.0000E+00	476.5	0.0000E+00	120.0	0.340000E-04
9	1174.	450.0	7.244	0.0000E+00	493.8	0.0000E+00	120.0	0.340000E-04

SUMMARY OF SILT DISTRIBUTIONS AFTER 2100.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 437.02
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 5159.4

SUMMARY OF SILT DISTRIBUTIONS AFTER 2400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 436.87
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 5159.5

SUMMARY OF SILT DISTRIBUTIONS AFTER 2700.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 436.74
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 5159.7

CONCENTRATIONS ABOVE BACKGROUND OF SILT (MG/L) IN THE CLOUD 2700.00 SECONDS AFTER DUMP

60.00 FT BELOW THE WATER SURFACE

...MULTIPLY DISPLAYED VALUES BY 1.000 (LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)

M N=	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
18	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
19	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
20	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
21	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
22	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
23	+	+	+	.01	.01	.02	.02	.03	.04	.05	.06	.07	.08	.09	.10	.10	.10	.10	.10	.09	.08	.07	.06	.05	.04	.03	.02	.02	0	0
24	.01	.01	.02	.03	.04	.05	.07	.09	.12	.15	.17	.20	.23	.25	.27	.28	.29	.28	.27	.25	.23	.20	.17	.15	.12	.09	.07	.05	0	0
25	.02	.03	.05	.07	.10	.14	.18	.24	.30	.37	.44	.51	.58	.64	.68	.71	.72	.71	.68	.64	.58	.51	.44	.37	.30	.24	.18	.14	0	0
26	.05	.07	.11	.16	.23	.31	.41	.53	.67	.83	.99	1.1	1.3	1.4	1.5	1.6	1.6	1.6	1.5	1.4	1.3	1.1	.99	.83	.67	.53	.41	.31	0	0
27	.10	.15	.22	.32	.45	.62	.83	1.0	1.3	1.7	2.0	2.3	2.7	3.0	3.2	3.3	3.4	3.3	3.2	3.0	2.7	2.3	2.0	1.7	1.3	1.0	.83	.62	0	0
28	.18	.27	.40	.58	.82	1.1	1.5	1.9	2.5	3.1	3.8	4.5	5.2	5.8	6.3	6.6	6.8	6.6	6.3	5.8	5.2	4.5	3.8	3.1	2.5	1.9	1.5	1.10	0	0
29	.29	.44	.65	.95	1.3	1.8	2.5	3.3	4.2	5.4	6.7	8.1	10	11	13	14	14	14	13	11	10	8.1	6.7	5.4	4.2	3.3	2.5	1.80	0	0
30	.42	.64	.95	1.3	1.9	2.7	3.7	5.0	6.6	8.7	12	15	20	25	30	34	35	34	30	25	20	15	12	8.7	6.6	5.0	3.7	2.70	0	0
31	.54	.83	1.2	1.8	2.6	3.6	5.0	6.8	9.4	13	19	28	40	55	70	81	85	81	70	55	40	28	19	13	9.4	6.8	5.0	3.60	0	0
32	.63	.97	1.4	2.1	3.0	4.3	6.0	8.4	12	18	28	44	67	95	123	145	154	145	123	95	67	44	28	18	12	8.4	6.0	4.30	0	0
33	.66	1.0	1.5	2.2	3.2	4.5	6.3	9.0	13	20	32	51	78	112	146	173	183	173	146	112	78	51	32	20	13	9.0	6.3	4.50	0	0
34	.62	.95	1.4	2.0	3.0	4.2	5.8	8.2	12	17	26	41	61	86	112	132	139	132	112	86	61	41	26	17	12	8.2	5.8	4.20	0	0
35	.52	.80	1.2	1.7	2.5	3.4	4.7	6.5	8.8	12	17	25	35	47	59	68	71	68	59	47	35	25	17	12	8.8	6.5	4.7	3.40	0	0
36	.39	.60	.90	1.3	1.8	2.5	3.5	4.6	6.1	7.9	10	13	17	21	25	28	29	28	25	21	17	13	10	7.9	6.1	4.6	3.5	2.50	0	0
37	.26	.40	.60	.87	1.2	1.7	2.3	3.0	3.9	4.9	6.0	7.2	8.6	10	11	12	12	12	11	10	8.6	7.2	6.0	4.9	3.9	3.0	2.3	1.70	0	0
38	.16	.24	.36	.53	.74	1.0	1.3	1.7	2.2	2.8	3.4	4.0	4.6	5.1	5.5	5.8	5.9	5.8	5.5	5.1	4.6	4.0	3.4	2.8	2.2	1.7	1.3	1.00	0	0
39	.09	.13	.20	.28	.40	.55	.73	.96	1.2	1.5	1.8	2.1	2.3	2.6	2.8	2.9	3.0	2.9	2.8	2.6	2.3	2.1	1.8	1.5	1.2	.96	.73	.550	0	0
40	.04	.06	.10	.14	.19	.27	.36	.46	.58	.72	.86	1.0	1.1	1.2	1.3	1.4	1.4	1.4	1.3	1.2	1.1	1.0	.86	.72	.58	.46	.36	.270	0	0
41	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
42	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
43	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
44	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0

CONCENTRATIONS ABOVE BACKGROUND OF SILT (MG/L) IN THE CLOUD 2700.00 SECONDS AFTER DUMP

119.00 FT BELOW THE WATER SURFACE

...MULTIPLY DISPLAYED VALUES BY 1.000 (LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)

M N=	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
18	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
19	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
20	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
21	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
22	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
23	+	+	+	+	+	+	+	+	+	.01	.01	.01	.01	.01	.01	.02	.02	.02	.01	.01	.01	.01	.01	.01	+	+	+	+	0	0
24	+	+	+	+	+	.01	.01	.01	.02	.03	.03	.04	.05	.05	.06	.06	.06	.06	.06	.05	.05	.04	.03	.03	.02	.01	.01	.01	0	0
25	+	+	+	.01	.02	.02	.04	.05	.07	.09	.11	.14	.16	.18	.20	.21	.21	.21	.20	.18	.16	.14	.11	.09	.07	.05	.04	.02	0	0
26	0	+	.01	.02	.03	.05	.07	.10	.14	.20	.26	.33	.41	.49	.56	.61	.65	.66	.65	.61	.56	.49	.41	.33	.26	.20	.14	.10	.07	0
27	0	.01	.03	.05	.07	.12	.18	.26	.37	.52	.70	.90	1.1	1.3	1.5	1.7	1.8	1.9	1.8	1.7	1.5	1.3	1.1	.90	.70	.52	.37	.26	.18	0
28	0	.03	.06	.10	.16	.26	.40	.60	.87	1.2	1.6	2.2	2.8	3.4	4.0	4.5	4.8	4.9	4.8	4.5	4.0	3.4	2.8	2.2	1.6	1.2	.87	.60	.40	0
29	0	.06	.11	.19	.31	.50	.79	1.2	1.8	2.6	3.6	4.8	6.3	7.8	9.4	11	12	12	12	11	9.4	7.8	6.3	4.8	3.6	2.6	1.8	1.2	.79	0
30	0	.10	.18	.31	.53	.86	1.3	2.1	3.2	4.8	6.8	9.4	13	16	20	23	25	26	25	23	20	16	13	9.4	6.8	4.8	3.2	2.1	1.3	0
31	0	.15	.26	.45	.77	1.2	2.0	3.2	5.0	7.6	11	16	22	28	35	42	46	48	46	42	35	28	22	16	11	7.6	5.0	3.2	2.0	0
32	0	.18	.32	.56	.96	1.6	2.6	4.2	6.6	10	15	22	30	41	52	62	69	72	69	62	52	41	30	22	15	10	6.6	4.2	2.6	0
33	0	.19	.34	.60	1.0	1.7	2.8	4.5	7.1	11	16	24	33	45	58	69	78	81	78	69	58	45	33	24	16	11	7.1	4.5	2.8	0
34	0	.18	.31	.55	.93	1.5	2.5	4.0	6.3	10	14	21	29	38	49	58	65	67	65	58	49	38	29	21	14	10	6.3	4.0	2.5	0
35	0	.14	.25	.43	.72	1.2	1.9	3.0	4.7	7.0	10	14	20	26	32	37	41	43	41	37	32	26	20	14	10	7.0	4.7	3.0	1.9	0
36	0	.10	.17	.29	.48	.79	1.2	1.9	2.9	4.3	6.1	8.4	11	14	17	20	22	22	22	20	17	14	11	8.4	6.1	4.3	2.9	1.9	1.2	0
37	0	.06	.10	.17	.28	.45	.70	1.0	1.5	2.2	3.1	4.2	5.4	6.7	8.0	9.1	10	10	10	9.1	8.0	6.7	5.4	4.2	3.1	2.2	1.5	1.0	.70	0
38	0	.03	.05	.09	.14	.22	.34	.51	.75	1.0	1.4	1.8	2.3	2.9	3.4	3.8	4.0	4.1	4.0	3.8	3.4	2.9	2.3	1.8	1.4	1.0	.75	.51	.34	0
39	0	.01	.02	.04	.06	.10	.15	.22	.31	.43	.58	.75	.94	1.1	1.3	1.4	1.5	1.5	1.5	1.4	1.3	1.1	.94	.75	.58	.43	.31	.22	.15	0
40	0	+	.01	.01	.02	.04	.06	.08	.12	.16	.21	.27	.33	.40	.45	.50	.53	.54	.53	.50	.45	.40	.33	.27	.21	.16	.12	.08	.06	0
41	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
42	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
43	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
44	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0

BOTTOM ACCUMULATION OF SILT (CU FT/GRID SQUARE) , 2700.00 SECONDS AFTER DUMP

...MULTIPLY DISPLAYED VALUES BY 1.000 (LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)

M N=	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31
2	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O
3	O	O	O	O	.	.	.	.	+	+	+	+	+	+	+	+	.01	.01	.01	.02	.02	.02	.01	.01	.01	+	+	+	+	+	+	+0000
4	O	O	O	.	.	+	+	+	+	+	+	+	.01	.02	.04	.06	.08	.10	.12	.13	.13	.13	.12	.10	.08	.06	.04	.02	.01	+	+	+0000
5	O	O	O	+	+	+	+	+	.01	.02	.04	.08	.13	.20	.29	.40	.50	.59	.65	.68	.65	.59	.50	.40	.29	.20	.13	.08	.04	.02	.010000
6	O	O	O	+	+	+	.01	.02	.04	.09	.18	.31	.51	.78	1.1	1.5	1.9	2.2	2.4	2.5	2.4	2.2	1.9	1.5	1.1	.78	.51	.31	.18	.09	.040000
7	O	O	O	+	+	.01	.03	.06	.14	.28	.53	.92	1.5	2.3	3.3	4.4	5.5	6.5	7.2	7.4	7.2	6.5	5.5	4.4	3.3	2.3	1.5	.92	.53	.28	.140000
8	O	O	O	+	.01	.03	.07	.16	.33	.66	1.2	2.1	3.4	5.2	7.5	10	13	15	16	17	16	15	13	10	7.5	5.2	3.4	2.1	1.2	.66	.330000
9	O	O	O	+	.02	.06	.14	.30	.63	1.2	2.2	3.9	6.3	10	14	18	23	27	30	31	30	27	23	18	14	10	6.3	3.9	2.2	1.2	.630000
10	O	O	O	.01	.04	.10	.22	.49	.99	1.9	3.4	5.8	9.4	14	20	27	33	39	43	44	43	39	33	27	20	14	9.4	5.8	3.4	1.9	.990000
11	O	O	O	.02	.06	.14	.32	.68	1.3	2.5	4.5	7.5	12	18	25	33	41	47	52	54	52	47	41	33	25	18	12	7.5	4.5	2.5	1.30000
12	O	O	O	.03	.09	.20	.42	.86	1.6	3.0	5.2	8.6	13	20	27	36	44	51	55	57	55	51	44	36	27	20	13	8.6	5.2	3.0	1.60000
13	O	O	O	.05	.11	.25	.52	1.0	1.9	3.4	5.7	9.2	14	20	28	36	44	50	55	56	55	50	44	36	28	20	14	9.2	5.7	3.4	1.90000
14	O	O	O	.06	.13	.29	.59	1.1	2.0	3.5	5.9	9.3	14	20	27	34	41	47	51	52	51	47	41	34	27	20	14	9.3	5.9	3.5	2.00000
15	O	O	O	.07	.15	.31	.61	1.1	2.0	3.5	5.7	8.8	13	18	24	31	37	42	45	46	45	42	37	31	24	18	13	8.8	5.7	3.5	2.00000
16	O	O	O	.07	.15	.30	.59	1.0	1.9	3.1	5.0	7.7	11	16	21	26	31	35	38	38	38	35	31	26	21	16	11	7.7	5.0	3.1	1.90000
17	O	O	O	.06	.13	.27	.51	.92	1.6	2.6	4.1	6.2	9.0	12	16	20	24	27	29	30	29	27	24	20	16	12	9.0	6.2	4.1	2.6	1.60000
18	O	O	O	.05	.11	.21	.40	.71	1.2	2.0	3.1	4.6	6.6	9.0	12	14	17	19	21	21	21	19	17	14	12	9.0	6.6	4.6	3.1	2.0	1.20000
19	O	O	O	.04	.08	.15	.28	.50	.84	1.3	2.1	3.1	4.4	5.9	7.6	9.4	11	12	13	14	13	12	11	9.4	7.6	5.9	4.4	3.1	2.1	1.3	.840000
20	O	O	O	.02	.05	.10	.18	.31	.53	.84	1.2	1.8	2.6	3.5	4.5	5.5	6.5	7.3	7.8	8.0	7.8	7.3	6.5	5.5	4.5	3.5	2.6	1.8	1.2	.84	.530000
21	O	O	O	.01	.03	.06	.10	.18	.30	.47	.72	1.0	1.4	1.9	2.4	3.0	3.5	3.9	4.2	4.3	4.2	3.9	3.5	3.0	2.4	1.9	1.4	1.0	.72	.47	.300000
22	O	O	+	.01	.03	.05	.09	.15	.24	.37	.53	.74	.98	1.2	1.5	1.7	1.9	2.0	2.1	2.0	1.9	1.7	1.5	1.2	.98	.74	.53	.37	.24	.150000
23	O	O	+	+	.01	.02	.04	.07	.11	.17	.25	.34	.45	.57	.69	.80	.90	.96	.98	.96	.90	.80	.69	.57	.45	.34	.25	.17	.11	.070000
24	O	O	+	+	+	.01	.02	.03	.05	.07	.10	.14	.19	.24	.29	.34	.38	.40	.41	.40	.38	.34	.29	.24	.19	.14	.10	.07	.05	.030000
25	O	O	+	+	+	+	.01	.01	.02	.04	.05	.07	.09	.11	.13	.14	.15	.16	.15	.14	.13	.11	.09	.07	.05	.04	.02	.01	.010000
26	O	O	+	+	+	+	+	+	+	.01	.01	.02	.03	.04	.04	.05	.05	.05	.05	.05	.04	.04	.03	.02	.01	.01	+	+	+0000
27	O	O	.	+	+	+	+	+	+	+	+	+	.01	.01	.01	.02	.02	.02	.02	.02	.01	.01	.01	+	+	+	+	+	+0000
28	O	O	.	.	.	+	+	+	+	+	+	+	+	+	+	+	.01	.01	.01	+	+	+	+	+	+	+	+	+	+0000
29	O	O	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+0000
30	O	O	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+0000
31	O	O	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+0000
32	O	O	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+0000
33	O	O	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+0000
34	O	O	.	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.0000
35	O	O	.	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.0000
36	O	O	.	.	.	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.0000
37	O	O	.	.	.	.	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.0000
38	O	0	.	.	.	.	.	.	.	.	.	.	.	.	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.0000
39	O	0	0	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.0000
40	O	0	0	0	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.0000
41	O	0	0	0	0	0	0	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	0	00000
42	O	0	0	0	0	0	0	0	0	0	0	0	.	.	.	.	.	.	.	.	.	.	0	0	0	0	0	0	00000
43	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
44	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O

SMALL CLOUDS AT 2700.00 SECONDS ELAPSED TIME FOR SILT

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID	LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	1594.	450.0	72.90	0.0000E+00	237.6	0.0000E+00	120.0	0.415773E-04
2	1595.	450.0	64.04	0.0000E+00	265.5	0.0000E+00	120.0	0.351531E-04
3	1595.	450.0	88.10	0.0000E+00	314.4	70.74	49.26	0.628029E-04
4	1595.	450.0	111.2	0.0000E+00	414.1	87.94	32.06	0.632610E-04
5	1595.	450.0	48.20	0.0000E+00	486.9	37.05	82.95	0.340000E-04
6	1595.	450.0	22.67	0.0000E+00	531.1	0.0000E+00	120.0	0.340000E-04
7	1595.	450.0	13.17	0.0000E+00	560.4	0.0000E+00	120.0	0.340000E-04
8	1595.	450.0	9.238	0.0000E+00	582.7	0.0000E+00	120.0	0.340000E-04
9	1595.	450.0	7.243	0.0000E+00	601.3	0.0000E+00	120.0	0.340000E-04

SUMMARY OF SILT DISTRIBUTIONS AFTER 3000.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 436.65
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 5159.8

SUMMARY OF SILT DISTRIBUTIONS AFTER 3300.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 436.59
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 5159.8

SUMMARY OF SILT DISTRIBUTIONS AFTER 3600.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 436.54
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 5159.9

CONCENTRATIONS ABOVE BACKGROUND OF SILT (MG/L) IN THE CLOUD 3600.00 SECONDS AFTER DUMP

60.00 FT BELOW THE WATER SURFACE

...MULTIPLY DISPLAYED VALUES BY 1.000 (LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)

M	N=	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
15	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
16	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
17	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
18	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
19	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
20	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
21	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
22	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
23	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
24	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
25	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
26	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
27	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
28	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
29	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
30	0	.01	.01	.02	.02	.03	.04	.05	.06	.07	.08	.09	.11	.12	.12	.13	.13	.14	.13	.13	.12	.12	.11	.09	.08	.07	.06	.05	.040000		
31	0	.02	.03	.04	.06	.08	.10	.12	.14	.17	.20	.23	.26	.28	.30	.32	.33	.33	.33	.32	.30	.28	.26	.23	.20	.17	.14	.12	.100000		
32	0	.05	.07	.10	.13	.17	.21	.27	.32	.39	.45	.52	.59	.65	.70	.74	.76	.77	.76	.74	.70	.65	.59	.52	.45	.39	.32	.27	.210000		
33	0	.11	.15	.20	.27	.35	.45	.56	.69	.83	.98	1.1	1.2	1.4	1.5	1.6	1.6	1.7	1.6	1.6	1.5	1.4	1.2	1.1	.98	.83	.69	.56	.450000		
34	0	.21	.29	.39	.52	.68	.88	1.1	1.3	1.6	2.0	2.3	2.6	2.9	3.2	3.4	3.6	3.6	3.6	3.4	3.2	2.9	2.6	2.3	2.0	1.6	1.3	1.1	.880000		
35	0	.37	.51	.70	.94	1.2	1.6	2.0	2.6	3.2	3.9	4.6	5.3	6.1	6.7	7.2	7.5	7.6	7.5	7.2	6.7	6.1	5.3	4.6	3.9	3.2	2.6	2.0	1.60000		
36	0	.61	.85	1.1	1.6	2.1	2.8	3.7	4.7	5.9	7.3	8.9	11	12	14	15	15	16	15	15	14	12	11	8.9	7.3	5.9	4.7	3.7	2.80000		
37	0	.92	1.3	1.8	2.5	3.4	4.6	6.1	8.1	10	13	16	20	23	27	29	31	32	31	29	27	23	20	16	13	10	8.1	6.1	4.60000		
38	0	1.3	1.8	2.6	3.7	5.1	7.0	10	13	17	22	28	35	42	49	55	58	60	58	55	49	42	35	28	22	17	13	10	7.00000		
39	0	1.6	2.4	3.5	4.9	7.0	10	14	19	26	34	44	56	69	81	91	98	101	98	91	81	69	56	44	34	26	19	14	100000		
40	0	2.0	2.9	4.2	6.0	8.6	12	17	24	34	46	61	78	97	115	130	141	145	141	130	115	97	78	61	46	34	24	17	120000		
41	0	2.1	3.1	4.5	6.6	10	14	19	27	38	53	70	91	113	135	154	166	171	166	154	135	113	91	70	53	38	27	19	140000		
42	0	2.1	3.1	4.5	6.4	9.3	13	19	27	37	51	68	88	109	130	148	160	164	160	148	130	109	88	68	51	37	27	19	130000		
43	0	1.9	2.7	3.9	5.6	8.0	11	16	22	31	42	55	70	86	102	116	125	128	125	116	102	86	70	55	42	31	22	16	110000		
44	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0

CONCENTRATIONS ABOVE BACKGROUND OF SILT (MG/L) IN THE CLOUD 3600.00 SECONDS AFTER DUMP

119.00 FT BELOW THE WATER SURFACE

...MULTIPLY DISPLAYED VALUES BY 1.000 (LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)

M N=	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
18	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
19	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
20	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
21	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
22	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
23	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
24	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
25	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
26	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
27	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
28	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
29	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
30	0	+	+	+	+	+	+	+	.01	.01	.01	.01	.01	.01	.02	.02	.02	.02	.02	.01	.01	.01	.01	.01	.01	+	+	+0	0	0
31	0	+	+	+	.01	.01	.01	.02	.02	.03	.03	.04	.04	.04	.05	.05	.05	.05	.05	.04	.04	.04	.03	.03	.02	.02	.01	.01	0	0
32	0	+	.01	.01	.02	.02	.03	.04	.05	.06	.07	.08	.09	.10	.11	.12	.12	.12	.12	.12	.11	.10	.09	.08	.07	.06	.05	.04	.03	0
33	0	.01	.02	.03	.04	.05	.07	.09	.11	.13	.16	.18	.21	.23	.25	.27	.28	.28	.28	.27	.25	.23	.21	.18	.16	.13	.11	.09	.07	0
34	0	.03	.04	.06	.08	.11	.14	.18	.22	.28	.33	.39	.45	.51	.56	.59	.62	.63	.62	.59	.56	.51	.45	.39	.33	.28	.22	.18	.14	0
35	0	.05	.08	.11	.15	.20	.27	.35	.44	.55	.67	.80	.93	1.0	1.1	1.2	1.3	1.3	1.3	1.2	1.1	1.0	.93	.80	.67	.55	.44	.35	.27	0
36	0	.09	.13	.19	.26	.36	.48	.63	.82	1.0	1.2	1.5	1.8	2.1	2.3	2.5	2.6	2.7	2.6	2.5	2.3	2.1	1.8	1.5	1.2	1.0	.82	.63	.48	0
37	0	.15	.21	.30	.43	.59	.80	1.0	1.4	1.8	2.3	2.8	3.4	4.0	4.5	5.0	5.2	5.3	5.2	5.0	4.5	4.0	3.4	2.8	2.3	1.8	1.4	1.0	.80	0
38	0	.21	.31	.45	.63	.89	1.2	1.6	2.2	2.9	3.8	4.8	5.9	7.1	8.2	9.1	10	10	10	9.1	8.2	7.1	5.9	4.8	3.8	2.9	2.2	1.6	1.2	0
39	0	.28	.41	.60	.86	1.2	1.7	2.3	3.2	4.3	5.8	7.5	9.4	11	13	15	16	16	16	15	13	11	9.4	7.5	5.8	4.3	3.2	2.3	1.7	0
40	0	.33	.49	.72	1.0	1.5	2.1	3.0	4.1	5.7	7.7	10	13	16	19	21	23	23	23	21	19	16	13	10	7.7	5.7	4.1	3.0	2.1	0
41	0	.36	.54	.79	1.1	1.6	2.3	3.3	4.7	6.5	8.8	12	15	18	22	25	27	27	27	25	22	18	15	12	8.8	6.5	4.7	3.3	2.3	0
42	0	.36	.53	.77	1.1	1.6	2.3	3.2	4.5	6.3	8.5	11	14	18	21	24	26	26	26	24	21	18	14	11	8.5	6.3	4.5	3.2	2.3	0
43	0	.32	.47	.68	.98	1.4	1.9	2.7	3.8	5.2	7.0	9.1	12	14	17	19	20	21	20	19	17	14	12	9.1	7.0	5.2	3.8	2.7	1.9	0
44	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0

BOTTOM ACCUMULATION OF SILT (CU FT/GRID SQUARE) , 3600.00 SECONDS AFTER DUMP

...MULTIPLY DISPLAYED VALUES BY 1.000 (LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)

M N=	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31
2	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O
3	O	O	O	O	.	.	.	.	+	+	+	+	+	+	+	+	.01	.01	.01	.02	.02	.02	.01	.01	.01	+	+	+	+	+	+	+0
4	O	O	O	.	.	+	+	+	+	+	+	.01	.02	.04	.06	.08	.10	.12	.13	.13	.13	.12	.10	.08	.06	.04	.02	.01	+	+	+0
5	O	O	O	+	+	+	+	+	.01	.02	.04	.08	.13	.20	.29	.40	.50	.59	.65	.68	.65	.59	.50	.40	.29	.20	.13	.08	.04	.02	.01	0
6	O	O	O	+	+	+	.01	.02	.04	.09	.18	.31	.51	.78	1.1	1.5	1.9	2.2	2.4	2.5	2.4	2.2	1.9	1.5	1.1	.78	.51	.31	.18	.09	.04	0
7	O	O	O	+	+	.01	.03	.06	.14	.28	.53	.92	1.5	2.3	3.3	4.4	5.5	6.5	7.2	7.4	7.2	6.5	5.5	4.4	3.3	2.3	1.5	.92	.53	.28	.14	0
8	O	O	O	+	.01	.03	.07	.16	.33	.66	1.2	2.1	3.4	5.2	7.5	10	13	15	16	17	16	15	13	10	7.5	5.2	3.4	2.1	1.2	.66	.33	0
9	O	O	O	+	.02	.06	.14	.30	.63	1.2	2.2	3.9	6.3	10	14	18	23	27	30	31	30	27	23	18	14	10	6.3	3.9	2.2	1.2	.63	0
10	O	O	O	.01	.04	.10	.22	.49	.99	1.9	3.4	5.8	9.4	14	20	27	33	39	43	44	43	39	33	27	20	14	9.4	5.8	3.4	1.9	.99	0
11	O	O	O	.02	.06	.14	.32	.68	1.3	2.5	4.5	7.5	12	18	25	33	41	47	52	54	52	47	41	33	25	18	12	7.5	4.5	2.5	1.3	0
12	O	O	O	.03	.09	.20	.42	.86	1.6	3.0	5.2	8.6	13	20	27	36	44	51	55	57	55	51	44	36	27	20	13	8.6	5.2	3.0	1.6	0
13	O	O	O	.05	.11	.25	.52	1.0	1.9	3.4	5.7	9.2	14	20	28	36	44	50	55	56	55	50	44	36	28	20	14	9.2	5.7	3.4	1.9	0
14	O	O	O	.06	.13	.29	.59	1.1	2.0	3.5	5.9	9.3	14	20	27	34	41	47	51	52	51	47	41	34	27	20	14	9.3	5.9	3.5	2.0	0
15	O	O	O	.07	.15	.31	.61	1.1	2.0	3.5	5.7	8.8	13	18	24	31	37	42	45	46	45	42	37	31	24	18	13	8.8	5.7	3.5	2.0	0
16	O	O	O	.07	.15	.30	.59	1.0	1.9	3.1	5.0	7.7	11	16	21	26	31	35	38	38	38	35	31	26	21	16	11	7.7	5.0	3.1	1.9	0
17	O	O	O	.06	.13	.27	.51	.92	1.6	2.6	4.1	6.2	9.0	12	16	20	24	27	29	30	29	27	24	20	16	12	9.0	6.2	4.1	2.6	1.6	0
18	O	O	O	.05	.11	.21	.40	.71	1.2	2.0	3.1	4.6	6.6	9.0	12	14	17	19	21	21	21	19	17	14	12	9.0	6.6	4.6	3.1	2.0	1.2	0
19	O	O	O	.04	.08	.15	.28	.50	.84	1.3	2.1	3.1	4.4	5.9	7.6	9.4	11	12	13	14	13	12	11	9.4	7.6	5.9	4.4	3.1	2.1	1.3	.840	0
20	O	O	O	.02	.05	.10	.18	.31	.53	.84	1.2	1.8	2.6	3.5	4.5	5.5	6.5	7.3	7.8	8.0	7.8	7.3	6.5	5.5	4.5	3.5	2.6	1.8	1.2	.84	.530	0
21	O	O	O	.01	.03	.06	.10	.18	.30	.47	.72	1.0	1.4	1.9	2.4	3.0	3.5	3.9	4.2	4.3	4.2	3.9	3.5	3.0	2.4	1.9	1.4	1.0	.72	.47	.300	0
22	O	O	O	+	.01	.03	.05	.09	.15	.24	.37	.53	.74	.98	1.2	1.5	1.7	1.9	2.0	2.1	2.0	1.9	1.7	1.5	1.2	.98	.74	.53	.37	.24	.150	0
23	O	O	O	+	+	.01	.02	.04	.07	.11	.17	.25	.34	.45	.57	.69	.80	.90	.96	.98	.96	.90	.80	.69	.57	.45	.34	.25	.17	.11	.070	0
24	O	O	O	+	+	+	.01	.02	.03	.05	.07	.10	.14	.19	.24	.29	.34	.38	.40	.41	.40	.38	.34	.29	.24	.19	.14	.10	.07	.05	.030	0
25	O	O	O	+	+	+	+	.01	.01	.02	.04	.05	.07	.09	.11	.13	.14	.15	.16	.15	.14	.13	.11	.09	.07	.05	.04	.02	.01	.010	0
26	O	O	O	+	+	+	+	+	+	.01	.01	.02	.03	.04	.04	.05	.05	.05	.05	.05	.04	.04	.03	.02	.01	.01	+	+	+0	0
27	O	O	O	.	+	+	+	+	+	+	+	+	.01	.01	.01	.02	.02	.02	.02	.02	.01	.01	.01	+	+	+	+	+	+0	0
28	O	O	O	.	.	.	+	+	+	+	+	+	+	+	+	+	.01	.01	.01	+	+	+	+	+	+	+	+	+	+0	0
29	O	O	O	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+0	0
30	O	O	O	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+0	0
31	O	O	O	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+0	0
32	O	O	O	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+0	0
33	O	O	O	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+0	0
34	O	O	O	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+0	0
35	O	O	O	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+0	0
36	O	O	O	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+0	0
37	O	O	O	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+0	0
38	O	O	O	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+0	0
39	O	O	O	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+0	0
40	O	O	O	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+0	0
41	O	O	O	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+0	0
42	O	O	O	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.0	0
43	O	O	O	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.0	0
44	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O

SMALL CLOUDS AT 3600.00 SECONDS ELAPSED TIME FOR SILT

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID	LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	2014.	450.0	72.88	0.0000E+00	322.9	0.0000E+00	120.0	0.340000E-04
2	2015.	450.0	64.02	0.0000E+00	353.9	0.0000E+00	120.0	0.340000E-04
3	2015.	450.0	88.06	0.0000E+00	407.5	15.08	104.9	0.340000E-04
4	2016.	450.0	111.1	0.0000E+00	515.6	37.77	82.23	0.340000E-04
5	2016.	450.0	48.19	0.0000E+00	593.8	0.0000E+00	120.0	0.340000E-04
6	2016.	450.0	22.66	0.0000E+00	641.0	0.0000E+00	120.0	0.340000E-04
7	2016.	450.0	13.16	0.0000E+00	672.2	0.0000E+00	120.0	0.340000E-04
8	2015.	450.0	9.236	0.0000E+00	695.9	0.0000E+00	120.0	0.340000E-04
9	2015.	450.0	7.241	0.0000E+00	715.7	0.0000E+00	120.0	0.340000E-04

BOTTOM ACCUMULATION OF SILT (CU FT/GRID SQUARE) , 3600.00 SECONDS AFTER DUMP

...MULTIPLY DISPLAYED VALUES BY 1.000 (LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)

M N=	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31
2	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O
3	O	O	O	O	.	.	.	.	+	+	+	+	+	+	+	+	.01	.01	.01	.02	.02	.02	.01	.01	.01	+	+	+	+	+	+	+0
4	O	O	O	.	.	+	+	+	+	+	+	.01	.02	.04	.06	.08	.10	.12	.13	.13	.13	.12	.10	.08	.06	.04	.02	.01	+	+	+0
5	O	O	O	+	+	+	+	+	.01	.02	.04	.08	.13	.20	.29	.40	.50	.59	.65	.68	.65	.59	.50	.40	.29	.20	.13	.08	.04	.02	.01	0
6	O	O	O	+	+	+	.01	.02	.04	.09	.18	.31	.51	.78	1.1	1.5	1.9	2.2	2.4	2.5	2.4	2.2	1.9	1.5	1.1	.78	.51	.31	.18	.09	.04	0
7	O	O	O	+	+	.01	.03	.06	.14	.28	.53	.92	1.5	2.3	3.3	4.4	5.5	6.5	7.2	7.4	7.2	6.5	5.5	4.4	3.3	2.3	1.5	.92	.53	.28	.14	0
8	O	O	O	+	.01	.03	.07	.16	.33	.66	1.2	2.1	3.4	5.2	7.5	10	13	15	16	17	16	15	13	10	7.5	5.2	3.4	2.1	1.2	.66	.33	0
9	O	O	O	+	.02	.06	.14	.30	.63	1.2	2.2	3.9	6.3	10	14	18	23	27	30	31	30	27	23	18	14	10	6.3	3.9	2.2	1.2	.63	0
10	O	O	O	.01	.04	.10	.22	.49	.99	1.9	3.4	5.8	9.4	14	20	27	33	39	43	44	43	39	33	27	20	14	9.4	5.8	3.4	1.9	.99	0
11	O	O	O	.02	.06	.14	.32	.68	1.3	2.5	4.5	7.5	12	18	25	33	41	47	52	54	52	47	41	33	25	18	12	7.5	4.5	2.5	1.3	0
12	O	O	O	.03	.09	.20	.42	.86	1.6	3.0	5.2	8.6	13	20	27	36	44	51	55	57	55	51	44	36	27	20	13	8.6	5.2	3.0	1.6	0
13	O	O	O	.05	.11	.25	.52	1.0	1.9	3.4	5.7	9.2	14	20	28	36	44	50	55	56	55	50	44	36	28	20	14	9.2	5.7	3.4	1.9	0
14	O	O	O	.06	.13	.29	.59	1.1	2.0	3.5	5.9	9.3	14	20	27	34	41	47	51	52	51	47	41	34	27	20	14	9.3	5.9	3.5	2.0	0
15	O	O	O	.07	.15	.31	.61	1.1	2.0	3.5	5.7	8.8	13	18	24	31	37	42	45	46	45	42	37	31	24	18	13	8.8	5.7	3.5	2.0	0
16	O	O	O	.07	.15	.30	.59	1.0	1.9	3.1	5.0	7.7	11	16	21	26	31	35	38	38	38	35	31	26	21	16	11	7.7	5.0	3.1	1.9	0
17	O	O	O	.06	.13	.27	.51	.92	1.6	2.6	4.1	6.2	9.0	12	16	20	24	27	29	30	29	27	24	20	16	12	9.0	6.2	4.1	2.6	1.6	0
18	O	O	O	.05	.11	.21	.40	.71	1.2	2.0	3.1	4.6	6.6	9.0	12	14	17	19	21	21	21	19	17	14	12	9.0	6.6	4.6	3.1	2.0	1.2	0
19	O	O	O	.04	.08	.15	.28	.50	.84	1.3	2.1	3.1	4.4	5.9	7.6	9.4	11	12	13	14	13	12	11	9.4	7.6	5.9	4.4	3.1	2.1	1.3	.840	0
20	O	O	O	.02	.05	.10	.18	.31	.53	.84	1.2	1.8	2.6	3.5	4.5	5.5	6.5	7.3	7.8	8.0	7.8	7.3	6.5	5.5	4.5	3.5	2.6	1.8	1.2	.84	.530	0
21	O	O	O	.01	.03	.06	.10	.18	.30	.47	.72	1.0	1.4	1.9	2.4	3.0	3.5	3.9	4.2	4.3	4.2	3.9	3.5	3.0	2.4	1.9	1.4	1.0	.72	.47	.300	0
22	O	O	O	+	.01	.03	.05	.09	.15	.24	.37	.53	.74	.98	1.2	1.5	1.7	1.9	2.0	2.1	2.0	1.9	1.7	1.5	1.2	.98	.74	.53	.37	.24	.150	0
23	O	O	O	+	+	.01	.02	.04	.07	.11	.17	.25	.34	.45	.57	.69	.80	.90	.96	.98	.96	.90	.80	.69	.57	.45	.34	.25	.17	.11	.070	0
24	O	O	O	+	+	+	.01	.02	.03	.05	.07	.10	.14	.19	.24	.29	.34	.38	.40	.41	.40	.38	.34	.29	.24	.19	.14	.10	.07	.05	.030	0
25	O	O	O	+	+	+	+	.01	.01	.02	.04	.05	.07	.09	.11	.13	.14	.15	.16	.15	.14	.13	.11	.09	.07	.05	.04	.02	.01	.010	0
26	O	O	O	+	+	+	+	+	+	.01	.01	.02	.03	.04	.04	.05	.05	.05	.05	.05	.04	.04	.03	.02	.01	.01	+	+	+0	0
27	O	O	O	.	+	+	+	+	+	+	+	+	.01	.01	.01	.02	.02	.02	.02	.02	.01	.01	.01	+	+	+	+	+	+0	0
28	O	O	O	.	.	.	+	+	+	+	+	+	+	+	+	+	.01	.01	.01	+	+	+	+	+	+	+	+	+	+0	0
29	O	O	O	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+0	0
30	O	O	O	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+0	0
31	O	O	O	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+0	0
32	O	O	O	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+0	0
33	O	O	O	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+0	0
34	O	O	O	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+0	0
35	O	O	O	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+0	0
36	O	O	O	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+0	0
37	O	O	O	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+0	0
38	O	O	O	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+0	0
39	O	O	O	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+0	0
40	O	O	O	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+0	0
41	O	O	O	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+0	0
42	O	O	O	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.0	0
43	O	O	O	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.0	0
44	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O

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THICKNESS (FT) OF SILT     ACCUMULATED ON BOTTOM,     3600.00 SECONDS AFTER DUMP
...MULTIPLY DISPLAYED VALUES BY   1.000          (LEGEND... + = .LT. .01    . = .LT. .0001   0 = .LT. .000001)
M N=  2    3    4    5    6    7    8    9   10   11   12   13   14   15   16   17   18   19   20   21   22   23   24   25   26   27   28   29   30  31
 2 000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000
 3 0000    0    0    0    0    0    .    .    .    .    .    .    .    .    .    .    +    +    +    .    .    .    .    .    .    .    .    .   .0000
 4 0000    0    0    .    .    .    .    .    .    .    +    +    +    +    +    +    +    +    +    +    +    +    +    +    +    .    .    .   .0000
 5 0000    0    .    .    .    .    .    +    +    +    +    +    +    +    +    +    +    +    +    +    +    +    +    +    +    .    +    +   .0000
 6 0000    .    .    .    .    +    +    +    +    +    +    +    +    +    +  .01  .01  .01  .01  .01    +    +    +    +    +    +    +    +   +0000
 7 0000    .    .    .    +    +    +    +    +    +    +  .01  .01  .02  .02  .03  .03  .03  .03  .03  .02  .02  .01  .01    +    +    +    +   +0000
 8 0000    .    .    +    +    +    +    +    +  .01  .01  .02  .03  .04  .06  .07  .07  .08  .07  .07  .06  .04  .03  .02  .01  .01    +    +   +0000
 9 0000    .    +    +    +    +    +    +  .01  .01  .03  .04  .06  .08  .10  .12  .14  .14  .14  .12  .10  .08  .06  .04  .03  .01  .01    +   +0000
10 0000    .    +    +    +    +    +    +  .01  .02  .04  .06  .09  .12  .15  .18  .20  .21  .20  .18  .15  .12  .09  .06  .04  .02  .01    +   +0000
11 0000    +    +    +    +    +    +  .01  .02  .03  .05  .08  .11  .15  .19  .22  .24  .25  .24  .22  .19  .15  .11  .08  .05  .03  .02  .01   +0000
12 0000    +    +    +    +    +    +  .01  .02  .04  .06  .09  .13  .17  .20  .24  .26  .27  .26  .24  .20  .17  .13  .09  .06  .04  .02  .01   +0000
13 0000    +    +    +    +    +    +  .01  .02  .04  .06  .09  .13  .17  .20  .24  .26  .27  .26  .24  .20  .17  .13  .09  .06  .04  .02  .01   +0000
14 0000    +    +    +    +    +    +  .01  .02  .04  .06  .09  .12  .16  .19  .22  .24  .25  .24  .22  .19  .16  .12  .09  .06  .04  .02  .01   +0000
15 0000    +    +    +    +    +    +  .01  .02  .04  .06  .08  .11  .14  .17  .20  .21  .22  .21  .20  .17  .14  .11  .08  .06  .04  .02  .01   +0000
16 0000    +    +    +    +    +    +  .01  .02  .03  .05  .07  .09  .12  .14  .16  .18  .18  .18  .16  .14  .12  .09  .07  .05  .03  .02  .01   +0000
17 0000    +    +    +    +    +    +  .01  .02  .03  .04  .05  .07  .09  .11  .12  .13  .14  .13  .12  .11  .09  .07  .05  .04  .03  .02  .01   +0000
18 0000    +    +    +    +    +    +    +  .01  .02  .03  .04  .05  .06  .08  .09  .09  .10  .09  .09  .08  .06  .05  .04  .03  .02  .01    +   +0000
19 0000    +    +    +    +    +    +    +  .01  .01  .02  .02  .03  .04  .05  .05  .06  .06  .06  .05  .05  .04  .03  .02  .02  .01  .01    +   +0000
20 0000    +    +    +    +    +    +    +    +    +  .01  .01  .02  .02  .03  .03  .03  .03  .03  .03  .03  .02  .02  .01  .01    +    +    +   +0000
21 0000    .    +    +    +    +    +    +    +    +    +    +  .01  .01  .01  .01  .02  .02  .02  .01  .01  .01  .01    +    +    +    +    +   +0000
22 0000    .    .    +    +    +    +    +    +    +    +    +    +    +    +    +  .01  .01  .01    +    +    +    +    +    +    +    +    +   +0000
23 0000    .    .    .    +    +    +    +    +    +    +    +    +    +    +    +    +    +    +    +    +    +    +    +    +    +    +    +   +0000
24 0000    .    .    .    .    .    +    +    +    +    +    +    +    +    +    +    +    +    +    +    +    +    +    +    +    +    +    +   +0000
25 0000    .    .    .    .    .    .    .    +    +    +    +    +    +    +    +    +    +    +    +    +    +    +    +    +    +    +    .   .0000
26 0000    .    .    .    .    .    .    .    .    .    .    +    +    +    +    +    +    +    +    +    +    +    +    +    .    .    .    .   .0000
27 0000    0    0    .    .    .    .    .    .    .    .    .    .    .    .    .    +    +    +    .    .    .    .    .    .    .    .    .   .0000
28 0000    0    0    0    0    .    .    .    .    .    .    .    .    .    .    .    .    .    .    .    .    .    .    .    .    .    .    .   .0000
29 0000    0    0    0    0    0    .    .    .    .    .    .    .    .    .    .    .    .    .    .    .    .    .    .    .    .    .    .   .0000
30 0000    0    0    0    0    0    0    .    .    .    .    .    .    .    .    .    .    .    .    .    .    .    .    .    .    .    .    .   00000
31 0000    0    0    0    0    0    0    .    .    .    .    .    .    .    .    .    .    .    .    .    .    .    .    .    .    .    .    .   00000
32 0000    0    0    0    0    0    0    .    .    .    .    .    .    .    .    .    .    .    .    .    .    .    .    .    .    .    .    .   00000
33 0000    0    0    0    0    0    0    .    .    .    .    .    .    .    .    .    .    .    .    .    .    .    .    .    .    .    .    .   00000
34 0000    0    0    0    0    0    0    .    .    .    .    .    .    .    .    .    .    .    .    .    .    .    .    .    .    .    .    .   00000
35 0000    0    0    0    0    0    0    .    .    .    .    .    .    .    .    .    .    .    .    .    .    .    .    .    .    .    .    .   00000
36 0000    0    0    0    0    0    0    .    .    .    .    .    .    .    .    .    .    .    .    .    .    .    .    .    .    .    .    .   00000
37 0000    0    0    0    0    0    0    .    .    .    .    .    .    .    .    .    .    .    .    .    .    .    .    .    .    .    .    .   00000
38 0000    0    0    0    0    0    0    .    .    .    .    .    .    .    .    .    .    .    .    .    .    .    .    .    .    .    .    .   00000
39 0000    0    0    0    0    0    0    .    .    .    .    .    .    .    .    .    .    .    .    .    .    .    .    .    .    .    .    .   00000
40 0000    0    0    0    0    0    0    0    .    .    .    .    .    .    .    .    .    .    .    .    .    .    .    .    .    .    .    0   00000
41 0000    0    0    0    0    0    0    0    .    .    .    .    .    .    .    .    .    .    .    .    .    .    .    .    .    .    .    0   00000
42 0000    0    0    0    0    0    0    0    0    .    .    .    .    .    .    .    .    .    .    .    .    .    .    .    .    .    0    0   00000
43 0000    0    0    0    0    0    0    0    0    0    .    .    .    .    .    .    .    .    .    .    .    .    .    .    .    0    0    0   00000
44 000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000
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BEGIN LONG TERM SIMULATION OF FATE OF CLAY

SUMMARY OF CLAY DISTRIBUTIONS AFTER 300.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 1319.2
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 548.75

SUMMARY OF CLAY DISTRIBUTIONS AFTER 600.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 712.29
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 1154.6

SUMMARY OF CLAY DISTRIBUTIONS AFTER 900.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 220.68
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 1644.7

CONCENTRATIONS ABOVE BACKGROUND OF CLAY (MG/L) IN THE CLOUD 900.00 SECONDS AFTER DUMP

60.00 FT BELOW THE WATER SURFACE

...MULTIPLY DISPLAYED VALUES BY 1.000 (LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)

M	N=	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31
2	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O
3	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	O	0	0	0	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	0
9	O	0	0	0	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	0
10	O	0	0	0	+	+	+	+	+	+	+	.01	.01	.02	.02	.02	.03	.03	.03	.02	.02	.02	.01	.01	+	+	+	+	+	+	0
11	O	0	0	0	+	+	+	+	.01	.01	.02	.04	.06	.07	.09	.11	.12	.12	.12	.11	.09	.07	.06	.04	.02	.01	.01	+	+	+	0
12	O	0	0	0	+	+	.01	.01	.03	.05	.08	.13	.18	.24	.30	.35	.39	.40	.39	.35	.30	.24	.18	.13	.08	.05	.03	.01	+	+	0
13	O	0	0	0	+	.01	.02	.04	.08	.13	.21	.32	.45	.61	.76	.90	.99	1.0	.99	.90	.76	.61	.45	.32	.21	.13	.08	.04	+	+	0
14	O	0	0	0	.01	.02	.04	.08	.15	.25	.41	.62	.89	1.2	1.5	2.1	2.7	3.0	2.7	2.1	1.5	1.2	.89	.62	.41	.25	.15	.08	+	+	0
15	O	0	0	0	.01	.03	.06	.12	.22	.38	.61	.94	1.3	2.2	5.4	18	46	64	46	18	5.4	2.2	1.3	.94	.61	.38	.22	.12	+	+	0
16	O	0	0	0	.01	.03	.07	.14	.25	.44	.72	1.1	1.6	3.6	16	77	218	313	218	77	16	3.6	1.6	1.1	.72	.44	.25	.14	+	+	0
17	O	0	0	0	.01	.03	.06	.12	.23	.40	.64	.99	1.4	2.4	7.0	26	67	94	67	26	7.0	2.4	1.4	.99	.64	.40	.23	.12	+	+	0
18	O	0	0	0	.01	.02	.04	.09	.16	.28	.45	.68	.98	1.3	1.8	2.6	3.8	4.4	3.8	2.6	1.8	1.3	.98	.68	.45	.28	.16	.09	+	+	0
19	O	0	0	0	+	.01	.02	.05	.09	.15	.24	.36	.52	.70	.88	1.0	1.1	1.1	1.1	1.0	.88	.70	.52	.36	.24	.15	.09	.05	+	+	0
20	O	0	0	0	+	+	.01	.02	.04	.06	.10	.15	.22	.29	.36	.42	.47	.48	.47	.42	.36	.29	.22	.15	.10	.06	.04	.02	+	+	0
21	O	0	0	0	+	+	+	+	.01	.02	.03	.05	.07	.09	.12	.14	.15	.16	.15	.14	.12	.09	.07	.05	.03	.02	.01	+	+	+	0
22	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
23	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
24	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
25	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
26	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
27	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
28	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
29	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
30	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
31	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
32	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
33	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
34	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
35	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
36	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
37	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
38	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
39	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
40	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
41	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
42	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
43	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
44	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O

CONCENTRATIONS ABOVE BACKGROUND OF CLAY (MG/L) IN THE CLOUD 900.00 SECONDS AFTER DUMP

119.00 FT BELOW THE WATER SURFACE

...MULTIPLY DISPLAYED VALUES BY 1.000 (LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)

M	N=	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31
2	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O
3	O	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	O	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	O	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	O	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	O	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	O	O	0	0	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	0	0
9	O	O	0	0	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	0	0
10	O	O	0	0	+	+	+	+	+	+	+	.01	.01	.02	.02	.03	.03	.03	.03	.03	.02	.02	.01	.01	+	+	+	+	+	+	0	0
11	O	O	0	0	+	+	+	+	.01	.02	.03	.05	.07	.10	.13	.16	.18	.18	.18	.16	.13	.10	.07	.05	.03	.02	.01	+	+	+	0	0
12	O	O	0	0	+	+	.01	.02	.03	.06	.11	.19	.29	.43	.59	.74	.85	.89	.85	.74	.59	.43	.29	.19	.11	.06	.03	.02	+	+	0	0
13	O	O	0	0	+	.01	.02	.05	.10	.19	.36	.64	1.0	1.6	2.4	3.2	3.8	4.0	3.8	3.2	2.4	1.6	1.0	.64	.36	.19	.10	.05	+	+	0	0
14	O	O	0	0	.01	.02	.05	.11	.22	.46	.91	1.7	3.1	5.3	8.3	12	15	16	15	12	8.3	5.3	3.1	1.7	.91	.46	.22	.11	+	+	0	0
15	O	O	0	0	.01	.03	.08	.17	.38	.82	1.7	3.5	6.7	12	22	35	50	57	50	35	22	12	6.7	3.5	1.7	.82	.38	.17	+	+	0	0
16	O	O	0	0	.01	.04	.09	.21	.47	1.0	2.2	4.6	9.2	18	34	62	102	123	102	62	34	18	9.2	4.6	2.2	1.0	.47	.21	+	+	0	0
17	O	O	0	0	.01	.03	.08	.19	.41	.88	1.8	3.8	7.4	14	24	41	59	69	59	41	24	14	7.4	3.8	1.8	.88	.41	.19	+	+	0	0
18	O	O	0	0	.01	.02	.05	.12	.25	.52	1.0	2.0	3.7	6.4	10	15	18	20	18	15	10	6.4	3.7	2.0	1.0	.52	.25	.12	+	+	0	0
19	O	O	0	0	+	.01	.03	.06	.12	.23	.43	.78	1.3	2.1	3.1	4.1	4.9	5.2	4.9	4.1	3.1	2.1	1.3	.78	.43	.23	.12	.06	+	+	0	0
20	O	O	0	0	+	+	.01	.02	.04	.08	.14	.24	.38	.56	.77	.98	1.1	1.1	1.1	.98	.77	.56	.38	.24	.14	.08	.04	.02	+	+	0	0
21	O	O	0	0	+	+	+	+	.01	.02	.04	.06	.09	.13	.17	.21	.23	.24	.23	.21	.17	.13	.09	.06	.04	.02	.01	+	+	+	0	0
22	O	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
23	O	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
24	O	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
25	O	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
26	O	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
27	O	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
28	O	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
29	O	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
30	O	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
31	O	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
32	O	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
33	O	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
34	O	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
35	O	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
36	O	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
37	O	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
38	O	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
39	O	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
40	O	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
41	O	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
42	O	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
43	O	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
44	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O

BOTTOM ACCUMULATION OF CLAY (CU FT/GRID SQUARE) , 900.00 SECONDS AFTER DUMP

...MULTIPLY DISPLAYED VALUES BY 1.000 (LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)

M N=	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31
2	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O
3	O	O	O	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+
4	O	O	O	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+
5	O	O	O	.	+	+	+	+	+	+	+	.01	.02	.02	.03	.04	.04	.04	.04	.04	.03	.02	.02	.01	+	+	+	+	+	+
6	O	O	O	+	+	+	+	+	.01	.03	.06	.10	.17	.26	.37	.50	.63	.74	.82	.85	.82	.74	.63	.50	.37	.26	.17	.10	.06	.03
7	O	O	O	+	+	+	.01	.02	.04	.09	.17	.30	.50	.76	1.0	1.4	1.8	2.1	2.4	2.4	2.4	2.1	1.8	1.4	1.0	.76	.50	.30	.17	.09
8	O	O	O	+	+	.01	.02	.05	.11	.22	.40	.70	1.1	1.7	2.5	3.3	4.2	4.9	5.4	5.6	5.4	4.9	4.2	3.3	2.5	1.7	1.1	.70	.40	.22
9	O	O	O	+	+	.02	.04	.10	.21	.41	.75	1.3	2.1	3.1	4.5	6.0	7.6	8.9	10	10	10	8.9	7.6	6.0	4.5	3.1	2.1	1.3	.75	.41
10	O	O	O	+	.01	.03	.07	.16	.33	.63	1.1	1.9	3.1	4.7	6.6	8.8	11	13	14	15	14	13	11	8.8	6.6	4.7	3.1	1.9	1.1	.63
11	O	O	O	+	.02	.04	.10	.22	.45	.84	1.5	2.5	3.9	5.8	8.2	11	14	16	17	18	17	16	14	11	8.2	5.8	3.9	2.5	1.5	.84
12	O	O	.01	.02	.06	.14	.28	.55	1.0	1.7	2.8	4.4	6.5	9.0	12	15	17	18	19	18	17	15	12	9.0	6.5	4.4	2.8	1.7	1.0	.55
13	O	O	.01	.03	.08	.17	.33	.63	1.1	1.9	3.0	4.6	6.7	9.1	12	14	17	18	19	18	17	14	12	9.1	6.7	4.6	3.0	1.9	1.1	.63
14	O	O	.02	.04	.09	.19	.36	.67	1.1	1.9	3.0	4.5	6.5	8.7	11	14	16	17	17	17	16	14	11	8.7	6.5	4.5	3.0	1.9	1.1	.67
15	O	O	.02	.04	.09	.19	.36	.66	1.1	1.8	2.8	4.2	5.9	7.8	10	12	14	15	15	15	14	12	10	7.8	5.9	4.2	2.8	1.8	1.1	.66
16	O	O	.02	.04	.09	.18	.33	.59	.99	1.6	2.4	3.5	4.9	6.5	8.2	10	11	12	12	12	11	10	8.2	6.5	4.9	3.5	2.4	1.6	.99	.59
17	O	O	.01	.03	.07	.14	.27	.47	.78	1.2	1.9	2.7	3.7	4.9	6.1	7.3	8.3	8.9	9.1	8.9	8.3	7.3	6.1	4.9	3.7	2.7	1.9	1.2	.78	.47
18	O	O	.01	.02	.05	.10	.19	.33	.54	.86	1.3	1.8	2.5	3.3	4.1	4.9	5.5	5.9	6.1	5.9	5.5	4.9	4.1	3.3	2.5	1.8	1.3	.86	.54	.33
19	O	O	+	.01	.03	.06	.11	.19	.32	.51	.77	1.1	1.5	1.9	2.4	2.8	3.2	3.5	3.5	3.5	3.2	2.8	2.4	1.9	1.5	1.1	.77	.51	.32	.19
20	O	O	+	+	.01	.03	.05	.10	.16	.26	.39	.56	.76	.99	1.2	1.4	1.6	1.7	1.8	1.7	1.6	1.4	1.2	.99	.76	.56	.39	.26	.16	.10
21	O	O	+	+	+	.01	.02	.04	.07	.11	.16	.23	.32	.42	.52	.61	.69	.74	.76	.74	.69	.61	.52	.42	.32	.23	.16	.11	.07	.04
22	O	O	+	+	+	+	+	.01	.02	.04	.05	.08	.11	.15	.18	.21	.24	.26	.27	.26	.24	.21	.18	.15	.11	.08	.05	.04	.02	.01
23	O	O	+	+	+	+	+	+	+	.01	.01	.02	.03	.04	.05	.06	.07	.07	.08	.07	.07	.06	.05	.04	.03	.02	.01	.01	+	+
24	O	O	.	.	+	+	+	+	+	+	+	+	.01	.01	.01	.01	.01	.01	.01	.01	.01	.01	.01	+	+	+	+	+	+	+
25	O	O	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+
26	O	O	.	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.
27	O	O	0	0	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.
28	O	O	0	0	0	0	0	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.
29	O	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.	.	.	0	0	0	0	0	0	0	0	0	0	0
30	O	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
31	O	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
32	O	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
33	O	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
34	O	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
35	O	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
36	O	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
37	O	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
38	O	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
39	O	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
40	O	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
41	O	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
42	O	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
43	O	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
44	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O

SMALL CLOUDS AT 900.00 SECONDS ELAPSED TIME FOR CLAY

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID	LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	753.3	450.0	24.33	0.0000E+00	96.88	4.135	113.8	0.120757E-03
2	754.0	450.0	21.40	0.0000E+00	117.6	28.21	91.79	0.700614E-04
3	754.4	450.0	29.65	0.0000E+00	155.1	75.43	44.57	0.979618E-04
4	754.6	450.0	37.56	0.0000E+00	235.4	89.73	30.27	0.741920E-04
5	754.6	450.0	16.32	0.0000E+00	296.0	68.89	51.11	0.340000E-04
6	754.6	450.0	7.625	0.0000E+00	333.5	60.56	59.44	0.340000E-04
7	754.5	450.0	4.415	0.0000E+00	358.6	58.69	61.31	0.340000E-04
8	754.3	450.0	3.095	0.0000E+00	377.8	57.89	62.11	0.340000E-04
9	754.1	450.0	2.427	0.0000E+00	393.9	57.83	62.17	0.340000E-04
10	753.8	450.0	73.85	0.0000E+00	407.8	119.6	0.4016	0.690000E-02

SUMMARY OF CLAY DISTRIBUTIONS AFTER 1200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 146.93
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 1718.1

SUMMARY OF CLAY DISTRIBUTIONS AFTER 1500.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 146.91
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 1718.1

SUMMARY OF CLAY DISTRIBUTIONS AFTER 1800.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 146.89
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 1718.1

CONCENTRATIONS ABOVE BACKGROUND OF CLAY (MG/L) IN THE CLOUD 1800.00 SECONDS AFTER DUMP

60.00 FT BELOW THE WATER SURFACE

...MULTIPLY DISPLAYED VALUES BY 1.000 (LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)

M N=	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31
2	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O
3	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
4	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
5	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
6	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
7	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
8	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
9	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
10	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
11	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
12	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
13	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
14	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
15	O	0	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	O
16	O	0	+	+	+	+	+	+	+	+	.01	.01	.01	.02	.02	.02	.02	.03	.02	.02	.02	.02	.01	.01	.01	+	+	+	+	O
17	O	0	+	+	+	+	.01	.01	.02	.03	.04	.05	.06	.07	.09	.10	.10	.11	.10	.10	.09	.07	.06	.05	.04	.03	.02	.01	.01	0
18	O	0	+	+	.01	.01	.02	.04	.06	.09	.12	.16	.21	.25	.30	.33	.36	.37	.36	.33	.30	.25	.21	.16	.12	.09	.06	.04	.02	0
19	O	0	.01	.01	.02	.04	.07	.11	.17	.25	.36	.48	.62	.78	.92	1.0	1.1	1.1	1.1	1.0	.92	.78	.62	.48	.36	.25	.17	.11	.07	0
20	O	0	.02	.03	.06	.11	.17	.28	.43	.64	.92	1.2	1.6	2.1	2.6	2.9	3.2	3.3	3.2	2.9	2.6	2.1	1.6	1.2	.92	.64	.43	.28	.17	0
21	O	0	.04	.07	.12	.21	.36	.58	.92	1.4	2.0	2.9	4.1	5.4	6.7	8.0	8.9	9.2	8.9	8.0	6.7	5.4	4.1	2.9	2.0	1.4	.92	.58	.36	0
22	O	0	.06	.11	.21	.36	.62	1.0	1.6	2.6	4.1	6.1	8.9	12	17	21	25	26	25	21	17	12	8.9	6.1	4.1	2.6	1.6	1.0	.62	0
23	O	0	.09	.16	.30	.53	.92	1.5	2.6	4.2	6.7	11	17	26	40	57	73	79	73	57	40	26	17	11	6.7	4.2	2.6	1.5	.92	0
24	O	0	.10	.19	.36	.64	1.1	1.9	3.2	5.4	8.8	15	25	43	72	111	148	163	148	111	72	43	25	15	8.8	5.4	3.2	1.9	1.1	0
25	O	0	.10	.19	.36	.64	1.1	1.9	3.2	5.4	8.8	15	25	42	71	110	146	161	146	110	71	42	25	15	8.8	5.4	3.2	1.9	1.1	0
26	O	0	.09	.16	.30	.53	.92	1.5	2.6	4.2	6.7	11	17	26	39	56	71	77	71	56	39	26	17	11	6.7	4.2	2.6	1.5	.92	0
27	O	0	.06	.11	.21	.36	.62	1.0	1.6	2.6	4.1	6.1	8.8	12	17	21	25	26	25	21	17	12	8.8	6.1	4.1	2.6	1.6	1.0	.62	0
28	O	0	.04	.07	.12	.21	.36	.58	.92	1.4	2.0	2.9	4.1	5.3	6.7	7.9	8.8	9.1	8.8	7.9	6.7	5.3	4.1	2.9	2.0	1.4	.92	.58	.36	0
29	O	0	.02	.03	.06	.10	.17	.28	.43	.64	.92	1.2	1.6	2.1	2.5	2.9	3.2	3.3	3.2	2.9	2.5	2.1	1.6	1.2	.92	.64	.43	.28	.17	0
30	O	0	.01	.01	.02	.04	.07	.11	.17	.25	.36	.48	.62	.77	.92	1.0	1.1	1.1	1.1	1.0	.92	.77	.62	.48	.36	.25	.17	.11	.07	0
31	O	0	+	+	.01	.01	.02	.04	.06	.09	.12	.16	.21	.25	.30	.33	.35	.36	.35	.33	.30	.25	.21	.16	.12	.09	.06	.04	.02	0
32	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
33	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
34	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
35	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
36	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
37	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
38	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
39	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
40	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
41	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
42	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
43	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
44	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O

CONCENTRATIONS ABOVE BACKGROUND OF CLAY (MG/L) IN THE CLOUD 1800.00 SECONDS AFTER DUMP

119.00 FT BELOW THE WATER SURFACE

...MULTIPLY DISPLAYED VALUES BY 1.000 (LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)

M N=	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	0	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+
16	0	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+
17	0	+	+	+	+	+	+	+	+	+	+	+	+	.01	.01	.01	.01	.01	.01	.01	.01	.01	+	+	+	+	+	+	+	+
18	0	+	+	+	+	+	+	+	+	.01	.01	.02	.03	.03	.04	.05	.05	.05	.05	.05	.04	.03	.03	.02	.01	.01	+	+	+	+
19	0	+	+	+	+	.01	.01	.02	.03	.05	.07	.10	.12	.15	.17	.18	.19	.18	.17	.15	.12	.10	.07	.05	.03	.02	.01	.010000		
20	0	+	+	+	.01	.02	.04	.06	.10	.15	.21	.28	.37	.45	.53	.58	.60	.58	.53	.45	.37	.28	.21	.15	.10	.06	.04	.020000		
21	0	+	.01	.01	.03	.05	.09	.15	.23	.36	.53	.75	1.0	1.2	1.5	1.7	1.8	1.7	1.5	1.2	1.0	.75	.53	.36	.23	.15	.09	.050000		
22	0	+	.01	.03	.05	.10	.17	.28	.47	.75	1.1	1.7	2.5	3.4	4.3	5.1	5.4	5.1	4.3	3.4	2.5	1.7	1.1	.75	.47	.28	.17	.100000		
23	0	.01	.02	.04	.08	.15	.26	.45	.77	1.2	2.1	3.4	5.3	8.1	11	14	15	14	11	8.1	5.3	3.4	2.1	1.2	.77	.45	.26	.150000		
24	0	.01	.03	.05	.10	.18	.33	.58	1.0	1.7	2.9	5.0	8.6	14	21	27	30	27	21	14	8.6	5.0	2.9	1.7	1.0	.58	.33	.180000		
25	0	.01	.03	.05	.10	.18	.33	.58	1.0	1.7	2.9	5.0	8.5	14	21	27	30	27	21	14	8.5	5.0	2.9	1.7	1.0	.58	.33	.180000		
26	0	.01	.02	.04	.08	.15	.26	.45	.77	1.2	2.1	3.3	5.3	8.0	11	14	15	14	11	8.0	5.3	3.3	2.1	1.2	.77	.45	.26	.150000		
27	0	+	.01	.03	.05	.10	.17	.28	.47	.75	1.1	1.7	2.4	3.3	4.3	5.0	5.3	5.0	4.3	3.3	2.4	1.7	1.1	.75	.47	.28	.17	.100000		
28	0	+	.01	.01	.03	.05	.09	.15	.23	.36	.53	.74	1.0	1.2	1.5	1.7	1.7	1.7	1.5	1.2	1.0	.74	.53	.36	.23	.15	.09	.050000		
29	0	+	+	+	.01	.02	.04	.06	.10	.15	.21	.28	.37	.45	.53	.58	.60	.58	.53	.45	.37	.28	.21	.15	.10	.06	.04	.020000		
30	0	+	+	+	+	.01	.01	.02	.03	.05	.07	.10	.12	.15	.17	.18	.19	.18	.17	.15	.12	.10	.07	.05	.03	.02	.01	.010000		
31	0	+	+	+	+	+	+	+	.01	.01	.02	.03	.03	.04	.05	.05	.05	.05	.05	.04	.03	.03	.02	.01	.01	+	+	+	+	+
32	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
33	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
34	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
35	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
36	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
37	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
38	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
39	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
40	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
41	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
42	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
43	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
44	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0

BOTTOM ACCUMULATION OF CLAY (CU FT/GRID SQUARE) , 1800.00 SECONDS AFTER DUMP

...MULTIPLY DISPLAYED VALUES BY 1.000 (LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)

M N=	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31
2	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O
3	O	O	O	O	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+
4	O	O	O	.	.	.	+	+	+	+	+	.01	.02	.02	.03	.04	.04	.04	.04	.04	.03	.02	.02	.01	+	+	+	+	+	+
5	O	O	.	+	+	+	+	+	+	.01	.02	.04	.06	.09	.13	.16	.19	.21	.22	.21	.19	.16	.13	.09	.06	.04	.02	.01	+	+
6	O	O	+	+	+	+	+	.01	.03	.06	.10	.17	.26	.37	.50	.63	.74	.82	.85	.82	.74	.63	.50	.37	.26	.17	.10	.06	.03	.01
7	O	O	+	+	+	.01	.02	.04	.09	.17	.30	.50	.76	1.0	1.4	1.8	2.1	2.4	2.4	2.4	2.1	1.8	1.4	1.0	.76	.50	.30	.17	.09	.04
8	O	O	+	+	.01	.02	.05	.11	.22	.40	.70	1.1	1.7	2.5	3.3	4.2	4.9	5.4	5.6	5.4	4.9	4.2	3.3	2.5	1.7	1.1	.70	.40	.22	.11
9	O	O	+	+	.02	.04	.10	.21	.41	.75	1.3	2.1	3.1	4.5	6.0	7.6	8.9	10	10	10	8.9	7.6	6.0	4.5	3.1	2.1	1.3	.75	.41	.21
10	O	O	+	.01	.03	.07	.16	.33	.63	1.1	1.9	3.1	4.7	6.6	8.8	11	13	14	15	14	13	11	8.8	6.6	4.7	3.1	1.9	1.1	.63	.33
11	O	O	+	.02	.04	.10	.22	.45	.84	1.5	2.5	3.9	5.8	8.2	11	14	16	17	18	17	16	14	11	8.2	5.8	3.9	2.5	1.5	.84	.45
12	O	O	.01	.03	.06	.14	.28	.55	1.0	1.7	2.8	4.4	6.5	9.0	12	15	17	18	19	18	17	15	12	9.0	6.5	4.4	2.8	1.7	1.0	.55
13	O	O	.01	.03	.08	.17	.34	.63	1.1	1.9	3.0	4.6	6.7	9.2	12	14	17	18	19	18	17	14	12	9.2	6.7	4.6	3.0	1.9	1.1	.63
14	O	O	.02	.04	.09	.19	.37	.68	1.1	1.9	3.1	4.6	6.5	8.8	11	14	16	17	17	17	16	14	11	8.8	6.5	4.6	3.1	1.9	1.1	.68
15	O	O	.02	.05	.10	.20	.38	.68	1.1	1.9	2.9	4.3	6.0	8.0	10	12	14	15	15	15	14	12	10	8.0	6.0	4.3	2.9	1.9	1.1	.68
16	O	O	.02	.05	.10	.19	.36	.63	1.0	1.6	2.5	3.7	5.1	6.8	8.5	10	12	12	13	12	12	10	8.5	6.8	5.1	3.7	2.5	1.6	1.0	.63
17	O	O	.02	.04	.09	.17	.30	.53	.88	1.3	2.0	3.0	4.1	5.3	6.7	7.9	8.9	10	10	10	8.9	7.9	6.7	5.3	4.1	3.0	2.0	1.3	.88	.53
18	O	O	.01	.03	.07	.13	.23	.40	.66	1.0	1.5	2.2	2.9	3.8	4.8	5.6	6.3	6.8	7.0	6.8	6.3	5.6	4.8	3.8	2.9	2.2	1.5	1.0	.66	.40
19	O	O	.01	.02	.05	.09	.16	.28	.45	.70	1.0	1.4	1.9	2.5	3.1	3.6	4.1	4.4	4.5	4.4	4.1	3.6	3.1	2.5	1.9	1.4	1.0	.70	.45	.28
20	O	O	+	.01	.03	.06	.10	.17	.28	.43	.63	.88	1.1	1.5	1.8	2.1	2.4	2.6	2.6	2.6	2.4	2.1	1.8	1.5	1.1	.88	.63	.43	.28	.17
21	O	O	+	.01	.02	.03	.06	.10	.15	.24	.34	.48	.64	.82	1.0	1.1	1.3	1.3	1.4	1.3	1.3	1.1	1.0	.82	.64	.48	.34	.24	.15	.10
22	O	O	+	+	.01	.01	.03	.05	.08	.12	.17	.24	.32	.41	.50	.58	.64	.69	.70	.69	.64	.58	.50	.41	.32	.24	.17	.12	.08	.05
23	O	O	+	+	+	+	.01	.02	.03	.05	.08	.11	.15	.19	.23	.26	.29	.31	.32	.31	.29	.26	.23	.19	.15	.11	.08	.05	.03	.02
24	O	O	+	+	+	+	+	.01	.01	.02	.03	.04	.06	.08	.09	.11	.12	.13	.13	.13	.12	.11	.09	.08	.06	.04	.03	.02	.01	.01
25	O	O	+	+	+	+	+	+	+	+	.01	.01	.02	.03	.03	.04	.04	.04	.05	.04	.04	.04	.03	.03	.02	.01	.01	+	+	+
26	O	O	.	+	+	+	+	+	+	+	+	+	+	.01	.01	.01	.01	.01	.01	.01	.01	.01	+	+	+	+	+	+	+	+
27	O	O	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+
28	O	O	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+
29	O	O	.	.	.	.	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.
30	O	O	0	0	0	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.
31	O	O	0	0	0	0	0	0	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.
32	O	O	0	0	0	0	0	0	0	0	0	0	0	0	0	.	.	.	.	.	.	.	0	0	0	0	0	0	0	0
33	O	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
34	O	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
35	O	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
36	O	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
37	O	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
38	O	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
39	O	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
40	O	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
41	O	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
42	O	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
43	O	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
44	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O

SMALL CLOUDS AT 1800.00 SECONDS ELAPSED TIME FOR CLAY

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID	LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	1174.	450.0	24.32	0.0000E+00	161.8	0.0000E+00	120.0	0.360017E-04
2	1174.	450.0	21.39	0.0000E+00	186.4	0.0000E+00	120.0	0.340000E-04
3	1175.	450.0	29.62	0.0000E+00	230.0	42.80	77.20	0.392710E-04
4	1175.	450.0	37.53	0.0000E+00	320.4	39.62	80.38	0.340000E-04
5	1175.	450.0	16.32	0.0000E+00	387.4	0.0000E+00	120.0	0.340000E-04
6	1175.	450.0	7.622	0.0000E+00	428.4	0.0000E+00	120.0	0.340000E-04
7	1175.	450.0	4.414	0.0000E+00	455.7	0.0000E+00	120.0	0.340000E-04
8	1175.	450.0	3.094	0.0000E+00	476.5	0.0000E+00	120.0	0.340000E-04
9	1174.	450.0	2.426	0.0000E+00	493.8	0.0000E+00	120.0	0.340000E-04
10	1174.	450.0	0.1538	0.0000E+00	508.9	46.62	73.38	0.340000E-04

SUMMARY OF CLAY DISTRIBUTIONS AFTER 2100.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 146.87
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 1718.1

SUMMARY OF CLAY DISTRIBUTIONS AFTER 2400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 146.86
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 1718.2

SUMMARY OF CLAY DISTRIBUTIONS AFTER 2700.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 146.85
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 1718.2

CONCENTRATIONS ABOVE BACKGROUND OF CLAY (MG/L) IN THE CLOUD 2700.00 SECONDS AFTER DUMP

60.00 FT BELOW THE WATER SURFACE

...MULTIPLY DISPLAYED VALUES BY 1.000 (LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)

M N=	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
18	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
19	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
20	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
21	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
22	+	+	+	+	+	+	+	+	+	+	+	+	.01	.01	.01	.01	.01	.01	.01	.01	.01	+	+	+	+	+	+	+	+	+
23	+	+	+	+	+	+	.01	.01	.01	.02	.02	.02	.03	.03	.03	.03	.03	.03	.03	.03	.03	.02	.02	.02	.01	.01	.01	+	+	+
24	+	+	+	.01	.01	.02	.02	.03	.04	.05	.06	.07	.08	.09	.10	.10	.11	.10	.10	.09	.08	.07	.06	.05	.04	.03	.02	.02	0	0
25	0	+	.01	.01	.02	.03	.05	.06	.09	.11	.14	.17	.20	.23	.26	.28	.29	.29	.29	.28	.26	.23	.20	.17	.14	.11	.09	.06	.05	0
26	0	.01	.02	.04	.06	.08	.11	.16	.21	.27	.35	.43	.51	.59	.66	.72	.75	.77	.75	.72	.66	.59	.51	.43	.35	.27	.21	.16	.11	0
27	0	.03	.05	.08	.12	.18	.25	.35	.47	.62	.80	.99	1.2	1.4	1.6	1.7	1.8	1.8	1.8	1.7	1.6	1.4	1.2	.99	.80	.62	.47	.35	.25	0
28	0	.06	.10	.15	.23	.34	.50	.70	.96	1.3	1.7	2.1	2.6	3.2	3.6	4.1	4.3	4.4	4.3	4.1	3.6	3.2	2.6	2.1	1.7	1.3	.96	.70	.50	0
29	0	.11	.17	.26	.40	.61	.89	1.2	1.8	2.4	3.3	4.4	5.6	6.9	8.2	9.4	10	10	10	9.4	8.2	6.9	5.6	4.4	3.3	2.4	1.8	1.2	.89	0
30	0	.16	.26	.41	.63	.96	1.4	2.1	3.0	4.3	6.0	8.3	11	14	18	21	24	24	24	21	18	14	11	8.3	6.0	4.3	3.0	2.1	1.4	0
31	0	.21	.35	.55	.87	1.3	2.0	3.0	4.5	6.6	10	14	20	27	35	43	49	51	49	43	35	27	20	14	10	6.6	4.5	3.0	2.0	0
32	0	.26	.42	.67	1.0	1.6	2.5	3.8	5.8	8.8	13	20	30	42	56	70	80	84	80	70	56	42	30	20	13	8.8	5.8	3.8	2.5	0
33	0	.27	.44	.70	1.1	1.7	2.6	4.1	6.3	10	15	22	33	48	64	80	92	97	92	80	64	48	33	22	15	10	6.3	4.1	2.6	0
34	0	.25	.41	.65	1.0	1.5	2.4	3.7	5.6	8.5	13	19	28	39	52	65	74	77	74	65	52	39	28	19	13	8.5	5.6	3.7	2.4	0
35	0	.20	.33	.53	.82	1.2	1.9	2.8	4.2	6.2	9.0	13	18	24	31	38	43	44	43	38	31	24	18	13	9.0	6.2	4.2	2.8	1.9	0
36	0	.15	.24	.38	.58	.88	1.3	1.9	2.7	3.9	5.4	7.3	10	13	15	18	20	21	20	18	15	13	10	7.3	5.4	3.9	2.7	1.9	1.3	0
37	0	.10	.15	.24	.37	.55	.80	1.1	1.6	2.2	2.9	3.8	4.8	5.9	7.0	8.0	8.6	8.8	8.6	8.0	7.0	5.9	4.8	3.8	2.9	2.2	1.6	1.1	.80	0
38	0	.06	.09	.14	.21	.30	.44	.62	.85	1.1	1.4	1.8	2.3	2.7	3.1	3.4	3.7	3.8	3.7	3.4	3.1	2.7	2.3	1.8	1.4	1.1	.85	.62	.44	0
39	0	.03	.04	.07	.10	.15	.22	.30	.41	.53	.68	.85	1.0	1.2	1.3	1.4	1.5	1.6	1.5	1.4	1.3	1.2	1.0	.85	.68	.53	.41	.30	.22	0
40	0	.01	.02	.03	.05	.07	.10	.13	.18	.23	.29	.36	.43	.50	.55	.60	.63	.64	.63	.60	.55	.50	.43	.36	.29	.23	.18	.13	.10	0
41	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
42	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
43	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
44	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0

CONCENTRATIONS ABOVE BACKGROUND OF CLAY (MG/L) IN THE CLOUD 2700.00 SECONDS AFTER DUMP

119.00 FT BELOW THE WATER SURFACE

...MULTIPLY DISPLAYED VALUES BY 1.000 (LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)

M N=	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
18	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
19	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
20	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
21	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
22	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+
23	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+
24	+	+	+	+	+	+	+	+	+	+	+	.01	.01	.01	.01	.01	.01	.01	.01	.01	.01	.01	.01	+	+	+	+	+	+	+
25	+	+	+	+	+	+	.01	.01	.01	.02	.02	.02	.03	.03	.04	.04	.04	.04	.04	.03	.03	.02	.02	.02	.01	.01	.01	+	+	+
26	+	+	+	+	.01	.01	.02	.03	.04	.05	.06	.07	.08	.09	.10	.10	.11	.10	.10	.09	.08	.07	.06	.05	.04	.03	.02	.01	0	0
27	+	+	.01	.01	.02	.03	.05	.06	.09	.11	.14	.17	.20	.23	.25	.26	.27	.26	.25	.23	.20	.17	.14	.11	.09	.06	.05	.03	0	0
28	+	.01	.02	.03	.05	.07	.10	.14	.18	.24	.31	.38	.46	.53	.59	.63	.64	.63	.59	.53	.46	.38	.31	.24	.18	.14	.10	.07	0	0
29	.01	.02	.03	.05	.08	.12	.18	.26	.35	.48	.63	.81	1.0	1.1	1.3	1.4	1.5	1.4	1.3	1.1	1.0	.81	.63	.48	.35	.26	.18	.12	0	0
30	.02	.03	.05	.09	.13	.20	.30	.43	.62	.87	1.2	1.6	2.0	2.6	3.0	3.4	3.5	3.4	3.0	2.6	2.0	1.6	1.2	.87	.62	.43	.30	.20	0	0
31	.03	.05	.08	.12	.19	.29	.44	.65	.96	1.4	2.0	2.8	3.9	5.1	6.2	7.0	7.3	7.0	6.2	5.1	3.9	2.8	2.0	1.4	.96	.65	.44	.29	0	0
32	.03	.06	.09	.15	.23	.36	.55	.84	1.2	1.9	2.9	4.2	6.0	8.0	10	12	12	12	10	8.0	6.0	4.2	2.9	1.9	1.2	.84	.55	.36	0	0
33	.03	.06	.10	.16	.25	.38	.59	.91	1.3	2.1	3.2	4.8	6.8	9.2	12	13	14	13	12	9.2	6.8	4.8	3.2	2.1	1.3	.91	.59	.38	0	0
34	.03	.05	.09	.14	.23	.35	.53	.81	1.2	1.8	2.7	4.0	5.6	7.5	9.3	11	11	11	9.3	7.5	5.6	4.0	2.7	1.8	1.2	.81	.53	.35	0	0
35	.03	.04	.07	.11	.18	.27	.41	.61	.89	1.3	1.8	2.5	3.5	4.5	5.4	6.1	6.4	6.1	5.4	4.5	3.5	2.5	1.8	1.3	.89	.61	.41	.27	0	0
36	.02	.03	.05	.08	.12	.19	.27	.40	.56	.78	1.0	1.4	1.8	2.2	2.6	2.8	2.9	2.8	2.6	2.2	1.8	1.4	1.0	.78	.56	.40	.27	.19	0	0
37	.01	.02	.03	.05	.07	.11	.16	.23	.32	.42	.55	.70	.86	1.0	1.1	1.2	1.2	1.2	1.1	1.0	.86	.70	.55	.42	.32	.23	.16	.11	0	0
38	+	.01	.02	.03	.04	.06	.08	.12	.16	.21	.27	.33	.39	.45	.50	.53	.54	.53	.50	.45	.39	.33	.27	.21	.16	.12	.08	.06	0	0
39	+	+	.01	.01	.02	.03	.04	.05	.07	.09	.12	.14	.17	.19	.21	.22	.23	.22	.21	.19	.17	.14	.12	.09	.07	.05	.04	.03	0	0
40	+	+	+	+	.01	.01	.02	.02	.03	.04	.05	.06	.07	.08	.08	.09	.09	.09	.08	.08	.07	.06	.05	.04	.03	.02	.02	.01	0	0
41	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
42	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
43	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
44	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0

BOTTOM ACCUMULATION OF CLAY (CU FT/GRID SQUARE) , 2700.00 SECONDS AFTER DUMP

...MULTIPLY DISPLAYED VALUES BY 1.000 (LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)

M N=	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31
2	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O
3	O	O	O	O	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+0
4	O	O	O	.	.	.	+	+	+	+	+	+	+	.01	.02	.02	.03	.04	.04	.04	.04	.04	.03	.02	.02	.01	+	+	+	+0
5	O	O	.	+	+	+	+	+	+	+	.01	.02	.04	.06	.09	.13	.16	.19	.21	.22	.21	.19	.16	.13	.09	.06	.04	.02	.01	+	+0
6	O	O	+	+	+	+	+	.01	.03	.06	.10	.17	.26	.37	.50	.63	.74	.82	.85	.82	.74	.63	.50	.37	.26	.17	.10	.06	.03	.01	0
7	O	O	+	+	+	.01	.02	.04	.09	.17	.30	.50	.76	1.0	1.4	1.8	2.1	2.4	2.4	2.4	2.4	2.1	1.8	1.4	1.0	.76	.50	.30	.17	.09	.04	0
8	O	O	+	+	.01	.02	.05	.11	.22	.40	.70	1.1	1.7	2.5	3.3	4.2	4.9	5.4	5.6	5.4	4.9	4.2	3.3	2.5	1.7	1.1	.70	.40	.22	.11	0
9	O	O	+	+	.02	.04	.10	.21	.41	.75	1.3	2.1	3.1	4.5	6.0	7.6	8.9	10	10	10	8.9	7.6	6.0	4.5	3.1	2.1	1.3	.75	.41	.21	0
10	O	O	+	.01	.03	.07	.16	.33	.63	1.1	1.9	3.1	4.7	6.6	8.8	11	13	14	15	14	13	11	8.8	6.6	4.7	3.1	1.9	1.1	.63	.33	0
11	O	O	+	.02	.04	.10	.22	.45	.84	1.5	2.5	3.9	5.8	8.2	11	14	16	17	18	17	16	14	11	8.2	5.8	3.9	2.5	1.5	.84	.45	0
12	O	O	.01	.03	.06	.14	.28	.55	1.0	1.7	2.8	4.4	6.5	9.0	12	15	17	18	19	18	17	15	12	9.0	6.5	4.4	2.8	1.7	1.0	.55	0
13	O	O	.01	.03	.08	.17	.34	.63	1.1	1.9	3.0	4.6	6.7	9.2	12	14	17	18	19	18	17	14	12	9.2	6.7	4.6	3.0	1.9	1.1	.63	0
14	O	O	.02	.04	.09	.19	.37	.68	1.1	1.9	3.1	4.6	6.5	8.8	11	14	16	17	17	17	16	14	11	8.8	6.5	4.6	3.1	1.9	1.1	.68	0
15	O	O	.02	.05	.10	.20	.38	.68	1.1	1.9	2.9	4.3	6.0	8.0	10	12	14	15	15	15	14	12	10	8.0	6.0	4.3	2.9	1.9	1.1	.68	0
16	O	O	.02	.05	.10	.19	.36	.63	1.0	1.6	2.5	3.7	5.1	6.8	8.5	10	12	12	13	12	12	10	8.5	6.8	5.1	3.7	2.5	1.6	1.0	.63	0
17	O	O	.02	.04	.09	.17	.30	.53	.88	1.3	2.0	3.0	4.1	5.3	6.7	7.9	8.9	10	10	10	8.9	7.9	6.7	5.3	4.1	3.0	2.0	1.3	.88	.53	0
18	O	O	.01	.03	.07	.13	.23	.40	.66	1.0	1.5	2.2	2.9	3.8	4.8	5.6	6.3	6.8	7.0	6.8	6.3	5.6	4.8	3.8	2.9	2.2	1.5	1.0	.66	.40	0
19	O	O	.01	.02	.05	.09	.16	.28	.45	.70	1.0	1.4	1.9	2.5	3.1	3.6	4.1	4.4	4.5	4.4	4.1	3.6	3.1	2.5	1.9	1.4	1.0	.70	.45	.28	0
20	O	O	+	.01	.03	.06	.10	.17	.28	.43	.63	.88	1.1	1.5	1.8	2.1	2.4	2.6	2.6	2.6	2.4	2.1	1.8	1.5	1.1	.88	.63	.43	.28	.17	0
21	O	O	+	.01	.02	.03	.06	.10	.15	.24	.34	.48	.64	.82	1.0	1.1	1.3	1.3	1.4	1.3	1.3	1.1	1.0	.82	.64	.48	.34	.24	.15	.10	0
22	O	O	+	+	.01	.01	.03	.05	.08	.12	.17	.24	.32	.41	.50	.58	.64	.69	.70	.69	.64	.58	.50	.41	.32	.24	.17	.12	.08	.05	0
23	O	O	+	+	+	+	.01	.02	.03	.05	.08	.11	.15	.19	.23	.26	.29	.31	.32	.31	.29	.26	.23	.19	.15	.11	.08	.05	.03	.02	0
24	O	O	+	+	+	+	+	.01	.01	.02	.03	.04	.06	.08	.09	.11	.12	.13	.13	.13	.12	.11	.09	.08	.06	.04	.03	.02	.01	.01	0
25	O	O	+	+	+	+	+	+	+	+	.01	.01	.02	.03	.03	.04	.04	.04	.05	.04	.04	.04	.03	.03	.02	.01	.01	+	+	+0
26	O	O	.	+	+	+	+	+	+	+	+	+	.01	.01	.01	.01	.01	.01	.01	.01	.01	.01	.01	+	+	+	+	+	+	+0
27	O	O	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+0
28	O	O	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+0
29	O	O	.	.	.	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.0
30	O	O	.	.	.	.	.	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.0
31	O	O	.	.	.	.	.	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.0
32	O	O	.	.	.	.	.	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.0
33	O	O	.	.	.	.	.	.	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.0
34	O	O	0	.	.	.	.	.	.	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.0
35	O	O	0	.	.	.	.	.	.	.	.	.	.	.	.	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.0
36	O	O	0	0	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.0
37	O	O	0	0	0	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.0
38	O	O	0	0	0	0	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.0
39	O	O	0	0	0	0	0	0	0	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	0	0
40	O	O	0	0	0	0	0	0	0	0	0	0	.	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0	0
41	O	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
42	O	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
43	O	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
44	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O

SMALL CLOUDS AT 2700.00 SECONDS ELAPSED TIME FOR CLAY

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID	LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	1594.	450.0	24.31	0.0000E+00	237.6	0.0000E+00	120.0	0.340000E-04
2	1595.	450.0	21.39	0.0000E+00	265.5	0.0000E+00	120.0	0.340000E-04
3	1595.	450.0	29.61	0.0000E+00	314.4	0.0000E+00	120.0	0.340000E-04
4	1595.	450.0	37.52	0.0000E+00	414.1	0.0000E+00	120.0	0.340000E-04
5	1595.	450.0	16.31	0.0000E+00	486.9	0.0000E+00	120.0	0.340000E-04
6	1595.	450.0	7.620	0.0000E+00	531.1	0.0000E+00	120.0	0.340000E-04
7	1595.	450.0	4.413	0.0000E+00	560.4	0.0000E+00	120.0	0.340000E-04
8	1595.	450.0	3.094	0.0000E+00	582.7	0.0000E+00	120.0	0.340000E-04
9	1595.	450.0	2.425	0.0000E+00	601.3	0.0000E+00	120.0	0.340000E-04
10	1595.	450.0	0.1538	0.0000E+00	617.4	0.0000E+00	120.0	0.340000E-04

SUMMARY OF CLAY DISTRIBUTIONS AFTER 3000.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 146.84
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 1718.2

SUMMARY OF CLAY DISTRIBUTIONS AFTER 3300.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 146.82
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 1718.2

SUMMARY OF CLAY DISTRIBUTIONS AFTER 3600.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 146.81
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 1718.2

CONCENTRATIONS ABOVE BACKGROUND OF CLAY (MG/L) IN THE CLOUD 3600.00 SECONDS AFTER DUMP

60.00 FT BELOW THE WATER SURFACE

...MULTIPLY DISPLAYED VALUES BY 1.000 (LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)

M N=	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31
2	00000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000																													
3	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
4	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
5	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
6	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
7	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
8	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
9	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
10	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
11	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
12	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
13	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
14	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
15	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
16	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
17	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
18	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
19	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
20	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
21	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
22	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
23	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
24	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
25	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
26	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
27	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
28	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
29	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
30	0000	+	+	+	+	.01	.01	.01	.02	.02	.02	.03	.03	.04	.04	.04	.04	.04	.04	.04	.04	.04	.03	.03	.02	.02	.02	.01	.010000	
31	0000	+	.01	.01	.02	.02	.03	.04	.05	.06	.06	.07	.08	.09	.10	.11	.11	.11	.11	.11	.10	.09	.08	.07	.06	.06	.05	.04	.030000	
32	0000	.02	.02	.03	.04	.05	.07	.09	.11	.13	.15	.17	.20	.22	.23	.25	.26	.26	.26	.25	.23	.22	.20	.17	.15	.13	.11	.09	.070000	
33	0000	.03	.05	.07	.09	.12	.15	.19	.23	.28	.33	.38	.43	.48	.52	.55	.57	.58	.57	.55	.52	.48	.43	.38	.33	.28	.23	.19	.150000	
34	0000	.07	.10	.13	.17	.23	.30	.38	.47	.57	.68	.80	.91	1.0	1.1	1.1	1.2	1.2	1.2	1.1	1.1	1.0	.91	.80	.68	.57	.47	.38	.300000	
35	0000	.12	.17	.24	.32	.42	.55	.71	.89	1.1	1.3	1.5	1.8	2.0	2.2	2.4	2.5	2.5	2.5	2.4	2.2	2.0	1.8	1.5	1.3	1.1	.89	.71	.550000	
36	0000	.20	.29	.40	.54	.73	.97	1.2	1.6	2.0	2.5	3.0	3.5	4.0	4.5	4.9	5.2	5.3	5.2	4.9	4.5	4.0	3.5	3.0	2.5	2.0	1.6	1.2	.970000	
37	0000	.31	.44	.62	.86	1.1	1.5	2.1	2.7	3.5	4.4	5.5	6.6	7.8	8.9	10	10	11	10	10	8.9	7.8	6.6	5.5	4.4	3.5	2.7	2.1	1.50000	
38	0000	.44	.63	.90	1.2	1.7	2.4	3.2	4.3	5.7	7.4	9.4	12	14	16	18	19	20	19	18	16	14	12	9.4	7.4	5.7	4.3	3.2	2.40000	
39	0000	.57	.83	1.1	1.6	2.3	3.3	4.6	6.3	8.5	11	15	19	23	27	30	33	33	33	30	27	23	19	15	11	8.5	6.3	4.6	3.30000	
40	0000	.68	.99	1.4	2.0	2.9	4.1	5.8	8.1	11	15	20	26	32	38	43	47	48	47	43	38	32	26	20	15	11	8.1	5.8	4.10000	
41	0000	.74	1.0	1.5	2.2	3.2	4.6	6.5	9.2	13	18	23	30	38	45	51	55	57	55	51	45	38	30	23	18	13	9.2	6.5	4.60000	
42	0000	.72	1.0	1.5	2.2	3.1	4.4	6.3	8.9	12	17	23	29	36	43	49	53	54	53	49	43	36	29	23	17	12	8.9	6.3	4.40000	
43	0000	.64	.94	1.3	1.9	2.7	3.8	5.4	7.5	10	14	18	23	29	34	38	41	42	41	38	34	29	23	18	14	10	7.5	5.4	3.80000	
44	00000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000																													

CONCENTRATIONS ABOVE BACKGROUND OF CLAY (MG/L) IN THE CLOUD 3600.00 SECONDS AFTER DUMP

119.00 FT BELOW THE WATER SURFACE

...MULTIPLY DISPLAYED VALUES BY 1.000 (LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)

M N=	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
18	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
19	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
20	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
21	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
22	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
23	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
24	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
25	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
26	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
27	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
28	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
29	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
30	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+
31	+	+	+	+	+	+	+	+	+	.01	.01	.01	.01	.01	.01	.01	.01	.01	.01	.01	.01	.01	.01	.01	.01	+	+	+	+	+
32	+	+	+	+	+	.01	.01	.01	.01	.02	.02	.02	.03	.03	.03	.03	.03	.03	.03	.03	.03	.03	.02	.02	.02	.01	.01	.01	.01	0
33	+	+	.01	.01	.01	.02	.02	.03	.04	.04	.05	.06	.07	.07	.08	.08	.08	.08	.08	.07	.07	.06	.05	.04	.04	.03	.02	.02	0	0
34	.01	.01	.01	.02	.03	.04	.05	.06	.08	.09	.11	.13	.14	.16	.17	.17	.18	.17	.17	.16	.14	.13	.11	.09	.08	.06	.05	.04	0	0
35	.01	.02	.03	.04	.06	.08	.10	.12	.16	.19	.22	.26	.29	.33	.35	.37	.37	.37	.35	.33	.29	.26	.22	.19	.16	.12	.10	.08	0	0
36	.03	.04	.05	.07	.10	.14	.18	.23	.29	.36	.43	.51	.59	.66	.71	.75	.76	.75	.71	.66	.59	.51	.43	.36	.29	.23	.18	.14	0	0
37	.04	.06	.09	.12	.17	.22	.30	.39	.51	.64	.79	.96	1.1	1.2	1.4	1.4	1.5	1.4	1.4	1.2	1.1	.96	.79	.64	.51	.39	.30	.22	0	0
38	.06	.09	.13	.18	.25	.34	.47	.63	.83	1.0	1.3	1.6	2.0	2.3	2.6	2.8	2.8	2.8	2.6	2.3	2.0	1.6	1.3	1.0	.83	.63	.47	.34	0	0
39	.08	.12	.17	.24	.34	.48	.66	.91	1.2	1.6	2.1	2.7	3.3	3.8	4.3	4.7	4.8	4.7	4.3	3.8	3.3	2.7	2.1	1.6	1.2	.91	.66	.48	0	0
40	.09	.14	.20	.29	.42	.60	.84	1.1	1.6	2.2	2.9	3.7	4.6	5.5	6.2	6.7	6.9	6.7	6.2	5.5	4.6	3.7	2.9	2.2	1.6	1.1	.84	.60	0	0
41	.10	.15	.22	.32	.46	.66	.94	1.3	1.8	2.5	3.3	4.3	5.4	6.4	7.3	7.9	8.1	7.9	7.3	6.4	5.4	4.3	3.3	2.5	1.8	1.3	.94	.66	0	0
42	.10	.15	.22	.31	.45	.64	.92	1.2	1.7	2.4	3.2	4.2	5.2	6.2	7.0	7.6	7.8	7.6	7.0	6.2	5.2	4.2	3.2	2.4	1.7	1.2	.92	.64	0	0
43	.09	.13	.19	.27	.39	.55	.78	1.0	1.4	2.0	2.6	3.3	4.1	4.9	5.5	5.9	6.1	5.9	5.5	4.9	4.1	3.3	2.6	2.0	1.4	1.0	.78	.55	0	0
44	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0

BOTTOM ACCUMULATION OF CLAY (CU FT/GRID SQUARE) , 3600.00 SECONDS AFTER DUMP

...MULTIPLY DISPLAYED VALUES BY 1.000 (LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)

M N=	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31
2	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O
3	O	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+
4	O	.	.	.	+	+	+	+	+	+	+	.01	.02	.02	.03	.04	.04	.04	.04	.04	.03	.02	.02	.01	+	+	+	+	+	+
5	O	.	+	+	+	+	+	+	.01	.02	.04	.06	.09	.13	.16	.19	.21	.22	.21	.19	.16	.13	.09	.06	.04	.02	.01	+	+	+
6	O	+	+	+	+	+	.01	.03	.06	.10	.17	.26	.37	.50	.63	.74	.82	.85	.82	.74	.63	.50	.37	.26	.17	.10	.06	.03	.01	0
7	O	+	+	+	.01	.02	.04	.09	.17	.30	.50	.76	1.0	1.4	1.8	2.1	2.4	2.4	2.4	2.1	1.8	1.4	1.0	.76	.50	.30	.17	.09	.04	0
8	O	+	+	.01	.02	.05	.11	.22	.40	.70	1.1	1.7	2.5	3.3	4.2	4.9	5.4	5.6	5.4	4.9	4.2	3.3	2.5	1.7	1.1	.70	.40	.22	.11	0
9	O	+	+	.02	.04	.10	.21	.41	.75	1.3	2.1	3.1	4.5	6.0	7.6	8.9	10	10	10	8.9	7.6	6.0	4.5	3.1	2.1	1.3	.75	.41	.21	0
10	O	+	.01	.03	.07	.16	.33	.63	1.1	1.9	3.1	4.7	6.6	8.8	11	13	14	15	14	13	11	8.8	6.6	4.7	3.1	1.9	1.1	.63	.33	0
11	O	+	.02	.04	.10	.22	.45	.84	1.5	2.5	3.9	5.8	8.2	11	14	16	17	18	17	16	14	11	8.2	5.8	3.9	2.5	1.5	.84	.45	0
12	O	.01	.03	.06	.14	.28	.55	1.0	1.7	2.8	4.4	6.5	9.0	12	15	17	18	19	18	17	15	12	9.0	6.5	4.4	2.8	1.7	1.0	.55	0
13	O	.01	.03	.08	.17	.34	.63	1.1	1.9	3.0	4.6	6.7	9.2	12	14	17	18	19	18	17	14	12	9.2	6.7	4.6	3.0	1.9	1.1	.63	0
14	O	.02	.04	.09	.19	.37	.68	1.1	1.9	3.1	4.6	6.5	8.8	11	14	16	17	17	17	16	14	11	8.8	6.5	4.6	3.1	1.9	1.1	.68	0
15	O	.02	.05	.10	.20	.38	.68	1.1	1.9	2.9	4.3	6.0	8.0	10	12	14	15	15	15	14	12	10	8.0	6.0	4.3	2.9	1.9	1.1	.68	0
16	O	.02	.05	.10	.19	.36	.63	1.0	1.6	2.5	3.7	5.1	6.8	8.5	10	12	12	13	12	12	10	8.5	6.8	5.1	3.7	2.5	1.6	1.0	.63	0
17	O	.02	.04	.09	.17	.30	.53	.88	1.3	2.0	3.0	4.1	5.3	6.7	7.9	8.9	10	10	10	8.9	7.9	6.7	5.3	4.1	3.0	2.0	1.3	.88	.53	0
18	O	.01	.03	.07	.13	.23	.40	.66	1.0	1.5	2.2	2.9	3.8	4.8	5.6	6.3	6.8	7.0	6.8	6.3	5.6	4.8	3.8	2.9	2.2	1.5	1.0	.66	.40	0
19	O	.01	.02	.05	.09	.16	.28	.45	.70	1.0	1.4	1.9	2.5	3.1	3.6	4.1	4.4	4.5	4.4	4.1	3.6	3.1	2.5	1.9	1.4	1.0	.70	.45	.28	0
20	O	+	.01	.03	.06	.10	.17	.28	.43	.63	.88	1.1	1.5	1.8	2.1	2.4	2.6	2.6	2.6	2.4	2.1	1.8	1.5	1.1	.88	.63	.43	.28	.17	0
21	O	+	.01	.02	.03	.06	.10	.15	.24	.34	.48	.64	.82	1.0	1.1	1.3	1.3	1.4	1.3	1.3	1.1	1.0	.82	.64	.48	.34	.24	.15	.10	0
22	O	+	+	.01	.01	.03	.05	.08	.12	.17	.24	.32	.41	.50	.58	.64	.69	.70	.69	.64	.58	.50	.41	.32	.24	.17	.12	.08	.05	0
23	O	+	+	+	+	.01	.02	.03	.05	.08	.11	.15	.19	.23	.26	.29	.31	.32	.31	.29	.26	.23	.19	.15	.11	.08	.05	.03	.02	0
24	O	+	+	+	+	+	.01	.01	.02	.03	.04	.06	.08	.09	.11	.12	.13	.13	.13	.12	.11	.09	.08	.06	.04	.03	.02	.01	.01	0
25	O	+	+	+	+	+	+	+	+	.01	.01	.02	.03	.03	.04	.04	.04	.05	.04	.04	.04	.03	.03	.02	.01	.01	+	+	+	+
26	O	.	+	+	+	+	+	+	+	+	+	+	.01	.01	.01	.01	.01	.01	.01	.01	.01	.01	.01	+	+	+	+	+	+	+
27	O	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+
28	O	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+
29	O	.	.	.	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	0
30	O	.	.	.	.	.	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	0
31	O	.	.	.	.	.	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	0
32	O	.	.	.	.	.	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	0
33	O	.	.	.	.	.	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	0
34	O	.	.	.	.	.	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	0
35	O	.	.	.	.	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	0
36	O	.	.	.	.	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	0
37	O	.	.	.	.	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	0
38	O	.	.	.	.	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	0
39	O	.	.	.	.	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	0
40	O	.	.	.	.	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	0
41	O	.	.	.	.	.	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	0
42	O	.	.	.	.	.	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	0
43	O	.	.	.	.	.	.	.	.	.	.	.	.	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	0
44	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O

SMALL CLOUDS AT 3600.00 SECONDS ELAPSED TIME FOR CLAY

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID	LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	2014.	450.0	24.31	0.0000E+00	322.9	0.0000E+00	120.0	0.340000E-04
2	2015.	450.0	21.38	0.0000E+00	353.9	0.0000E+00	120.0	0.340000E-04
3	2015.	450.0	29.61	0.0000E+00	407.5	0.0000E+00	120.0	0.340000E-04
4	2016.	450.0	37.51	0.0000E+00	515.6	0.0000E+00	120.0	0.340000E-04
5	2016.	450.0	16.31	0.0000E+00	593.8	0.0000E+00	120.0	0.340000E-04
6	2016.	450.0	7.618	0.0000E+00	641.0	0.0000E+00	120.0	0.340000E-04
7	2016.	450.0	4.412	0.0000E+00	672.2	0.0000E+00	120.0	0.340000E-04
8	2015.	450.0	3.093	0.0000E+00	695.9	0.0000E+00	120.0	0.340000E-04
9	2015.	450.0	2.425	0.0000E+00	715.7	0.0000E+00	120.0	0.340000E-04
10	2015.	450.0	0.1537	0.0000E+00	732.8	0.0000E+00	120.0	0.340000E-04

BOTTOM ACCUMULATION OF CLAY (CU FT/GRID SQUARE) , 3600.00 SECONDS AFTER DUMP

...MULTIPLY DISPLAYED VALUES BY 1.000 (LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)

M N=	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31
2	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O
3	O	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+
4	O	.	.	.	+	+	+	+	+	+	+	.01	.02	.02	.03	.04	.04	.04	.04	.04	.03	.02	.02	.01	+	+	+	+	+	+
5	O	.	+	+	+	+	+	+	.01	.02	.04	.06	.09	.13	.16	.19	.21	.22	.21	.19	.16	.13	.09	.06	.04	.02	.01	+	+	+
6	O	+	+	+	+	+	.01	.03	.06	.10	.17	.26	.37	.50	.63	.74	.82	.85	.82	.74	.63	.50	.37	.26	.17	.10	.06	.03	.01	0
7	O	+	+	+	.01	.02	.04	.09	.17	.30	.50	.76	1.0	1.4	1.8	2.1	2.4	2.4	2.4	2.1	1.8	1.4	1.0	.76	.50	.30	.17	.09	.04	0
8	O	+	+	.01	.02	.05	.11	.22	.40	.70	1.1	1.7	2.5	3.3	4.2	4.9	5.4	5.6	5.4	4.9	4.2	3.3	2.5	1.7	1.1	.70	.40	.22	.11	0
9	O	+	+	.02	.04	.10	.21	.41	.75	1.3	2.1	3.1	4.5	6.0	7.6	8.9	10	10	10	8.9	7.6	6.0	4.5	3.1	2.1	1.3	.75	.41	.21	0
10	O	+	.01	.03	.07	.16	.33	.63	1.1	1.9	3.1	4.7	6.6	8.8	11	13	14	15	14	13	11	8.8	6.6	4.7	3.1	1.9	1.1	.63	.33	0
11	O	+	.02	.04	.10	.22	.45	.84	1.5	2.5	3.9	5.8	8.2	11	14	16	17	18	17	16	14	11	8.2	5.8	3.9	2.5	1.5	.84	.45	0
12	O	.01	.03	.06	.14	.28	.55	1.0	1.7	2.8	4.4	6.5	9.0	12	15	17	18	19	18	17	15	12	9.0	6.5	4.4	2.8	1.7	1.0	.55	0
13	O	.01	.03	.08	.17	.34	.63	1.1	1.9	3.0	4.6	6.7	9.2	12	14	17	18	19	18	17	14	12	9.2	6.7	4.6	3.0	1.9	1.1	.63	0
14	O	.02	.04	.09	.19	.37	.68	1.1	1.9	3.1	4.6	6.5	8.8	11	14	16	17	17	17	16	14	11	8.8	6.5	4.6	3.1	1.9	1.1	.68	0
15	O	.02	.05	.10	.20	.38	.68	1.1	1.9	2.9	4.3	6.0	8.0	10	12	14	15	15	15	14	12	10	8.0	6.0	4.3	2.9	1.9	1.1	.68	0
16	O	.02	.05	.10	.19	.36	.63	1.0	1.6	2.5	3.7	5.1	6.8	8.5	10	12	12	13	12	12	10	8.5	6.8	5.1	3.7	2.5	1.6	1.0	.63	0
17	O	.02	.04	.09	.17	.30	.53	.88	1.3	2.0	3.0	4.1	5.3	6.7	7.9	8.9	10	10	10	8.9	7.9	6.7	5.3	4.1	3.0	2.0	1.3	.88	.53	0
18	O	.01	.03	.07	.13	.23	.40	.66	1.0	1.5	2.2	2.9	3.8	4.8	5.6	6.3	6.8	7.0	6.8	6.3	5.6	4.8	3.8	2.9	2.2	1.5	1.0	.66	.40	0
19	O	.01	.02	.05	.09	.16	.28	.45	.70	1.0	1.4	1.9	2.5	3.1	3.6	4.1	4.4	4.5	4.4	4.1	3.6	3.1	2.5	1.9	1.4	1.0	.70	.45	.28	0
20	O	+	.01	.03	.06	.10	.17	.28	.43	.63	.88	1.1	1.5	1.8	2.1	2.4	2.6	2.6	2.6	2.4	2.1	1.8	1.5	1.1	.88	.63	.43	.28	.17	0
21	O	+	.01	.02	.03	.06	.10	.15	.24	.34	.48	.64	.82	1.0	1.1	1.3	1.3	1.4	1.3	1.3	1.1	1.0	.82	.64	.48	.34	.24	.15	.10	0
22	O	+	+	.01	.01	.03	.05	.08	.12	.17	.24	.32	.41	.50	.58	.64	.69	.70	.69	.64	.58	.50	.41	.32	.24	.17	.12	.08	.05	0
23	O	+	+	+	+	.01	.02	.03	.05	.08	.11	.15	.19	.23	.26	.29	.31	.32	.31	.29	.26	.23	.19	.15	.11	.08	.05	.03	.02	0
24	O	+	+	+	+	+	.01	.01	.02	.03	.04	.06	.08	.09	.11	.12	.13	.13	.13	.12	.11	.09	.08	.06	.04	.03	.02	.01	.01	0
25	O	+	+	+	+	+	+	+	+	.01	.01	.02	.03	.03	.04	.04	.04	.05	.04	.04	.04	.03	.03	.02	.01	.01	+	+	+	+
26	O	.	+	+	+	+	+	+	+	+	+	+	.01	.01	.01	.01	.01	.01	.01	.01	.01	.01	.01	+	+	+	+	+	+	+
27	O	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+
28	O	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+
29	O	.	.	.	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	0
30	O	.	.	.	.	.	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	0
31	O	.	.	.	.	.	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	0
32	O	.	.	.	.	.	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	0
33	O	.	.	.	.	.	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	0
34	O	.	.	.	.	.	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	0
35	O	.	.	.	.	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	0
36	O	.	.	.	.	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	0
37	O	.	.	.	.	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	0
38	O	.	.	.	.	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	0
39	O	.	.	.	.	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	0
40	O	.	.	.	.	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	0
41	O	.	.	.	.	.	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	0
42	O	.	.	.	.	.	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	0
43	O	.	.	.	.	.	.	.	.	.	.	.	.	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	0
44	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O

THICKNESS (FT) OF CLAY ACCUMULATED ON BOTTOM, 3600.00 SECONDS AFTER DUMP
...MULTIPLY DISPLAYED VALUES BY 1.000 (LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)

M N=	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31
2	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O
3	O	O	0	0	0	0	0	0	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	0
4	O	O	0	0	.	.	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	0
5	O	O	0	.	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	0
6	O	O	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	0
7	O	O	.	.	.	.	+	+	+	+	+	+	+	.01	.01	.01	.01	.01	.01	.01	.01	.01	+	+	+	+	+	+	+	0
8	O	O	.	.	.	+	+	+	+	+	+	+	.01	.01	.02	.03	.03	.03	.04	.03	.03	.03	.02	.01	.01	+	+	+	+	0
9	O	O	.	.	+	+	+	+	+	+	+	.01	.02	.03	.04	.05	.06	.07	.07	.07	.06	.05	.04	.03	.02	.01	+	+	+	0
10	O	O	.	+	+	+	+	+	+	+	.01	.02	.03	.04	.06	.07	.09	.10	.10	.10	.09	.07	.06	.04	.03	.02	.01	+	+	0
11	O	O	.	+	+	+	+	+	+	.01	.01	.02	.04	.05	.07	.09	.11	.12	.12	.12	.11	.09	.07	.05	.04	.02	.01	.01	+	0
12	O	O	.	+	+	+	+	+	+	.01	.02	.03	.04	.06	.08	.10	.12	.13	.13	.13	.12	.10	.08	.06	.04	.03	.02	.01	+	0
13	O	O	+	+	+	+	+	+	+	.01	.02	.03	.04	.06	.08	.10	.12	.13	.13	.13	.12	.10	.08	.06	.04	.03	.02	.01	+	0
14	O	O	+	+	+	+	+	+	+	.01	.02	.03	.04	.06	.08	.09	.11	.12	.12	.12	.11	.09	.08	.06	.04	.03	.02	.01	+	0
15	O	O	+	+	+	+	+	+	+	.01	.02	.03	.04	.05	.07	.08	.10	.10	.11	.10	.10	.08	.07	.05	.04	.03	.02	.01	+	0
16	O	O	+	+	+	+	+	+	+	.01	.01	.02	.03	.04	.06	.07	.08	.08	.09	.08	.08	.07	.06	.04	.03	.02	.01	.01	+	0
17	O	O	+	+	+	+	+	+	+	.01	.01	.02	.02	.03	.04	.05	.06	.06	.07	.06	.06	.05	.04	.03	.02	.02	.01	.01	+	0
18	O	O	+	+	+	+	+	+	+	+	.01	.01	.02	.02	.03	.04	.04	.04	.05	.04	.04	.04	.03	.02	.02	.01	.01	+	+	0
19	O	O	.	+	+	+	+	+	+	+	+	.01	.01	.01	.02	.02	.02	.03	.03	.03	.02	.02	.02	.01	.01	.01	+	+	+	0
20	O	O	.	+	+	+	+	+	+	+	+	+	.01	.01	.01	.01	.01	.01	.01	.01	.01	.01	.01	+	+	+	+	+	+	0
21	O	O	.	.	+	+	+	+	+	+	+	+	+	+	+	+	.01	.01	.01	+	+	+	+	+	+	+	+	+	+	0
22	O	O	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	0
23	O	O	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	0
24	O	O	.	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	0
25	O	O	.	.	.	.	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	0
26	O	O	0	.	.	.	.	.	.	.	.	.	.	.	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	0
27	O	O	0	0	0	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	0
28	O	O	0	0	0	0	0	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	0
29	O	O	0	0	0	0	0	0	0	0	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0	0
30	O	O	0	0	0	0	0	0	0	0	0	.	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0	0	0
31	O	O	0	0	0	0	0	0	0	0	0	0	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0	0	0	0
32	O	O	0	0	0	0	0	0	0	0	0	0	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0	0	0	0
33	O	O	0	0	0	0	0	0	0	0	0	0	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0	0	0	0
34	O	O	0	0	0	0	0	0	0	0	0	0	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0	0	0	0
35	O	O	0	0	0	0	0	0	0	0	0	.	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0	0	0
36	O	O	0	0	0	0	0	0	0	0	0	.	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0	0	0
37	O	O	0	0	0	0	0	0	0	0	0	.	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0	0	0
38	O	O	0	0	0	0	0	0	0	0	0	.	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0	0	0
39	O	O	0	0	0	0	0	0	0	0	0	.	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0	0	0
40	O	O	0	0	0	0	0	0	0	0	0	.	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0	0	0
41	O	O	0	0	0	0	0	0	0	0	0	0	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0	0	0
42	O	O	0	0	0	0	0	0	0	0	0	0	0	.	.	.	.	.	.	.	.	.	.	0	0	0	0	0	0	0
43	O	O	0	0	0	0	0	0	0	0	0	0	0	0	0	.	.	.	.	.	0	0	0	0	0	0	0	0	0	0
44	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O

BEGIN LONG TERM SIMULATION OF FATE OF FLUID

SUMMARY OF FLUID DISTRIBUTIONS AFTER 300.00 SEC

TOTAL FLUID FRACTION VOLUME FROM DISPOSAL (CU FT) = 5066.6

SMALL CLOUDS AT 300.00 SECONDS ELAPSED TIME FOR FLUID

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID	LOCATION OF CLOUD CENTROID DISTANCE FROM LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	473.5	450.0	5067.	0.0000E+00	344.8	90.14	29.86	0.000000E+00

SUMMARY OF FLUID DISTRIBUTIONS AFTER 600.00 SEC

TOTAL FLUID FRACTION VOLUME FROM DISPOSAL (CU FT) = 5066.6

SMALL CLOUDS AT 600.00 SECONDS ELAPSED TIME FOR FLUID

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID	LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	613.7	450.0	5067.	0.0000E+00	375.9	62.76	57.24	0.000000E+00

SUMMARY OF FLUID DISTRIBUTIONS AFTER 900.00 SEC

TOTAL FLUID FRACTION VOLUME FROM DISPOSAL (CU FT) = 5066.6

CONCENTRATIONS ABOVE BACKGROUND OF FLUID (VOLUMETRIC RATIO OF DUMP FLUID TO AMBIENT WATER) IN THE CLOUD 900.00 SECONDS AFTER DUMP

60.00 FT BELOW THE WATER SURFACE

...MULTIPLY DISPLAYED VALUES BY 0.1000E-03 (LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)

M	N=	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31
2		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8		0	0	0	+	+	+	+	+	+	+	+	+	.01	.01	.01	.01	.01	.01	.01	.01	.01	+	+	+	+	+	+	+	+	0
9		0	0	0	+	+	+	+	.01	.01	.02	.03	.03	.04	.05	.06	.06	.07	.06	.06	.05	.04	.03	.03	.02	.01	.01	+	+	+	0
10		0	0	0	+	+	.01	.02	.03	.05	.07	.10	.13	.16	.20	.22	.24	.24	.24	.22	.20	.16	.13	.10	.07	.05	.03	.02	+	+	0
11		0	0	0	.01	.02	.04	.06	.10	.15	.22	.30	.39	.48	.57	.64	.69	.71	.69	.64	.57	.48	.39	.30	.22	.15	.10	.06	+	+	0
12		0	0	0	.03	.05	.09	.15	.24	.37	.53	.72	.93	1.1	1.3	1.5	1.6	1.6	1.6	1.5	1.3	1.1	.93	.72	.53	.37	.24	.15	+	+	0
13		0	0	0	.06	.11	.19	.31	.48	.73	1.0	1.4	1.8	2.2	2.6	3.0	3.2	3.3	3.2	3.0	2.6	2.2	1.8	1.4	1.0	.73	.48	.31	+	+	0
14		0	0	0	.09	.18	.30	.50	.79	1.1	1.6	2.3	2.9	3.6	4.3	4.9	5.2	5.3	5.2	4.9	4.3	3.6	2.9	2.3	1.6	1.1	.79	.50	+	+	0
15		0	0	0	.13	.24	.41	.68	1.0	1.6	2.2	3.1	4.0	4.9	5.8	6.6	7.0	7.2	7.0	6.6	5.8	4.9	4.0	3.1	2.2	1.6	1.0	.68	+	+	0
16		0	0	0	.14	.27	.46	.76	1.1	1.7	2.5	3.4	4.4	5.5	6.5	7.3	7.9	8.0	7.9	7.3	6.5	5.5	4.4	3.4	2.5	1.7	1.1	.76	+	+	0
17		0	0	0	.13	.24	.42	.70	1.1	1.6	2.3	3.1	4.1	5.1	6.0	6.7	7.2	7.4	7.2	6.7	6.0	5.1	4.1	3.1	2.3	1.6	1.1	.70	+	+	0
18		0	0	0	.10	.19	.32	.53	.84	1.2	1.7	2.4	3.1	3.9	4.6	5.1	5.5	5.7	5.5	5.1	4.6	3.9	3.1	2.4	1.7	1.2	.84	.53	+	+	0
19		0	0	0	.06	.12	.20	.34	.53	.79	1.1	1.5	2.0	2.4	2.9	3.2	3.5	3.6	3.5	3.2	2.9	2.4	2.0	1.5	1.1	.79	.53	.34	+	+	0
20		0	0	0	.03	.06	.10	.17	.27	.41	.59	.80	1.0	1.2	1.5	1.7	1.8	1.8	1.8	1.7	1.5	1.2	1.0	.80	.59	.41	.27	.17	+	+	0
21		0	0	0	.01	.02	.04	.07	.12	.18	.25	.35	.45	.56	.66	.74	.80	.82	.80	.74	.66	.56	.45	.35	.25	.18	.12	.07	+	+	0
22		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
23		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
24		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
25		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
26		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
27		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
28		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
29		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
30		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
31		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
32		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
33		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
34		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
35		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
36		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
37		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
38		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
39		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
40		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
41		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
42		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
43		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
44		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0

CONCENTRATIONS ABOVE BACKGROUND OF FLUID (VOLUMETRIC RATIO OF DUMP FLUID TO AMBIENT WATER) IN THE CLOUD 900.00 SECONDS AFTER DUMP

119.00 FT BELOW THE WATER SURFACE

...MULTIPLY DISPLAYED VALUES BY 0.1000E-03 (LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)

M	N=	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31
2		O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O
3		O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
4		O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
5		O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
6		O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
7		O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
8		O	0	0	0	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	O
9		O	0	0	0	+	+	+	+	+	+	+	+	+	.01	.01	.01	.01	.01	.01	.01	.01	.01	+	+	+	+	+	+	+	O
10		O	0	0	0	+	+	+	+	+	.01	.01	.02	.02	.03	.04	.04	.05	.05	.05	.04	.04	.03	.02	.02	.01	.01	+	+	+	O
11		O	0	0	0	+	+	+	.01	.02	.03	.04	.06	.08	.10	.12	.13	.14	.14	.14	.13	.12	.10	.08	.06	.04	.03	.02	.01	+	O
12		O	0	0	0	+	.01	.02	.03	.05	.07	.11	.15	.19	.24	.28	.32	.34	.35	.34	.32	.28	.24	.19	.15	.11	.07	.05	.03	+	O
13		O	0	0	0	.01	.02	.04	.06	.10	.15	.21	.29	.38	.47	.56	.63	.68	.69	.68	.63	.56	.47	.38	.29	.21	.15	.10	.06	+	O
14		O	0	0	0	.02	.03	.06	.10	.16	.25	.35	.48	.62	.77	.91	1.0	1.1	1.1	1.1	1.0	.91	.77	.62	.48	.35	.25	.16	.10	+	O
15		O	0	0	0	.02	.05	.08	.14	.22	.33	.48	.65	.84	1.0	1.2	1.3	1.4	1.5	1.4	1.3	1.2	1.0	.84	.65	.48	.33	.22	.14	+	O
16		O	0	0	0	.03	.05	.09	.16	.25	.37	.53	.72	.94	1.1	1.3	1.5	1.6	1.7	1.6	1.5	1.3	1.1	.94	.72	.53	.37	.25	.16	+	O
17		O	0	0	0	.02	.05	.09	.14	.23	.34	.49	.67	.87	1.0	1.2	1.4	1.5	1.5	1.5	1.4	1.2	1.0	.87	.67	.49	.34	.23	.14	+	O
18		O	0	0	0	.02	.04	.06	.11	.17	.26	.37	.51	.66	.82	.97	1.0	1.1	1.2	1.1	1.0	.97	.82	.66	.51	.37	.26	.17	.11	+	O
19		O	0	0	0	.01	.02	.04	.07	.11	.16	.23	.32	.42	.52	.61	.69	.74	.76	.74	.69	.61	.52	.42	.32	.23	.16	.11	.07	+	O
20		O	0	0	0	+	.01	.02	.03	.05	.08	.12	.17	.22	.27	.32	.36	.38	.39	.38	.36	.32	.27	.22	.17	.12	.08	.05	.03	+	O
21		O	0	0	0	+	+	+	.01	.02	.03	.05	.07	.09	.11	.13	.15	.16	.17	.16	.15	.13	.11	.09	.07	.05	.03	.02	.01	+	O
22		O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
23		O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
24		O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
25		O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
26		O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
27		O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
28		O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
29		O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
30		O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
31		O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
32		O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
33		O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
34		O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
35		O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
36		O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
37		O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
38		O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
39		O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
40		O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
41		O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
42		O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
43		O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
44		O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O

CONCENTRATIONS ABOVE BACKGROUND OF FLUID (VOLUMETRIC RATIO OF DUMP FLUID TO AMBIENT WATER) IN THE CLOUD 900.00 SECONDS AFTER DUMP

THESE CONCENTRATIONS ARE THE MAXIMUM OCCURING IN THE WATER COLUMN AT THIS TIME

...MULTIPLY DISPLAYED VALUES BY 0.1000E-02 (LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)

M N=	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31
2	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O
3	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
4	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
5	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
6	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
7	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
8	O	0	0	0	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	O
9	O	0	0	0	+	+	+	+	+	+	+	+	+	+	+	+	+	.01	+	+	+	+	+	+	+	+	+	+	+	O
10	O	0	0	0	+	+	+	+	+	+	.01	.01	.01	.02	.02	.03	.03	.03	.03	.03	.02	.02	.01	.01	.01	+	+	+	+	O
11	O	0	0	0	+	+	+	+	.01	.02	.03	.04	.05	.06	.08	.09	.09	.10	.09	.09	.08	.06	.05	.04	.03	.02	.01	+	+	O
12	O	0	0	0	+	+	.01	.02	.03	.05	.07	.10	.13	.16	.19	.21	.23	.23	.23	.21	.19	.16	.13	.10	.07	.05	.03	.02	+	O
13	O	0	0	0	+	.01	.02	.04	.06	.10	.14	.20	.26	.32	.38	.42	.45	.47	.45	.42	.38	.32	.26	.20	.14	.10	.06	.04	+	O
14	O	0	0	0	.01	.02	.04	.07	.11	.16	.24	.32	.42	.52	.61	.69	.74	.76	.74	.69	.61	.52	.42	.32	.24	.16	.11	.07	+	O
15	O	0	0	0	.01	.03	.05	.09	.15	.22	.32	.44	.57	.70	.83	.93	1.0	1.0	1.0	.93	.83	.70	.57	.44	.32	.22	.15	.09	+	O
16	O	0	0	0	.02	.03	.06	.10	.16	.25	.36	.49	.63	.78	.92	1.0	1.1	1.1	1.1	1.0	.92	.78	.63	.49	.36	.25	.16	.10	+	O
17	O	0	0	0	.01	.03	.06	.09	.15	.23	.33	.45	.58	.72	.85	.96	1.0	1.0	1.0	.96	.85	.72	.58	.45	.33	.23	.15	.09	+	O
18	O	0	0	0	.01	.02	.04	.07	.11	.17	.25	.34	.44	.55	.65	.73	.79	.80	.79	.73	.65	.55	.44	.34	.25	.17	.11	.07	+	O
19	O	0	0	0	+	.01	.02	.04	.07	.11	.16	.21	.28	.35	.41	.46	.50	.51	.50	.46	.41	.35	.28	.21	.16	.11	.07	.04	+	O
20	O	0	0	0	+	+	.01	.02	.03	.05	.08	.11	.14	.18	.21	.24	.26	.26	.26	.24	.21	.18	.14	.11	.08	.05	.03	.02	+	O
21	O	0	0	0	+	+	+	.01	.01	.02	.03	.04	.06	.07	.09	.10	.11	.11	.11	.10	.09	.07	.06	.04	.03	.02	.01	.01	+	O
22	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
23	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
24	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
25	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
26	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
27	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
28	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
29	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
30	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
31	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
32	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
33	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
34	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
35	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
36	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
37	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
38	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
39	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
40	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
41	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
42	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
43	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
44	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O

SMALL CLOUDS AT 900.00 SECONDS ELAPSED TIME FOR FLUID

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID	LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	753.8	450.0	5067.	0.0000E+00	407.8	35.37	84.63	0.000000E+00

SUMMARY OF FLUID DISTRIBUTIONS AFTER 1200.00 SEC

TOTAL FLUID FRACTION VOLUME FROM DISPOSAL (CU FT) = 5066.6

SMALL CLOUDS AT 1200.00 SECONDS ELAPSED TIME FOR FLUID

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID	LOCATION OF CLOUD CENTROID DISTANCE FROM LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	893.9	450.0	5067.	0.0000E+00	440.7	7.984	112.0	0.000000E+00

SUMMARY OF FLUID DISTRIBUTIONS AFTER 1500.00 SEC

TOTAL FLUID FRACTION VOLUME FROM DISPOSAL (CU FT) = 5066.6

SMALL CLOUDS AT 1500.00 SECONDS ELAPSED TIME FOR FLUID

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID	LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	1034.	450.0	5067.	0.0000E+00	474.4	0.0000E+00	120.0	0.000000E+00

SUMMARY OF FLUID DISTRIBUTIONS AFTER 1800.00 SEC

TOTAL FLUID FRACTION VOLUME FROM DISPOSAL (CU FT) = 5066.6

CONCENTRATIONS ABOVE BACKGROUND OF FLUID   (VOLUMETRIC RATIO OF DUMP FLUID TO AMBIENT WATER) IN THE CLOUD   1800.00 SECONDS AFTER DUMP

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              60.00 FT BELOW THE WATER SURFACE
 ...MULTIPLY DISPLAYED VALUES BY  0.1000E-03     (LEGEND... + = .LT. .01   . = .LT. .0001   0 = .LT. .000001)
 M N=  2   3   4   5   6   7   8   9  10  11  12  13  14  15  16  17  18  19  20  21  22  23  24  25  26  27  28  29  30  31
  2 000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000
  3 OOOO   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0  00000
  4 OOOO   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0  00000
  5 OOOO   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0  00000
  6 OOOO   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0  00000
  7 OOOO   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0  00000
  8 OOOO   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0  00000
  9 OOOO   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0  00000
 10 OOOO   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0  00000
 11 OOOO   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0  00000
 12 OOOO   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0  00000
 13 OOOO   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0  00000
 14 OOOO   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0  00000
 15 OOOO   0   +   +   +   +   +   +   +   + .01 .01 .01 .01 .01 .02 .02 .02 .02 .02 .01 .01 .01 .01 .01   +   +   +  +0000
 16 OOOO   0   +   +   +   + .01 .01 .01 .02 .03 .03 .04 .05 .05 .06 .06 .06 .06 .06 .05 .05 .04 .03 .03 .02 .01 .01 .010000
 17 OOOO   0   +   + .01 .01 .02 .03 .05 .06 .08 .10 .11 .13 .15 .16 .17 .17 .17 .16 .15 .13 .11 .10 .08 .06 .05 .03 .020000
 18 OOOO   0 .01 .02 .03 .04 .06 .08 .11 .15 .19 .23 .27 .31 .35 .38 .40 .40 .40 .38 .35 .31 .27 .23 .19 .15 .11 .08 .060000
 19 OOOO   0 .02 .04 .06 .09 .13 .18 .24 .31 .39 .48 .57 .65 .73 .79 .82 .84 .82 .79 .73 .65 .57 .48 .39 .31 .24 .18 .130000
 20 OOOO   0 .05 .07 .11 .17 .24 .33 .45 .58 .73 .89 1.0 1.2 1.3 1.4 1.5 1.5 1.5 1.4 1.3 1.2 1.0 .89 .73 .58 .45 .33 .240000
 21 OOOO   0 .08 .12 .19 .28 .39 .54 .73 .94 1.1 1.4 1.7 1.9 2.1 2.3 2.4 2.4 2.4 2.3 2.1 1.9 1.7 1.4 1.1 .94 .73 .54 .390000
 22 OOOO   0 .11 .18 .27 .40 .57 .78 1.0 1.3 1.7 2.0 2.4 2.8 3.1 3.3 3.5 3.5 3.5 3.3 3.1 2.8 2.4 2.0 1.7 1.3 1.0 .78 .570000
 23 OOOO   0 .15 .23 .35 .51 .72 .99 1.3 1.7 2.1 2.6 3.1 3.5 3.9 4.2 4.4 4.5 4.4 4.2 3.9 3.5 3.1 2.6 2.1 1.7 1.3 .99 .720000
 24 OOOO   0 .16 .26 .39 .57 .81 1.1 1.5 1.9 2.4 2.9 3.5 4.0 4.4 4.8 5.0 5.1 5.0 4.8 4.4 4.0 3.5 2.9 2.4 1.9 1.5 1.1 .810000
 25 OOOO   0 .16 .26 .39 .57 .81 1.1 1.4 1.9 2.4 2.9 3.5 4.0 4.4 4.8 5.0 5.1 5.0 4.8 4.4 4.0 3.5 2.9 2.4 1.9 1.4 1.1 .810000
 26 OOOO   0 .14 .23 .34 .51 .72 .99 1.3 1.7 2.1 2.6 3.0 3.5 3.9 4.2 4.4 4.5 4.4 4.2 3.9 3.5 3.0 2.6 2.1 1.7 1.3 .99 .720000
 27 OOOO   0 .11 .18 .27 .39 .56 .77 1.0 1.3 1.6 2.0 2.4 2.7 3.0 3.3 3.4 3.5 3.4 3.3 3.0 2.7 2.4 2.0 1.6 1.3 1.0 .77 .560000
 28 OOOO   0 .08 .12 .18 .27 .39 .53 .71 .93 1.1 1.4 1.6 1.9 2.1 2.3 2.4 2.4 2.4 2.3 2.1 1.9 1.6 1.4 1.1 .93 .71 .53 .390000
 29 OOOO   0 .04 .07 .11 .17 .24 .33 .44 .57 .71 .87 1.0 1.1 1.3 1.4 1.4 1.5 1.4 1.4 1.3 1.1 1.0 .87 .71 .57 .44 .33 .240000
 30 OOOO   0 .02 .04 .06 .09 .13 .18 .24 .31 .39 .47 .56 .64 .71 .77 .80 .82 .80 .77 .71 .64 .56 .47 .39 .31 .24 .18 .130000
 31 OOOO   0 .01 .02 .03 .04 .06 .08 .11 .15 .18 .22 .27 .31 .34 .37 .39 .39 .39 .37 .34 .31 .27 .22 .18 .15 .11 .08 .060000
 32 OOOO   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0  00000
 33 OOOO   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0  00000
 34 OOOO   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0  00000
 35 OOOO   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0  00000
 36 OOOO   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0  00000
 37 OOOO   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0  00000
 38 OOOO   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0  00000
 39 OOOO   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0  00000
 40 OOOO   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0  00000
 41 OOOO   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0  00000
 42 OOOO   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0  00000
 43 OOOO   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0  00000
 44 000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000
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CONCENTRATIONS ABOVE BACKGROUND OF FLUID (VOLUMETRIC RATIO OF DUMP FLUID TO AMBIENT WATER) IN THE CLOUD 1800.00 SECONDS AFTER DUMP

119.00 FT BELOW THE WATER SURFACE

...MULTIPLY DISPLAYED VALUES BY 0.1000E-04 (LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)

M	N=	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31
2		O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O
3		0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
4		0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
5		0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
6		0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
7		0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
8		0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
9		0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
10		0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
11		0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
12		0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
13		0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
14		0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
15		0000	0	+	+	+	+	+	+	+	.01	.01	.01	.02	.02	.02	.03	.03	.03	.03	.03	.02	.02	.02	.01	.01	.01	+	+	+	+0000
16		0000	0	+	+	+	.01	.01	.02	.02	.03	.04	.05	.06	.07	.08	.09	.09	.09	.09	.09	.08	.07	.06	.05	.04	.03	.02	.02	.010000
17		0000	0	+	.01	.01	.02	.04	.05	.07	.09	.11	.14	.17	.19	.21	.23	.24	.25	.24	.23	.21	.19	.17	.14	.11	.09	.07	.05	.040000
18		0000	0	.01	.03	.04	.06	.09	.12	.17	.22	.27	.34	.40	.46	.51	.55	.57	.58	.57	.55	.51	.46	.40	.34	.27	.22	.17	.12	.090000
19		0000	0	.04	.06	.09	.13	.19	.26	.35	.46	.57	.70	.83	.95	1.0	1.1	1.1	1.2	1.1	1.1	1.0	.95	.83	.70	.57	.46	.35	.26	.190000
20		0000	0	.07	.11	.17	.25	.35	.48	.65	.84	1.0	1.2	1.5	1.7	1.9	2.0	2.1	2.2	2.1	2.0	1.9	1.7	1.5	1.2	1.0	.84	.65	.48	.350000
21		0000	0	.11	.18	.27	.40	.57	.79	1.0	1.3	1.7	2.0	2.4	2.8	3.1	3.3	3.5	3.6	3.5	3.3	3.1	2.8	2.4	2.0	1.7	1.3	1.0	.79	.570000
22		0000	0	.17	.26	.39	.58	.82	1.1	1.5	1.9	2.4	2.9	3.5	4.0	4.5	4.8	5.0	5.1	5.0	4.8	4.5	4.0	3.5	2.9	2.4	1.9	1.5	1.1	.820000
23		0000	0	.21	.33	.50	.74	1.0	1.4	1.9	2.4	3.1	3.8	4.5	5.1	5.7	6.1	6.4	6.5	6.4	6.1	5.7	5.1	4.5	3.8	3.1	2.4	1.9	1.4	1.00000
24		0000	0	.24	.37	.57	.83	1.1	1.6	2.1	2.8	3.5	4.2	5.0	5.8	6.4	6.9	7.3	7.4	7.3	6.9	6.4	5.8	5.0	4.2	3.5	2.8	2.1	1.6	1.10000
25		0000	0	.24	.37	.57	.83	1.1	1.6	2.1	2.8	3.5	4.2	5.0	5.8	6.4	6.9	7.2	7.4	7.2	6.9	6.4	5.8	5.0	4.2	3.5	2.8	2.1	1.6	1.10000
26		0000	0	.21	.33	.50	.73	1.0	1.4	1.9	2.4	3.1	3.7	4.4	5.1	5.7	6.1	6.4	6.5	6.4	6.1	5.7	5.1	4.4	3.7	3.1	2.4	1.9	1.4	1.00000
27		0000	0	.16	.26	.39	.57	.81	1.1	1.5	1.9	2.4	2.9	3.5	4.0	4.4	4.8	5.0	5.1	5.0	4.8	4.4	4.0	3.5	2.9	2.4	1.9	1.5	1.1	.810000
28		0000	0	.11	.18	.27	.40	.56	.78	1.0	1.3	1.6	2.0	2.4	2.7	3.0	3.3	3.4	3.5	3.4	3.3	3.0	2.7	2.4	2.0	1.6	1.3	1.0	.78	.560000
29		0000	0	.07	.11	.16	.24	.34	.47	.63	.82	1.0	1.2	1.4	1.7	1.9	2.0	2.1	2.1	2.1	2.0	1.9	1.7	1.4	1.2	1.0	.82	.63	.47	.340000
30		0000	0	.03	.06	.09	.13	.18	.26	.34	.45	.56	.68	.81	.93	1.0	1.1	1.1	1.1	1.1	1.1	1.0	.93	.81	.68	.56	.45	.34	.26	.180000
31		0000	0	.01	.02	.04	.06	.09	.12	.16	.21	.27	.33	.39	.44	.49	.53	.56	.57	.56	.53	.49	.44	.39	.33	.27	.21	.16	.12	.090000
32		0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
33		0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
34		0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
35		0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
36		0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
37		0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
38		0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
39		0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
40		0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
41		0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
42		0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
43		0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
44		O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O

CONCENTRATIONS ABOVE BACKGROUND OF FLUID (VOLUMETRIC RATIO OF DUMP FLUID TO AMBIENT WATER) IN THE CLOUD 1800.00 SECONDS AFTER DUMP

THESE CONCENTRATIONS ARE THE MAXIMUM OCCURING IN THE WATER COLUMN AT THIS TIME

...MULTIPLY DISPLAYED VALUES BY 0.1000E-03 (LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)

M N=	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31
2	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O
3	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O
4	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O
5	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O
6	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O
7	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O
8	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O
9	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O
10	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O
11	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O
12	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O
13	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O
14	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O
15	O	+	+	+	+	+	+	+	+	.01	.01	.01	.01	.01	.02	.02	.02	.02	.02	.01	.01	.01	.01	.01	+	+	+	+	+	+
16	O	+	+	+	+	.01	.01	.01	.02	.03	.03	.04	.05	.05	.06	.06	.06	.06	.06	.05	.05	.04	.03	.03	.02	.01	.01	.01	.01	.01
17	O	+	+	.01	.01	.02	.03	.05	.06	.08	.10	.11	.13	.15	.16	.17	.17	.17	.16	.15	.13	.11	.10	.08	.06	.05	.03	.02	.02	.02
18	O	.01	.02	.03	.04	.06	.08	.11	.15	.19	.23	.27	.31	.35	.38	.40	.40	.40	.38	.35	.31	.27	.23	.19	.15	.11	.08	.06	.06	.06
19	O	.02	.04	.06	.09	.13	.18	.24	.31	.39	.48	.57	.65	.73	.79	.82	.84	.82	.79	.73	.65	.57	.48	.39	.31	.24	.18	.13	.13	.13
20	O	.05	.07	.11	.17	.24	.33	.45	.58	.73	.89	1.0	1.2	1.3	1.4	1.5	1.5	1.5	1.4	1.3	1.2	1.0	.89	.73	.58	.45	.33	.24	.24	.24
21	O	.08	.12	.19	.28	.39	.54	.73	.94	1.1	1.4	1.7	1.9	2.1	2.3	2.4	2.4	2.4	2.4	2.3	2.1	1.9	1.7	1.4	1.1	.94	.73	.54	.39	.39
22	O	.11	.18	.27	.40	.57	.78	1.0	1.3	1.7	2.0	2.4	2.8	3.1	3.3	3.5	3.5	3.5	3.3	3.1	2.8	2.4	2.0	1.7	1.3	1.0	.78	.57	.57	.57
23	O	.15	.23	.35	.51	.72	.99	1.3	1.7	2.1	2.6	3.1	3.5	3.9	4.2	4.4	4.5	4.4	4.2	3.9	3.5	3.1	2.6	2.1	1.7	1.3	.99	.72	.72	.72
24	O	.16	.26	.39	.57	.81	1.1	1.5	1.9	2.4	2.9	3.5	4.0	4.4	4.8	5.0	5.1	5.0	4.8	4.4	4.0	3.5	2.9	2.4	1.9	1.5	1.1	.81	.81	.81
25	O	.16	.26	.39	.57	.81	1.1	1.4	1.9	2.4	2.9	3.5	4.0	4.4	4.8	5.0	5.1	5.0	4.8	4.4	4.0	3.5	2.9	2.4	1.9	1.4	1.1	.81	.81	.81
26	O	.14	.23	.34	.51	.72	.99	1.3	1.7	2.1	2.6	3.0	3.5	3.9	4.2	4.4	4.5	4.4	4.2	3.9	3.5	3.0	2.6	2.1	1.7	1.3	.99	.72	.72	.72
27	O	.11	.18	.27	.39	.56	.77	1.0	1.3	1.6	2.0	2.4	2.7	3.0	3.3	3.4	3.5	3.4	3.3	3.0	2.7	2.4	2.0	1.6	1.3	1.0	.77	.56	.56	.56
28	O	.08	.12	.18	.27	.39	.53	.71	.93	1.1	1.4	1.6	1.9	2.1	2.3	2.4	2.4	2.4	2.3	2.1	1.9	1.6	1.4	1.1	.93	.71	.53	.39	.39	.39
29	O	.04	.07	.11	.17	.24	.33	.44	.57	.71	.87	1.0	1.1	1.3	1.4	1.4	1.5	1.4	1.4	1.3	1.1	1.0	.87	.71	.57	.44	.33	.24	.24	.24
30	O	.02	.04	.06	.09	.13	.18	.24	.31	.39	.47	.56	.64	.71	.77	.80	.82	.80	.77	.71	.64	.56	.47	.39	.31	.24	.18	.13	.13	.13
31	O	.01	.02	.03	.04	.06	.08	.11	.15	.18	.22	.27	.31	.34	.37	.39	.39	.39	.37	.34	.31	.27	.22	.18	.15	.11	.08	.06	.06	.06
32	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O
33	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O
34	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O
35	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O
36	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O
37	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O
38	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O
39	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O
40	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O
41	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O
42	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O
43	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O
44	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O

SMALL CLOUDS AT 1800.00 SECONDS ELAPSED TIME FOR FLUID

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID	LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	1174.	450.0	5067.	0.0000E+00	508.9	0.0000E+00	120.0	0.000000E+00

SUMMARY OF FLUID DISTRIBUTIONS AFTER 2100.00 SEC

TOTAL FLUID FRACTION VOLUME FROM DISPOSAL (CU FT) = 5066.6

SMALL CLOUDS AT 2100.00 SECONDS ELAPSED TIME FOR FLUID

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID	LOCATION OF CLOUD CENTROID DISTANCE FROM LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	1314.	450.0	5067.	0.0000E+00	544.3	0.0000E+00	120.0	0.000000E+00

SUMMARY OF FLUID DISTRIBUTIONS AFTER 2400.00 SEC

TOTAL FLUID FRACTION VOLUME FROM DISPOSAL (CU FT) = 5066.6

SMALL CLOUDS AT 2400.00 SECONDS ELAPSED TIME FOR FLUID

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID	LOCATION OF CLOUD CENTROID DISTANCE FROM LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	1454.	450.0	5067.	0.0000E+00	580.4	0.0000E+00	120.0	0.000000E+00

SUMMARY OF FLUID DISTRIBUTIONS AFTER 2700.00 SEC

TOTAL FLUID FRACTION VOLUME FROM DISPOSAL (CU FT) = 5066.6

CONCENTRATIONS ABOVE BACKGROUND OF FLUID (VOLUMETRIC RATIO OF DUMP FLUID TO AMBIENT WATER) IN THE CLOUD 2700.00 SECONDS AFTER DUMP

60.00 FT BELOW THE WATER SURFACE

...MULTIPLY DISPLAYED VALUES BY 0.1000E-03 (LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)

M N=	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31
2	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O
3	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
4	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
5	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
6	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
7	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
8	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
9	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
10	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
11	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
12	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
13	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
14	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
15	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
16	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
17	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
18	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
19	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
20	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
21	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
22	O	+	+	+	+	+	+	+	.01	.01	.01	.01	.02	.02	.02	.02	.02	.02	.02	.02	.02	.02	.02	.01	.01	.01	.01	+	+	O
23	O	+	+	+	.01	.01	.01	.02	.02	.03	.03	.04	.04	.05	.05	.06	.06	.06	.06	.06	.05	.05	.04	.04	.03	.03	.02	.02	.01	O
24	O	+	.01	.01	.02	.03	.03	.04	.05	.07	.08	.09	.10	.11	.12	.13	.13	.13	.13	.13	.12	.11	.10	.09	.08	.07	.05	.04	.03	O
25	O	.01	.02	.03	.04	.06	.07	.09	.11	.14	.16	.18	.21	.23	.24	.26	.26	.27	.26	.26	.24	.23	.21	.18	.16	.14	.11	.09	.07	O
26	O	.03	.04	.06	.08	.11	.14	.17	.21	.25	.30	.34	.38	.42	.45	.47	.49	.49	.49	.47	.45	.42	.38	.34	.30	.25	.21	.17	.14	O
27	O	.06	.08	.11	.14	.19	.24	.30	.36	.43	.51	.58	.65	.71	.77	.81	.83	.84	.83	.81	.77	.71	.65	.58	.51	.43	.36	.30	.24	O
28	O	.09	.12	.17	.23	.29	.37	.47	.57	.68	.79	.91	1.0	1.1	1.2	1.2	1.3	1.3	1.3	1.2	1.2	1.1	1.0	.91	.79	.68	.57	.47	.37	O
29	O	.13	.18	.25	.33	.42	.54	.67	.82	.98	1.1	1.3	1.4	1.6	1.7	1.8	1.8	1.8	1.8	1.8	1.7	1.6	1.4	1.3	1.1	.98	.82	.67	.54	O
30	O	.17	.24	.33	.43	.56	.72	.89	1.0	1.2	1.5	1.7	1.9	2.1	2.2	2.4	2.4	2.5	2.4	2.4	2.2	2.1	1.9	1.7	1.5	1.2	1.0	.89	.72	O
31	O	.21	.30	.40	.53	.69	.87	1.0	1.3	1.5	1.8	2.1	2.3	2.5	2.7	2.9	3.0	3.0	3.0	2.9	2.7	2.5	2.3	2.1	1.8	1.5	1.3	1.0	.87	O
32	O	.24	.33	.45	.60	.77	.98	1.2	1.4	1.7	2.0	2.3	2.6	2.9	3.1	3.2	3.3	3.4	3.3	3.2	3.1	2.9	2.6	2.3	2.0	1.7	1.4	1.2	.98	O
33	O	.25	.34	.46	.61	.80	1.0	1.2	1.5	1.8	2.1	2.4	2.7	2.9	3.2	3.3	3.4	3.5	3.4	3.3	3.2	2.9	2.7	2.4	2.1	1.8	1.5	1.2	1.00	O
34	O	.24	.33	.44	.58	.76	.96	1.1	1.4	1.7	2.0	2.3	2.5	2.8	3.0	3.2	3.3	3.3	3.3	3.2	3.0	2.8	2.5	2.3	2.0	1.7	1.4	1.1	.960	O
35	O	.21	.28	.39	.51	.66	.84	1.0	1.2	1.5	1.7	2.0	2.2	2.4	2.6	2.8	2.9	2.9	2.9	2.8	2.6	2.4	2.2	2.0	1.7	1.5	1.2	1.0	.840	O
36	O	.16	.23	.31	.41	.53	.68	.84	1.0	1.2	1.4	1.6	1.8	2.0	2.1	2.2	2.3	2.3	2.3	2.2	2.1	2.0	1.8	1.6	1.4	1.2	1.0	.84	.680	O
37	O	.12	.17	.23	.30	.39	.50	.62	.76	.91	1.0	1.2	1.3	1.4	1.6	1.6	1.7	1.7	1.7	1.6	1.6	1.4	1.3	1.2	1.0	.91	.76	.62	.500	O
38	O	.08	.11	.16	.21	.27	.34	.43	.52	.62	.72	.83	.93	1.0	1.0	1.1	1.1	1.2	1.1	1.1	1.0	1.0	.93	.83	.72	.62	.52	.43	.340	O
39	O	.05	.07	.10	.13	.17	.21	.27	.32	.39	.45	.52	.58	.64	.69	.72	.75	.75	.75	.72	.69	.64	.58	.52	.45	.39	.32	.27	.210	O
40	O	.03	.04	.05	.07	.09	.12	.15	.19	.22	.26	.30	.34	.37	.40	.42	.43	.44	.43	.42	.40	.37	.34	.30	.26	.22	.19	.15	.120	O
41	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
42	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
43	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
44	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O

CONCENTRATIONS ABOVE BACKGROUND OF FLUID (VOLUMETRIC RATIO OF DUMP FLUID TO AMBIENT WATER) IN THE CLOUD 2700.00 SECONDS AFTER DUMP

119.00 FT BELOW THE WATER SURFACE

...MULTIPLY DISPLAYED VALUES BY 0.1000E-04 (LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)

M	N= 2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30 31
2	OOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOO																												
3	OOOO	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
4	OOOO	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
5	OOOO	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
6	OOOO	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
7	OOOO	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
8	OOOO	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
9	OOOO	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
10	OOOO	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
11	OOOO	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
12	OOOO	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
13	OOOO	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
14	OOOO	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
15	OOOO	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
16	OOOO	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
17	OOOO	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
18	OOOO	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
19	OOOO	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
20	OOOO	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
21	OOOO	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
22	OOOO	+	+	+	+	+	.01	.01	.01	.01	.02	.02	.02	.03	.03	.03	.03	.03	.03	.03	.03	.03	.02	.02	.02	.01	.01	.01	.010000
23	OOOO	+	+	.01	.01	.02	.02	.03	.03	.04	.05	.06	.07	.07	.08	.08	.08	.09	.08	.08	.08	.07	.07	.06	.05	.04	.03	.03	.020000
24	OOOO	.01	.01	.02	.03	.04	.05	.07	.08	.10	.11	.13	.15	.16	.17	.18	.19	.19	.19	.18	.17	.16	.15	.13	.11	.10	.08	.07	.050000
25	OOOO	.02	.03	.05	.06	.08	.11	.14	.17	.20	.23	.27	.30	.33	.35	.37	.38	.39	.38	.37	.35	.33	.30	.27	.23	.20	.17	.14	.110000
26	OOOO	.05	.07	.09	.12	.16	.20	.25	.31	.37	.43	.49	.55	.61	.65	.69	.71	.72	.71	.69	.65	.61	.55	.49	.43	.37	.31	.25	.200000
27	OOOO	.08	.12	.16	.21	.27	.35	.43	.53	.63	.73	.84	.94	1.0	1.1	1.1	1.2	1.2	1.2	1.1	1.1	1.0	.94	.84	.73	.63	.53	.43	.350000
28	OOOO	.13	.18	.25	.33	.43	.54	.68	.82	.98	1.1	1.3	1.4	1.6	1.7	1.8	1.8	1.9	1.8	1.8	1.7	1.6	1.4	1.3	1.1	.98	.82	.68	.540000
29	OOOO	.19	.26	.36	.48	.62	.78	.97	1.1	1.4	1.6	1.8	2.1	2.3	2.4	2.6	2.7	2.7	2.7	2.6	2.4	2.3	2.1	1.8	1.6	1.4	1.1	.97	.780000
30	OOOO	.25	.35	.48	.63	.82	1.0	1.2	1.5	1.8	2.1	2.4	2.7	3.0	3.3	3.4	3.5	3.6	3.5	3.4	3.3	3.0	2.7	2.4	2.1	1.8	1.5	1.2	1.00000
31	OOOO	.31	.43	.58	.77	1.0	1.2	1.5	1.9	2.2	2.6	3.0	3.4	3.7	4.0	4.2	4.3	4.4	4.3	4.2	4.0	3.7	3.4	3.0	2.6	2.2	1.9	1.5	1.20000
32	OOOO	.35	.48	.65	.86	1.1	1.4	1.7	2.1	2.5	2.9	3.4	3.8	4.1	4.5	4.7	4.8	4.9	4.8	4.7	4.5	4.1	3.8	3.4	2.9	2.5	2.1	1.7	1.40000
33	OOOO	.36	.50	.67	.89	1.1	1.4	1.8	2.2	2.6	3.0	3.5	3.9	4.3	4.6	4.9	5.0	5.1	5.0	4.9	4.6	4.3	3.9	3.5	3.0	2.6	2.2	1.8	1.40000
34	OOOO	.34	.47	.64	.85	1.1	1.3	1.7	2.1	2.5	2.9	3.3	3.7	4.1	4.4	4.6	4.8	4.8	4.8	4.6	4.4	4.1	3.7	3.3	2.9	2.5	2.1	1.7	1.30000
35	OOOO	.30	.41	.56	.74	.96	1.2	1.5	1.8	2.2	2.5	2.9	3.2	3.6	3.8	4.0	4.2	4.2	4.2	4.0	3.8	3.6	3.2	2.9	2.5	2.2	1.8	1.5	1.20000
36	OOOO	.24	.33	.45	.60	.77	.98	1.2	1.4	1.7	2.0	2.3	2.6	2.9	3.1	3.2	3.3	3.4	3.3	3.2	3.1	2.9	2.6	2.3	2.0	1.7	1.4	1.2	.980000
37	OOOO	.18	.25	.33	.44	.57	.73	.90	1.1	1.3	1.5	1.7	1.9	2.1	2.3	2.4	2.5	2.5	2.5	2.4	2.3	2.1	1.9	1.7	1.5	1.3	1.1	.90	.730000
38	OOOO	.12	.17	.23	.30	.39	.50	.62	.75	.90	1.0	1.2	1.3	1.4	1.5	1.6	1.7	1.7	1.7	1.6	1.5	1.4	1.3	1.2	1.0	.90	.75	.62	.500000
39	OOOO	.07	.10	.14	.19	.24	.31	.39	.47	.56	.66	.75	.84	.93	1.0	1.0	1.0	1.0	1.0	1.0	1.0	.93	.84	.75	.66	.56	.47	.39	.310000
40	OOOO	.04	.06	.08	.11	.14	.18	.22	.27	.32	.38	.43	.49	.53	.58	.61	.63	.63	.63	.61	.58	.53	.49	.43	.38	.32	.27	.22	.180000
41	OOOO	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
42	OOOO	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
43	OOOO	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
44	OOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOO																												

CONCENTRATIONS ABOVE BACKGROUND OF FLUID (VOLUMETRIC RATIO OF DUMP FLUID TO AMBIENT WATER) IN THE CLOUD 2700.00 SECONDS AFTER DUMP

THESE CONCENTRATIONS ARE THE MAXIMUM OCCURING IN THE WATER COLUMN AT THIS TIME

...MULTIPLY DISPLAYED VALUES BY 0.1000E-03 (LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)

M N=	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31
2	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O
3	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
18	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
19	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
20	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
21	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
22	O	+	+	+	+	+	+	+	.01	.01	.01	.01	.02	.02	.02	.02	.02	.02	.02	.02	.02	.02	.02	.01	.01	.01	.01	+	+0	0
23	O	+	+	+	.01	.01	.01	.02	.02	.03	.03	.04	.04	.05	.05	.06	.06	.06	.06	.06	.05	.05	.04	.04	.03	.03	.02	.02	.01	0
24	O	+	.01	.01	.02	.03	.03	.04	.05	.07	.08	.09	.10	.11	.12	.13	.13	.13	.13	.13	.12	.11	.10	.09	.08	.07	.05	.04	.03	0
25	O	.01	.02	.03	.04	.06	.07	.09	.11	.14	.16	.18	.21	.23	.24	.26	.26	.27	.26	.26	.24	.23	.21	.18	.16	.14	.11	.09	.07	0
26	O	.03	.04	.06	.08	.11	.14	.17	.21	.25	.30	.34	.38	.42	.45	.47	.49	.49	.49	.47	.45	.42	.38	.34	.30	.25	.21	.17	.14	0
27	O	.06	.08	.11	.14	.19	.24	.30	.36	.43	.51	.58	.65	.71	.77	.81	.83	.84	.83	.81	.77	.71	.65	.58	.51	.43	.36	.30	.24	0
28	O	.09	.12	.17	.23	.29	.37	.47	.57	.68	.79	.91	1.0	1.1	1.2	1.2	1.3	1.3	1.3	1.2	1.2	1.1	1.0	.91	.79	.68	.57	.47	.37	0
29	O	.13	.18	.25	.33	.42	.54	.67	.82	.98	1.1	1.3	1.4	1.6	1.7	1.8	1.8	1.8	1.8	1.8	1.7	1.6	1.4	1.3	1.1	.98	.82	.67	.54	0
30	O	.17	.24	.33	.43	.56	.72	.89	1.0	1.2	1.5	1.7	1.9	2.1	2.2	2.4	2.4	2.5	2.4	2.4	2.2	2.1	1.9	1.7	1.5	1.2	1.0	.89	.72	0
31	O	.21	.30	.40	.53	.69	.87	1.0	1.3	1.5	1.8	2.1	2.3	2.5	2.7	2.9	3.0	3.0	3.0	2.9	2.7	2.5	2.3	2.1	1.8	1.5	1.3	1.0	.87	0
32	O	.24	.33	.45	.60	.77	.98	1.2	1.4	1.7	2.0	2.3	2.6	2.9	3.1	3.2	3.3	3.4	3.3	3.2	3.1	2.9	2.6	2.3	2.0	1.7	1.4	1.2	.98	0
33	O	.25	.34	.46	.61	.80	1.0	1.2	1.5	1.8	2.1	2.4	2.7	2.9	3.2	3.3	3.4	3.5	3.4	3.3	3.2	2.9	2.7	2.4	2.1	1.8	1.5	1.2	1.0	0
34	O	.24	.33	.44	.58	.76	.96	1.1	1.4	1.7	2.0	2.3	2.5	2.8	3.0	3.2	3.3	3.3	3.3	3.2	3.0	2.8	2.5	2.3	2.0	1.7	1.4	1.1	.96	0
35	O	.21	.28	.39	.51	.66	.84	1.0	1.2	1.5	1.7	2.0	2.2	2.4	2.6	2.8	2.9	2.9	2.9	2.8	2.6	2.4	2.2	2.0	1.7	1.5	1.2	1.0	.84	0
36	O	.16	.23	.31	.41	.53	.68	.84	1.0	1.2	1.4	1.6	1.8	2.0	2.1	2.2	2.3	2.3	2.3	2.2	2.1	2.0	1.8	1.6	1.4	1.2	1.0	.84	.68	0
37	O	.12	.17	.23	.30	.39	.50	.62	.76	.91	1.0	1.2	1.3	1.4	1.6	1.6	1.7	1.7	1.7	1.6	1.6	1.4	1.3	1.2	1.0	.91	.76	.62	.50	0
38	O	.08	.11	.16	.21	.27	.34	.43	.52	.62	.72	.83	.93	1.0	1.0	1.1	1.1	1.2	1.1	1.1	1.0	1.0	.93	.83	.72	.62	.52	.43	.34	0
39	O	.05	.07	.10	.13	.17	.21	.27	.32	.39	.45	.52	.58	.64	.69	.72	.75	.75	.75	.72	.69	.64	.58	.52	.45	.39	.32	.27	.21	0
40	O	.03	.04	.05	.07	.09	.12	.15	.19	.22	.26	.30	.34	.37	.40	.42	.43	.44	.43	.42	.40	.37	.34	.30	.26	.22	.19	.15	.12	0
41	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
42	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
43	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
44	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O

SMALL CLOUDS AT 2700.00 SECONDS ELAPSED TIME FOR FLUID

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID	LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	1595.	450.0	5067.	0.0000E+00	617.4	0.0000E+00	120.0	0.000000E+00

SUMMARY OF FLUID DISTRIBUTIONS AFTER 3000.00 SEC

TOTAL FLUID FRACTION VOLUME FROM DISPOSAL (CU FT) = 5066.6

SMALL CLOUDS AT 3000.00 SECONDS ELAPSED TIME FOR FLUID

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID	LOCATION OF CLOUD CENTROID DISTANCE FROM LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	1735.	450.0	5067.	0.0000E+00	655.1	0.0000E+00	120.0	0.000000E+00

SUMMARY OF FLUID DISTRIBUTIONS AFTER 3300.00 SEC

TOTAL FLUID FRACTION VOLUME FROM DISPOSAL (CU FT) = 5066.6

SMALL CLOUDS AT 3300.00 SECONDS ELAPSED TIME FOR FLUID

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID	LOCATION OF CLOUD CENTROID DISTANCE FROM LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	1875.	450.0	5067.	0.0000E+00	693.6	0.0000E+00	120.0	0.000000E+00

SUMMARY OF FLUID DISTRIBUTIONS AFTER 3600.00 SEC

TOTAL FLUID FRACTION VOLUME FROM DISPOSAL (CU FT) = 5066.6

CONCENTRATIONS ABOVE BACKGROUND OF FLUID (VOLUMETRIC RATIO OF DUMP FLUID TO AMBIENT WATER) IN THE CLOUD 3600.00 SECONDS AFTER DUMP

60.00 FT BELOW THE WATER SURFACE

...MULTIPLY DISPLAYED VALUES BY 0.1000E-03 (LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)

M	N=	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31
2	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O
3	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O
4	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O
5	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O
6	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O
7	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O
8	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O
9	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O
10	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O
11	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O
12	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O
13	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O
14	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O
15	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O
16	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O
17	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O
18	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O
19	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O
20	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O
21	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O
22	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O
23	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O
24	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O
25	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O
26	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O
27	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O
28	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O
29	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O
30	O	O	+	.	0	1	1	1	2	2	2	3	3	4	4	4	5	5	5	5	5	5	5	5	5	4	4	4	3	3	2	2	O	O	O	O	O
31	O	O	O	.	1	2	2	3	3	4	5	6	7	7	8	9	10	10	10	11	11	11	10	10	10	9	8	7	7	6	5	4	O	O	O	O	O
32	O	O	O	3	3	4	5	6	8	9	11	12	13	15	16	17	18	19	19	20	19	19	18	17	16	15	13	12	11	9	8	O	O	O	O	O	O
33	O	O	O	5	6	7	9	11	13	16	18	20	23	25	27	29	31	32	33	33	33	32	31	29	27	25	23	20	18	16	13	O	O	O	O	O	O
34	O	O	O	8	10	12	15	18	21	25	29	33	36	40	44	47	49	51	52	52	52	51	49	47	44	40	36	33	29	25	21	O	O	O	O	O	O
35	O	O	O	12	15	18	22	27	32	37	43	49	54	60	65	69	73	76	78	78	78	76	73	69	65	60	54	49	43	37	32	O	O	O	O	O	O
36	O	O	O	16	21	26	32	38	45	53	61	69	77	84	91	98	1	1	1	1	1	1	1	98	91	84	77	69	61	53	45	O	O	O	O	O	O
37	O	O	O	22	28	34	42	51	60	70	80	91	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	91	80	70	60	O	O	O	O	O	O
38	O	O	O	28	35	43	53	63	75	87	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	87	75	63	O	O	O	O	O	O
39	O	O	O	33	41	51	62	75	88	1	1	1	1	1	1	1	1	2	2	2	2	2	2	2	1	1	1	1	1	1	88	O	O	O	O	O	O
40	O	O	O	36	46	56	69	83	98	1	1	1	1	1	1	1	2	2	2	2	2	2	2	2	2	1	1	1	1	1	98	O	O	O	O	O	O
41	O	O	O	38	48	59	72	87	1	1	1	1	1	1	1	2	2	2	2	2	2	2	2	2	2	2	1	1	1	1	1	O	O	O	O	O	O
42	O	O	O	38	47	59	71	86	1	1	1	1	1	1	1	2	2	2	2	2	2	2	2	2	2	2	1	1	1	1	1	O	O	O	O	O	O
43	O	O	O	35	44	55	67	80	95	1	1	1	1	1	1	2	2	2	2	2	2	2	2	2	2	1	1	1	1	1	95	O	O	O	O	O	O
44	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O

CONCENTRATIONS ABOVE BACKGROUND OF FLUID (VOLUMETRIC RATIO OF DUMP FLUID TO AMBIENT WATER) IN THE CLOUD 3600.00 SECONDS AFTER DUMP

119.00 FT BELOW THE WATER SURFACE

...MULTIPLY DISPLAYED VALUES BY 0.1000E-04 (LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)

M	N=	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31
2		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
4	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
5	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
6	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
7	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
8	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
9	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
10	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
11	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
12	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
13	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
14	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
15	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
16	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
17	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
18	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
19	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
20	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
21	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
22	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
23	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
24	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
25	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
26	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
27	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
28	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
29	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
30	0000	.01	.01	.02	.02	.03	.03	.04	.04	.05	.06	.06	.07	.07	.08	.08	.08	.08	.08	.08	.08	.07	.07	.06	.06	.05	.04	.04	.030000		
31	0000	.02	.03	.03	.04	.05	.06	.07	.09	.10	.11	.12	.13	.14	.15	.15	.16	.16	.16	.15	.15	.14	.13	.12	.11	.10	.09	.07	.060000		
32	0000	.04	.05	.06	.08	.10	.11	.13	.15	.18	.20	.22	.24	.25	.27	.28	.28	.28	.28	.28	.27	.25	.24	.22	.20	.18	.15	.13	.110000		
33	0000	.07	.09	.11	.14	.16	.19	.23	.26	.30	.33	.37	.40	.43	.45	.47	.48	.48	.48	.47	.45	.43	.40	.37	.33	.30	.26	.23	.190000		
34	0000	.11	.14	.18	.22	.26	.31	.36	.42	.47	.53	.58	.63	.67	.71	.74	.75	.76	.75	.74	.71	.67	.63	.58	.53	.47	.42	.36	.310000		
35	0000	.17	.21	.27	.33	.39	.46	.54	.62	.71	.79	.87	.94	1.0	1.0	1.1	1.1	1.1	1.1	1.1	1.0	1.0	.94	.87	.79	.71	.62	.54	.460000		
36	0000	.24	.30	.38	.46	.55	.65	.76	.88	.99	1.1	1.2	1.3	1.4	1.4	1.5	1.5	1.5	1.5	1.5	1.4	1.4	1.3	1.2	1.1	.99	.88	.76	.650000		
37	0000	.32	.40	.50	.61	.73	.87	1.0	1.1	1.3	1.4	1.6	1.7	1.8	1.9	2.0	2.0	2.1	2.0	2.0	1.9	1.8	1.7	1.6	1.4	1.3	1.1	1.0	.870000		
38	0000	.40	.50	.62	.76	.92	1.0	1.2	1.4	1.6	1.8	2.0	2.1	2.3	2.4	2.5	2.6	2.6	2.6	2.5	2.4	2.3	2.1	2.0	1.8	1.6	1.4	1.2	1.00000		
39	0000	.47	.59	.74	.90	1.0	1.2	1.4	1.7	1.9	2.1	2.3	2.5	2.7	2.9	3.0	3.0	3.1	3.0	3.0	2.9	2.7	2.5	2.3	2.1	1.9	1.7	1.4	1.20000		
40	0000	.53	.66	.82	1.0	1.2	1.4	1.6	1.9	2.1	2.4	2.6	2.8	3.0	3.2	3.3	3.4	3.4	3.4	3.3	3.2	3.0	2.8	2.6	2.4	2.1	1.9	1.6	1.40000		
41	0000	.55	.69	.86	1.0	1.2	1.4	1.7	2.0	2.2	2.5	2.7	3.0	3.2	3.3	3.5	3.5	3.6	3.5	3.5	3.3	3.2	3.0	2.7	2.5	2.2	2.0	1.7	1.40000		
42	0000	.54	.68	.85	1.0	1.2	1.4	1.7	1.9	2.2	2.4	2.7	2.9	3.1	3.3	3.4	3.5	3.5	3.5	3.4	3.3	3.1	2.9	2.7	2.4	2.2	1.9	1.7	1.40000		
43	0000	.51	.64	.79	.96	1.1	1.3	1.6	1.8	2.0	2.3	2.5	2.7	2.9	3.1	3.2	3.3	3.3	3.3	3.2	3.1	2.9	2.7	2.5	2.3	2.0	1.8	1.6	1.30000		
44		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0

CONCENTRATIONS ABOVE BACKGROUND OF FLUID (VOLUMETRIC RATIO OF DUMP FLUID TO AMBIENT WATER) IN THE CLOUD 3600.00 SECONDS AFTER DUMP

THESE CONCENTRATIONS ARE THE MAXIMUM OCCURING IN THE WATER COLUMN AT THIS TIME

...MULTIPLY DISPLAYED VALUES BY 0.1000E-03 (LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)

M N=	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31
2	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O
3	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
18	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
19	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
20	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
21	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
22	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
23	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
24	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
25	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
26	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
27	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
28	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
29	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
30	O	+	.01	.01	.01	.02	.02	.02	.03	.03	.04	.04	.04	.05	.05	.05	.05	.05	.05	.05	.05	.05	.04	.04	.04	.03	.03	.02	.02	0
31	O	.01	.02	.02	.03	.03	.04	.05	.06	.07	.07	.08	.09	.10	.10	.10	.11	.11	.11	.10	.10	.10	.09	.08	.07	.07	.06	.05	.04	0
32	O	.03	.03	.04	.05	.06	.08	.09	.11	.12	.13	.15	.16	.17	.18	.19	.19	.20	.19	.19	.18	.17	.16	.15	.13	.12	.11	.09	.08	0
33	O	.05	.06	.07	.09	.11	.13	.16	.18	.20	.23	.25	.27	.29	.31	.32	.33	.33	.33	.32	.31	.29	.27	.25	.23	.20	.18	.16	.13	0
34	O	.08	.10	.12	.15	.18	.21	.25	.29	.33	.36	.40	.44	.47	.49	.51	.52	.52	.52	.51	.49	.47	.44	.40	.36	.33	.29	.25	.21	0
35	O	.12	.15	.18	.22	.27	.32	.37	.43	.49	.54	.60	.65	.69	.73	.76	.78	.78	.78	.76	.73	.69	.65	.60	.54	.49	.43	.37	.32	0
36	O	.16	.21	.26	.32	.38	.45	.53	.61	.69	.77	.84	.91	.98	1.0	1.0	1.0	1.1	1.0	1.0	1.0	.98	.91	.84	.77	.69	.61	.53	.45	0
37	O	.22	.28	.34	.42	.51	.60	.70	.80	.91	1.0	1.1	1.2	1.3	1.3	1.4	1.4	1.4	1.4	1.4	1.3	1.3	1.2	1.1	1.0	.91	.80	.70	.60	0
38	O	.28	.35	.43	.53	.63	.75	.87	1.0	1.1	1.2	1.4	1.5	1.6	1.7	1.7	1.8	1.8	1.8	1.7	1.7	1.6	1.5	1.4	1.2	1.1	1.0	.87	.75	0
39	O	.33	.41	.51	.62	.75	.88	1.0	1.1	1.3	1.5	1.6	1.7	1.9	2.0	2.0	2.1	2.1	2.1	2.0	2.0	1.9	1.7	1.6	1.5	1.3	1.1	1.0	.88	0
40	O	.36	.46	.56	.69	.83	.98	1.1	1.3	1.4	1.6	1.8	1.9	2.1	2.2	2.3	2.3	2.3	2.3	2.3	2.2	2.1	1.9	1.8	1.6	1.4	1.3	1.1	.98	0
41	O	.38	.48	.59	.72	.87	1.0	1.2	1.3	1.5	1.7	1.9	2.0	2.2	2.3	2.4	2.4	2.5	2.4	2.4	2.3	2.2	2.0	1.9	1.7	1.5	1.3	1.2	1.00	0
42	O	.38	.47	.59	.71	.86	1.0	1.1	1.3	1.5	1.7	1.9	2.0	2.2	2.3	2.4	2.4	2.4	2.4	2.4	2.3	2.2	2.0	1.9	1.7	1.5	1.3	1.1	1.00	0
43	O	.35	.44	.55	.67	.80	.95	1.1	1.2	1.4	1.6	1.7	1.9	2.0	2.1	2.2	2.2	2.3	2.2	2.2	2.1	2.0	1.9	1.7	1.6	1.4	1.2	1.1	.950	0
44	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O

CONCENTRATIONS ABOVE BACKGROUND OF FLUID (VOLUMETRIC RATIO OF DUMP FLUID TO AMBIENT WATER) IN THE CLOUD 3600.00 SECONDS AFTER DUMP

THESE CONCENTRATIONS ARE THE MAXIMUM THAT EVER OCCURRED IN THE WATER COLUMN DURING THE SIMULATION

...MULTIPLY DISPLAYED VALUES BY 0.1000E-02 (LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)

M N=	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31
2	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O
3	O	O	O	O	O	O	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	0	0	0	O
4	O	O	O	O	O	O	+	+	+	+	+	+	+	.01	.01	.01	.01	.01	.01	.01	.01	.01	+	+	+	+	0	0	0	O
5	O	O	O	O	O	O	+	+	+	.01	.01	.02	.03	.05	.06	.07	.08	.08	.08	.07	.06	.05	.03	.02	.01	.01	0	0	0	O
6	O	O	O	O	O	+	+	.01	.02	.03	.06	.09	.14	.19	.24	.28	.31	.32	.31	.28	.24	.19	.14	.09	.06	.03	+	0	0	O
7	O	O	O	O	O	+	.01	.03	.06	.11	.18	.28	.40	.54	.68	.81	.89	.92	.89	.81	.68	.54	.40	.28	.18	.11	+	0	0	O
8	O	O	O	O	.	+	.03	.07	.14	.24	.40	.61	.89	1.1	1.5	1.7	1.9	2.0	1.9	1.7	1.5	1.1	.89	.61	.40	.24	+	+	0	O
9	O	O	O	O	+	+	.06	.12	.23	.41	.67	1.0	1.4	2.0	2.5	2.9	3.3	3.4	3.3	2.9	2.5	2.0	1.4	1.0	.67	.41	.02	+	0	O
10	O	O	O	O	+	.01	.08	.16	.30	.53	.87	1.3	1.9	2.6	3.2	3.8	4.2	4.4	4.2	3.8	3.2	2.6	1.9	1.3	.87	.53	.06	+	0	O
11	O	O	O	O	+	.02	.08	.16	.30	.53	.87	1.3	1.9	2.5	3.2	3.8	4.2	4.3	4.2	3.8	3.2	2.5	1.9	1.3	.87	.53	.11	+	0	O
12	O	O	O	O	+	.03	.06	.12	.23	.40	.66	1.0	1.4	1.9	2.4	2.9	3.2	3.3	3.2	2.9	2.4	1.9	1.4	1.0	.66	.40	.17	.02	0	O
13	O	O	O	+	+	.03	.06	.12	.20	.33	.50	.72	.98	1.2	1.5	1.7	1.9	1.9	1.9	1.7	1.5	1.2	.98	.72	.50	.33	.20	.04	+	O
14	O	O	O	+	.01	.03	.06	.11	.19	.31	.48	.69	.94	1.2	1.4	1.6	1.8	1.8	1.8	1.6	1.4	1.2	.94	.69	.48	.31	.19	.07	+	O
15	O	O	.	+	.01	.03	.05	.09	.15	.24	.36	.52	.71	.91	1.1	1.2	1.3	1.4	1.3	1.2	1.1	.91	.71	.52	.36	.24	.15	.09	+	O
16	O	O	+	+	.02	.03	.06	.10	.16	.25	.36	.49	.63	.78	.92	1.0	1.1	1.1	1.1	1.0	.92	.78	.63	.49	.36	.25	.16	.10	+	O
17	O	O	+	+	.01	.03	.06	.09	.15	.23	.33	.45	.58	.72	.85	.96	1.0	1.0	1.0	.96	.85	.72	.58	.45	.33	.23	.15	.09	.010	O
18	O	+	+	+	.02	.03	.06	.09	.13	.19	.25	.34	.44	.55	.65	.73	.79	.80	.79	.73	.65	.55	.44	.34	.25	.19	.13	.09	.020	O
19	O	+	+	.01	.02	.04	.06	.09	.14	.20	.27	.35	.44	.53	.61	.68	.72	.74	.72	.68	.61	.53	.44	.35	.27	.20	.14	.09	.040	O
20	O	+	+	.01	.02	.03	.05	.08	.13	.18	.24	.32	.40	.48	.55	.61	.65	.67	.65	.61	.55	.48	.40	.32	.24	.18	.13	.08	.050	O
21	O	+	+	.01	.03	.04	.07	.10	.14	.18	.24	.30	.37	.43	.49	.54	.56	.57	.56	.54	.49	.43	.37	.30	.24	.18	.14	.10	.070	O
22	O	+	.01	.01	.03	.04	.07	.10	.14	.19	.25	.31	.38	.44	.50	.55	.58	.59	.58	.55	.50	.44	.38	.31	.25	.19	.14	.10	.070	O
23	O	+	.01	.02	.03	.05	.07	.09	.13	.17	.22	.28	.34	.40	.45	.49	.52	.53	.52	.49	.45	.40	.34	.28	.22	.17	.13	.09	.070	O
24	O	+	.01	.02	.03	.05	.08	.11	.15	.19	.24	.29	.35	.40	.44	.48	.50	.51	.50	.48	.44	.40	.35	.29	.24	.19	.15	.11	.080	O
25	O	O	.01	.01	.02	.03	.05	.08	.11	.14	.19	.24	.29	.35	.40	.44	.48	.50	.51	.50	.48	.44	.40	.35	.29	.24	.19	.14	.11	.080
26	O	O	.01	.02	.03	.04	.06	.08	.11	.14	.17	.21	.26	.30	.35	.39	.42	.44	.45	.44	.42	.39	.35	.30	.26	.21	.17	.14	.11	.080
27	O	O	.01	.02	.03	.04	.06	.09	.12	.15	.19	.23	.28	.32	.36	.40	.42	.44	.45	.44	.42	.40	.36	.32	.28	.23	.19	.15	.12	.090
28	O	O	.01	.02	.03	.04	.06	.08	.11	.15	.18	.23	.27	.31	.35	.39	.42	.43	.44	.43	.42	.39	.35	.31	.27	.23	.18	.15	.11	.080
29	O	O	.01	.02	.03	.05	.07	.09	.11	.14	.17	.21	.24	.28	.31	.34	.36	.38	.38	.38	.36	.34	.31	.28	.24	.21	.17	.14	.11	.090
30	O	O	.02	.02	.04	.05	.07	.09	.12	.15	.18	.22	.26	.29	.33	.36	.38	.39	.39	.39	.38	.36	.33	.29	.26	.22	.18	.15	.12	.090
31	O	O	.02	.03	.04	.05	.07	.09	.11	.14	.18	.21	.25	.28	.31	.34	.36	.38	.38	.38	.36	.34	.31	.28	.25	.21	.18	.14	.11	.090
32	O	O	.02	.03	.04	.06	.07	.09	.12	.14	.17	.20	.23	.26	.29	.31	.32	.33	.34	.33	.32	.31	.29	.26	.23	.20	.17	.14	.12	.090
33	O	O	.02	.03	.04	.06	.08	.10	.12	.15	.18	.21	.24	.27	.29	.32	.33	.34	.35	.34	.33	.32	.29	.27	.24	.21	.18	.15	.12	.100
34	O	O	.02	.03	.04	.06	.07	.09	.11	.14	.17	.20	.23	.25	.28	.30	.32	.33	.33	.33	.32	.30	.28	.25	.23	.20	.17	.14	.11	.090
35	O	O	.02	.03	.05	.06	.08	.10	.12	.14	.17	.19	.22	.24	.26	.28	.29	.30	.30	.30	.29	.28	.26	.24	.22	.19	.17	.14	.12	.100
36	O	O	.03	.03	.05	.06	.08	.10	.12	.14	.17	.19	.22	.24	.27	.28	.30	.31	.31	.31	.30	.28	.27	.24	.22	.19	.17	.14	.12	.100
37	O	O	.03	.04	.05	.06	.08	.09	.11	.14	.16	.18	.21	.23	.25	.27	.28	.29	.29	.29	.28	.27	.25	.23	.21	.18	.16	.14	.11	.090
38	O	O	.03	.04	.05	.06	.08	.10	.12	.14	.16	.18	.20	.22	.24	.25	.26	.27	.27	.27	.26	.25	.24	.22	.20	.18	.16	.14	.12	.100
39	O	O	.03	.04	.05	.06	.08	.10	.12	.14	.16	.18	.20	.22	.24	.25	.26	.27	.27	.27	.26	.25	.24	.22	.20	.18	.16	.14	.12	.100
40	O	O	.03	.04	.05	.06	.08	.09	.11	.13	.15	.17	.19	.21	.22	.24	.25	.25	.26	.25	.25	.24	.22	.21	.19	.17	.15	.13	.11	.090
41	O	O	.03	.04	.05	.07	.08	.10	.12	.13	.15	.17	.19	.20	.22	.23	.24	.24	.25	.24	.24	.23	.22	.20	.19	.17	.15	.13	.12	.100
42	O	O	.03	.04	.05	.07	.08	.10	.11	.13	.15	.17	.19	.20	.22	.23	.24	.24	.24	.24	.24	.23	.22	.20	.19	.17	.15	.13	.11	.100
43	O	O	.03	.04	.05	.06	.08	.09	.11	.12	.14	.16	.17	.19	.20	.21	.22	.22	.23	.22	.22	.21	.20	.19	.17	.16	.14	.12	.11	.090
44	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O

SMALL CLOUDS AT 3600.00 SECONDS ELAPSED TIME FOR FLUID

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID	LOCATION OF CLOUD CENTROID DISTANCE FROM LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	2015.	450.0	5067.	0.0000E+00	732.8	0.0000E+00	120.0	0.000000E+00

FINAL DISTRIBUTIONS OF TOTAL SETTLED MATERIAL FOLLOW.....

TOTAL ACCUMULATED SOLID VOLUME ON BOTTOM (CU FT/GRID SQR), 3600.00 SECONDS AFTER DUMP

...MULTIPLY DISPLAYED VALUES BY 1.000 (LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)

M N=	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31
2	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O
3	O	O	O	O	.	.	.	+	+	+	+	+	.01	.01	.02	.03	.03	.03	.04	.03	.03	.03	.02	.01	.01	+	+	+	+	+0
4	O	O	O	O	.	+	+	+	+	+	+	.01	.03	.05	.07	.11	.15	.19	.22	.24	.25	.24	.22	.19	.15	.11	.07	.05	.03	.01
5	O	O	O	O	+	+	+	+	.01	.02	.04	.08	.15	.25	.38	.55	.74	.93	1.1	1.2	1.2	1.2	1.1	.93	.74	.55	.38	.25	.15	.08
6	O	O	O	O	+	+	+	.01	.04	.08	.17	.32	.57	.94	1.4	2.0	2.7	3.5	4.1	4.5	4.7	4.5	4.1	3.5	2.7	2.0	1.4	.94	.57	.32
7	O	O	O	O	+	+	.02	.05	.12	.26	.51	.96	1.6	2.7	4.2	6.0	8.1	10	12	13	14	13	12	10	8.1	6.0	4.2	2.7	1.6	.96
8	O	O	O	O	+	.02	.05	.12	.28	.60	1.1	2.1	3.8	6.2	10	14	18	23	27	34	42	34	27	23	18	14	10	6.2	3.8	2.1
9	O	O	O	O	.01	.04	.10	.23	.52	1.1	2.1	3.9	6.8	11	17	24	33	41	48	54	56	54	48	41	33	24	17	11	6.8	3.9
10	O	O	O	O	.02	.06	.16	.37	.80	1.6	3.2	5.8	10	16	24	35	46	58	69	76	79	76	69	58	46	35	24	16	10	5.8
11	O	O	O	O	.03	.09	.22	.50	1.0	2.1	4.0	7.2	12	19	29	41	54	68	80	88	92	88	80	68	54	41	29	19	12	7.2
12	O	O	O	O	.05	.12	.28	.62	1.2	2.4	4.5	7.9	13	21	30	42	55	69	80	88	91	88	80	69	55	42	30	21	13	7.9
13	O	O	O	O	.07	.16	.34	.72	1.4	2.7	4.8	8.2	13	20	29	40	52	64	75	83	86	83	75	64	52	40	29	20	13	8.2
14	O	O	O	O	.08	.18	.39	.80	1.5	2.8	4.9	8.1	13	19	27	37	47	58	66	73	75	73	66	58	47	37	27	19	13	8.1
15	O	O	O	O	.09	.20	.42	.82	1.5	2.7	4.7	7.6	12	18	25	33	41	50	57	62	63	62	57	50	41	33	25	18	12	7.6
16	O	O	O	O	.09	.20	.40	.78	1.4	2.5	4.2	6.8	10	15	21	28	34	41	47	52	53	52	47	41	34	28	21	15	10	6.8
17	O	O	O	O	.08	.18	.36	.68	1.2	2.1	3.5	5.5	8.4	12	17	22	27	32	36	39	40	39	36	32	27	22	17	12	8.4	5.5
18	O	O	O	O	.07	.14	.28	.53	.95	1.6	2.6	4.1	6.2	8.8	12	16	19	23	26	28	28	28	26	23	19	16	12	8.8	6.2	4.1
19	O	O	O	O	.05	.10	.20	.38	.66	1.1	1.8	2.8	4.1	5.8	7.9	10	13	15	17	18	19	18	17	15	13	10	7.9	5.8	4.1	2.8
20	O	O	O	O	.03	.07	.13	.24	.42	.70	1.1	1.7	2.5	3.5	4.7	6.0	7.4	8.7	10	11	11	11	10	8.7	7.4	6.0	4.7	3.5	2.5	1.7
21	O	O	O	O	.02	.04	.08	.14	.24	.40	.63	.96	1.4	1.9	2.5	3.3	4.0	4.7	5.3	5.7	5.9	5.7	5.3	4.7	4.0	3.3	2.5	1.9	1.4	.96
22	O	O	O	O	.01	.02	.04	.07	.13	.21	.33	.49	.71	.98	1.3	1.6	2.0	2.3	2.7	2.9	3.0	2.9	2.7	2.3	2.0	1.6	1.3	.98	.71	.49
23	O	O	O	O	+	.01	.02	.03	.06	.10	.15	.23	.33	.46	.60	.76	.93	1.0	1.2	1.3	1.3	1.3	1.2	1.0	.93	.76	.60	.46	.33	.23
24	O	O	O	O	+	+	+	.01	.02	.04	.06	.10	.14	.19	.25	.32	.39	.47	.54	.60	.62	.60	.54	.47	.39	.32	.25	.19	.14	.10
25	O	O	O	O	+	+	+	+	.01	.01	.02	.03	.05	.07	.09	.12	.15	.19	.23	.27	.28	.27	.23	.19	.15	.12	.09	.07	.05	.03
26	O	O	O	O	+	+	+	+	+	+	+	.01	.01	.02	.03	.04	.05	.07	.08	.10	.10	.10	.08	.07	.05	.04	.03	.02	.01	.01
27	O	O	O	O	+	+	+	+	+	+	+	+	.01	.01	.02	.03	.04	.04	.05	.04	.04	.03	.02	.01	.01	+	+	+	+	+0
28	O	O	O	O	.	.	+	+	+	+	+	+	+	.01	.01	.02	.03	.03	.03	.02	.01	.01	+	+	+	+	+	+	+	+0
29	O	O	O	O	.	.	.	.	+	+	+	+	+	+	+	.01	.01	.01	.01	.01	.01	.01	+	+	+	+	+	+	+	+0
30	O	O	O	O	.	.	.	.	+	+	+	+	+	+	+	+	.01	.01	.01	.01	.01	+	+	+	+	+	+	+	+	+0
31	O	O	O	O	.	.	.	.	+	+	+	+	+	+	+	+	+	.01	.01	.01	+	+	+	+	+	+	+	+	+	+0
32	O	O	O	O	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+0
33	O	O	O	O	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+0
34	O	O	O	O	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+0
35	O	O	O	O	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+0
36	O	O	O	O	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+0
37	O	O	O	O	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+0
38	O	O	O	O	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+0
39	O	O	O	O	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+0
40	O	O	O	O	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+0
41	O	O	O	O	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+0
42	O	O	O	O	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+0
43	O	O	O	O	.	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.0
44	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O

TOTAL THICKNESS (FT) OF NEW MATERIAL ON BOTTOM, 3600.00 SECONDS AFTER DUMP

...MULTIPLY DISPLAYED VALUES BY 1.000 (LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)

M N=	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31
2	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O
3	O	O	0	0	0	0	.	.	.	.	.	.	.	.	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.0000
4	O	O	0	0	.	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.0000
5	O	O	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+0000
6	O	O	.	.	.	.	+	+	+	+	+	+	+	.01	.01	.01	.02	.02	.02	.02	.02	.01	.01	.01	+	+	+	+	+	+0000
7	O	O	.	.	+	+	+	+	+	+	+	.01	.02	.02	.03	.05	.05	.06	.06	.06	.05	.05	.03	.02	.02	.01	+	+	+	+0000
8	O	O	.	+	+	+	+	+	+	.01	.01	.03	.04	.06	.09	.11	.13	.16	.20	.16	.13	.11	.09	.06	.04	.03	.01	.01	+	+0000
9	O	O	.	+	+	+	+	+	.01	.01	.03	.05	.08	.11	.16	.20	.23	.26	.27	.26	.23	.20	.16	.11	.08	.05	.03	.01	.01	+0000
10	O	O	+	+	+	+	+	+	.01	.02	.04	.07	.12	.17	.22	.28	.33	.37	.39	.37	.33	.28	.22	.17	.12	.07	.04	.02	.01	+0000
11	O	O	+	+	+	+	+	.01	.01	.03	.06	.09	.14	.20	.26	.33	.39	.43	.45	.43	.39	.33	.26	.20	.14	.09	.06	.03	.01	.010000
12	O	O	+	+	+	+	+	.01	.02	.03	.06	.10	.14	.20	.27	.33	.39	.43	.44	.43	.39	.33	.27	.20	.14	.10	.06	.03	.02	.010000
13	O	O	+	+	+	+	+	.01	.02	.04	.06	.10	.14	.19	.25	.31	.36	.40	.42	.40	.36	.31	.25	.19	.14	.10	.06	.04	.02	.010000
14	O	O	+	+	+	+	+	.01	.02	.04	.06	.09	.13	.18	.23	.28	.32	.35	.37	.35	.32	.28	.23	.18	.13	.09	.06	.04	.02	.010000
15	O	O	+	+	+	+	+	.01	.02	.03	.05	.08	.12	.16	.20	.24	.28	.30	.31	.30	.28	.24	.20	.16	.12	.08	.05	.03	.02	.010000
16	O	O	+	+	+	+	+	.01	.02	.03	.05	.07	.10	.13	.17	.20	.23	.25	.26	.25	.23	.20	.17	.13	.10	.07	.05	.03	.02	.010000
17	O	O	+	+	+	+	+	.01	.01	.02	.04	.05	.08	.10	.13	.15	.17	.19	.19	.19	.17	.15	.13	.10	.08	.05	.04	.02	.01	.010000
18	O	O	+	+	+	+	+	+	.01	.02	.03	.04	.05	.07	.09	.11	.12	.13	.14	.13	.12	.11	.09	.07	.05	.04	.03	.02	.01	+0000
19	O	O	+	+	+	+	+	+	+	.01	.02	.02	.03	.05	.06	.07	.08	.09	.09	.09	.08	.07	.06	.05	.03	.02	.02	.01	+	+0000
20	O	O	+	+	+	+	+	+	+	+	.01	.01	.02	.02	.03	.04	.04	.05	.05	.05	.04	.04	.03	.02	.02	.01	.01	+	+	+0000
21	O	O	+	+	+	+	+	+	+	+	+	.01	.01	.01	.02	.02	.02	.02	.02	.02	.02	.02	.01	.01	.01	+	+	+	+	+0000
22	O	O	.	+	+	+	+	+	+	+	+	+	+	+	.01	.01	.01	.01	.01	.01	.01	+	+	+	+	+	+	+	+	+0000
23	O	O	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+0000
24	O	O	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+0000
25	O	O	.	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.0000
26	O	O	.	.	.	.	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.0000
27	O	O	0	.	.	.	.	.	.	.	.	.	.	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.0000
28	O	O	0	0	0	0	.	.	.	.	.	.	.	.	.	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.0000
29	O	O	0	0	0	0	0	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.0000
30	O	O	0	0	0	0	0	0	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	00000
31	O	O	0	0	0	0	0	0	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	00000
32	O	O	0	0	0	0	0	0	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	00000
33	O	O	0	0	0	0	0	0	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	00000
34	O	O	0	0	0	0	0	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.0000
35	O	O	0	0	0	0	0	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.0000
36	O	O	0	0	0	0	0	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.0000
37	O	O	0	0	0	0	0	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.0000
38	O	O	0	0	0	0	0	0	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	00000
39	O	O	0	0	0	0	0	0	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	00000
40	O	O	0	0	0	0	0	0	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	00000
41	O	O	0	0	0	0	0	0	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	00000
42	O	O	0	0	0	0	0	0	0	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	0	00000
43	O	O	0	0	0	0	0	0	0	0	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	0	0	00000
44	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O

INITIAL MIXING COMPUTATIONS RESULTS FOR GRAVEL :

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND ON ENTIRE GRID (MG/L)	X-LOC (FT)	Z-LOC (FT)	MAX CONC ABOVE BACKGROUND OUTSIDE MIXING ZONE (MG/L)
0.25	60.0	0.000E+00	0.	0.	0.000E+00
0.50	60.0	0.000E+00	0.	0.	0.000E+00
0.75	60.0	0.000E+00	0.	0.	0.000E+00
1.00	60.0	0.000E+00	0.	0.	0.000E+00
0.25	119.0	0.000E+00	0.	0.	0.000E+00
0.50	119.0	0.000E+00	0.	0.	0.000E+00
0.75	119.0	0.000E+00	0.	0.	0.000E+00
1.00	119.0	0.000E+00	0.	0.	0.000E+00

INITIAL MIXING COMPUTATIONS RESULTS FOR SAND :

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND ON ENTIRE GRID (MG/L)	X-LOC (FT)	Z-LOC (FT)	MAX CONC ABOVE BACKGROUND OUTSIDE MIXING ZONE (MG/L)
0.25	60.0	0.318E+00	750.	450.	0.318E+00
0.50	60.0	0.156E-07	1150.	450.	0.156E-07
0.75	60.0	0.149E-19	1600.	450.	0.149E-19
1.00	60.0	0.000E+00	0.	0.	0.000E+00
0.25	119.0	0.256E+02	750.	450.	0.256E+02
0.50	119.0	0.852E+00	1150.	450.	0.852E+00
0.75	119.0	0.159E-01	1600.	450.	0.159E-01
1.00	119.0	0.705E-04	2000.	450.	0.705E-04

INITIAL MIXING COMPUTATIONS RESULTS FOR SILT :

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND ON ENTIRE GRID (MG/L)	X-LOC (FT)	Z-LOC (FT)	MAX CONC ABOVE BACKGROUND OUTSIDE MIXING ZONE (MG/L)
0.25	60.0	0.894E+03	750.	450.	0.894E+03
0.50	60.0	0.315E+03	1150.	450.	0.315E+03
0.75	60.0	0.183E+03	1600.	450.	0.183E+03
1.00	60.0	0.171E+03	2000.	450.	0.171E+03
0.25	119.0	0.450E+03	750.	450.	0.450E+03
0.50	119.0	0.176E+03	1150.	450.	0.176E+03
0.75	119.0	0.809E+02	1600.	450.	0.809E+02
1.00	119.0	0.273E+02	2000.	450.	0.273E+02

INITIAL MIXING COMPUTATIONS RESULTS FOR CLAY :

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND ON ENTIRE GRID (MG/L)	X-LOC (FT)	Z-LOC (FT)	MAX CONC ABOVE BACKGROUND OUTSIDE MIXING ZONE (MG/L)
0.25	60.0	0.313E+03	750.	450.	0.313E+03
0.50	60.0	0.163E+03	1150.	450.	0.163E+03
0.75	60.0	0.970E+02	1600.	450.	0.970E+02
1.00	60.0	0.565E+02	2000.	450.	0.565E+02
0.25	119.0	0.123E+03	750.	450.	0.123E+03
0.50	119.0	0.299E+02	1150.	450.	0.299E+02
0.75	119.0	0.140E+02	1600.	450.	0.140E+02
1.00	119.0	0.817E+01	2000.	450.	0.817E+01

INITIAL MIXING COMPUTATIONS RESULTS FOR FLUID :

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND ON ENTIRE GRID (PERCENT)	X-LOC (FT)	Z-LOC (FT)	MAX CONC ABOVE BACKGROUND OUTSIDE MIXING ZONE (PERCENT)
0.08	60.0	0.536E-08	450.	450.	0.405E-08
0.17	60.0	0.179E-01	600.	450.	0.179E-01
0.25	60.0	0.810E-01	750.	450.	0.810E-01
0.33	60.0	0.735E-01	900.	450.	0.735E-01
0.42	60.0	0.595E-01	1050.	450.	0.595E-01
0.50	60.0	0.513E-01	1150.	450.	0.513E-01
0.58	60.0	0.453E-01	1300.	450.	0.453E-01
0.67	60.0	0.400E-01	1450.	450.	0.400E-01
0.75	60.0	0.353E-01	1600.	450.	0.353E-01
0.83	60.0	0.313E-01	1750.	450.	0.313E-01
0.92	60.0	0.278E-01	1850.	450.	0.278E-01
1.00	60.0	0.250E-01	2000.	450.	0.250E-01
0.08	119.0	0.776E-01	450.	450.	0.586E-01
0.17	119.0	0.308E-01	600.	450.	0.308E-01
0.25	119.0	0.171E-01	750.	450.	0.171E-01
0.33	119.0	0.108E-01	900.	450.	0.108E-01
0.42	119.0	0.860E-02	1050.	450.	0.860E-02
0.50	119.0	0.742E-02	1150.	450.	0.742E-02
0.58	119.0	0.655E-02	1300.	450.	0.655E-02
0.67	119.0	0.578E-02	1450.	450.	0.578E-02
0.75	119.0	0.511E-02	1600.	450.	0.511E-02
0.83	119.0	0.452E-02	1750.	450.	0.452E-02
0.92	119.0	0.402E-02	1850.	450.	0.402E-02
1.00	119.0	0.362E-02	2000.	450.	0.362E-02
0.08	60.0	0.442E+00	450.	450.	0.334E+00
0.17	60.0	0.198E+00	600.	450.	0.198E+00
0.25	60.0	0.115E+00	750.	450.	0.115E+00
0.33	60.0	0.742E-01	900.	450.	0.742E-01
0.42	60.0	0.595E-01	1050.	450.	0.595E-01
0.50	60.0	0.513E-01	1150.	450.	0.513E-01
0.58	60.0	0.453E-01	1300.	450.	0.453E-01
0.67	60.0	0.400E-01	1450.	450.	0.400E-01
0.75	60.0	0.353E-01	1600.	450.	0.353E-01
0.83	60.0	0.313E-01	1750.	450.	0.313E-01
0.92	60.0	0.278E-01	1850.	450.	0.278E-01
1.00	60.0	0.250E-01	2000.	450.	0.250E-01

RESULT: THE TOXICITY STANDARD FOR THE MIXING ZONE WAS NOT VIOLATED.

*** RUN COMPLETED ***

STFATE
Maximum Currents

MODEL: SHORT-TERM FATE OF DREDGED MATERIAL FROM SPLIT HULL BARGE OR HOPPER DREDGE
(PC Version 5.01 MAY, 1993)

TITLE: Douglas Harbor to Gastineau Channel Current 1.18

FILE: DHGAS400.DUE

AREA: THE PROJECT AREA IS DESCRIBED BY A 32 X 45 GRID.

THERE ARE 32 GRID POINTS (NMAX) IN THE Z-DIRECTION (FROM LEFT TO RIGHT)
AND 45 GRID POINTS (MMAX) IN THE X-DIRECTION (FROM TOP TO BOTTOM).

ZONE: THE MIXING ZONE IS REPRESENTED AS A RECTANGLE ON THE SITE GRID.

THE TOPMOST BOUNDARY IS LOCATED AT POINT # 3 (MDS1) FROM THE TOP OF THE GRID.

THE BOTTOMMOST BOUNDARY IS LOCATED AT POINT # 9 (MDS2) FROM THE TOP OF THE GRID.

THE LEFTMOST BOUNDARY IS LOCATED AT POINT #11 (NDS1) FROM THE LEFT OF THE GRID.

THE RIGHTMOST BOUNDARY IS LOCATED AT POINT #26 (NDS2) FROM THE LEFT OF THE GRID.

EXECUTION PARAMETERS:

MODEL COEFFICIENTS SPECIFIED IN INPUT DATA (KEY1 = 1).

PERFORM COMPLETE ANALYSIS INCLUDING DESCENT, COLLAPSE, AND TRANSPORT-DIFFUSION (KEY2 = 0).

PERFORM TIER III INLAND DUMPING INITIAL MIXING EVALUATION
TO COMPARE WITH TOXICITY STANDARD (KEY3 = 6).

MIXING ZONE HAS BEEN DESIGNATED -- NO MIXING ZONE WILL BE COMPUTED.

NO ANALYSIS OF A ZONE OF INITIAL DILUTION REQUESTED.

PRINTING OF CONVECTIVE DESCENT RESULTS NOT REQUESTED (IPCN = 0).

PRINTING OF CONVECTIVE DESCENT RESULTS NOT REQUESTED (IPCN = 0).

PRINTING OF DYNAMIC COLLAPSE RESULTS NOT REQUESTED (IPCL = 0).

QUARTERLY PRINTING OF LONG-TERM TRANSPORT DIFFUSION RESULTS REQUESTED (IPLT = 0).

LONG-TERM TRANSPORT DIFFUSION RESULTS REQUESTED AT THE FOLLOWING 2 DEPTH(S):
60.00 FT
119.00 FT

GRID: NUMBER OF LONG TERM GRID POINTS IN Z-DIRECTION (NMAX) = 32

NUMBER OF LONG TERM GRID POINTS IN X-DIRECTION (MMAX) = 45

GRID SPACING IN Z-DIRECTION (DZ) = 25.00000 FT

GRID SPACING IN X-DIRECTION (DX) = 100.00000 FT

CONSTANT DEPTH GRID SPECIFIED HAVING A DEPTH (DEPC) OF 120.00000 FT.

DEPTH GRID, FEET:

M	N = 1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17
1	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.
2	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.
3	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.
4	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.
5	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.
6	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.
7	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.
8	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.
9	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.
10	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.
11	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.
12	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.
13	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.
14	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.
15	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.
16	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.
17	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.
18	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.
19	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.
20	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.
21	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.
22	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.
23	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.
24	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.
25	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.
26	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.
27	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.
28	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.
29	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.
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31	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.
32	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.
33	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.
34	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.
35	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.
36	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.
37	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.
38	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.
39	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.
40	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.
41	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.
42	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.
43	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.
44	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.
45	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.

M	N = 18	19	20	21	22	23	24	25	26	27	28	29	30	31	32
1	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.
2	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.
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10	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.
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12	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.
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17	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.
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33	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.
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35	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.
36	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.
37	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.
38	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.
39	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.
40	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.
41	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.
42	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.
43	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.
44	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.
45	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.	120.

CODED GRID:

RANGE OF N IS   1 TO 32

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LEGEND FOR CODED GRID: W = WATER POINT

L = LAND POINT
O = OPEN BOUNDARY
B = MIXING ZONE BOUNDARY
Z = ZID BOUNDARY
D = DUMP LOCATION
X = DUMMY POINT

NUMBER OF GRID POINTS WITHIN ESTUARY = 1148

DISPOSAL LOCATION:

THE DUMP LOCATION IS 400.0 FT (XBARGE) OR ABOUT GRID POINT # 5 FROM THE TOP OF THE GRID
AND 300.0 FT (ZBARGE) OR ABOUT GRID POINT #13 FROM THE LEFT EDGE OF THE GRID.

THE BOTTOM SLOPE IN THE X-DIRECTION AT THE DUMP SITE (SLOPEX, POSITIVE IF DEPTH INCREASES
FROM TOP OF GRID TO BOTTOM OF GRID) IS 0.00 DEGREES.

THE BOTTOM SLOPE IN THE Z-DIRECTION AT THE DUMP SITE (SLOPEZ, POSITIVE IF DEPTH INCREASES
FROM LEFT SIDE OF GRID TO RIGHT SIDE OF GRID) IS 0.00 DEGREES.

THE DISPOSAL LOCATION IS NOT AT A HOLE OR DEPRESSION. (DHOLE = 0.0)

AMBIENT DENSITY PROFILE:

DEPTH (FT)	DENSITY (G/CC)
0.0000E+00	1.0200
120.0	1.0200

COMPUTED DEPTH:

THE DEPTH AT THE DUMP LOCATION WAS INTERPOLATED TO BE 120.0 FT.

VELOCITY DISTRIBUTION:

VERTICALLY AVERAGED X-DIRECTION (VAX = 1.18 FPS) AND
Z-DIRECTION (VAZ = 0.000E+00 FPS) VELOCITIES CONSTRUCTED AT EACH GRID POINT
FROM A SINGLE OBSERVATION AT A DEPTH (D) OF 95.0 FT.

VELOCITY GRID: X-DIRECTION, FPS

M	N= 1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17
1	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934
2	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934
3	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934
4	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934
5	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934
6	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934
7	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934
8	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934
9	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934
10	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934
11	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934
12	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934
13	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934
14	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934
15	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934
16	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934
17	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934
18	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934
19	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934
20	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934
21	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934
22	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934
23	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934
24	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934
25	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934
26	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934
27	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934
28	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934
29	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934
30	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934
31	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934
32	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934
33	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934
34	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934
35	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934
36	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934
37	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934
38	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934
39	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934
40	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934
41	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934
42	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934

43	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934
44	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934
45	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934

M	N= 18	19	20	21	22	23	24	25	26	27	28	29	30	31	32
1	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934
2	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934
3	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934
4	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934
5	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934
6	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934
7	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934
8	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934
9	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934
10	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934
11	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934
12	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934
13	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934
14	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934
15	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934
16	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934
17	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934
18	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934
19	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934
20	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934
21	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934
22	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934
23	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934
24	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934
25	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934
26	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934
27	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934
28	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934
29	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934
30	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934
31	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934
32	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934
33	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934
34	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934
35	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934
36	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934
37	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934
38	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934
39	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934
40	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934
41	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934
42	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934
43	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934
44	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934
45	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934	0.934

VELOCITY GRID: Z-DIRECTION, FPS

M	N= 1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17
1	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
2	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
3	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
4	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
5	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
6	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
7	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
8	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
9	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
10	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
11	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
12	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
13	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
14	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
15	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
16	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
17	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
18	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
19	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
20	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
21	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
22	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
23	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
24	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
25	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
26	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
27	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
28	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
29	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
30	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
31	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
32	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
33	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
34	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
35	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
36	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
37	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
38	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
39	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
40	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
41	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
42	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
43	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
44	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
45	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000

M	N= 18	19	20	21	22	23	24	25	26	27	28	29	30	31	32
1	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
2	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
3	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
4	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
5	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
6	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
7	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
8	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
9	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
10	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
11	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
12	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
13	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
14	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
15	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
16	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
17	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
18	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
19	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
20	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
21	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
22	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
23	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
24	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
25	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
26	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
27	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
28	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
29	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
30	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
31	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
32	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
33	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
34	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
35	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
36	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
37	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
38	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
39	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
40	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
41	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
42	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
43	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
44	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
45	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000

BOTTOM SHEAR STRESS, LBS/SQ FT:

M	N= 1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17
1	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
2	0.0000	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027
3	0.0000	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027
4	0.0000	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027
5	0.0000	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027
6	0.0000	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027
7	0.0000	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027
8	0.0000	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027
9	0.0000	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027
10	0.0000	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027
11	0.0000	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027
12	0.0000	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027
13	0.0000	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027
14	0.0000	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027
15	0.0000	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027
16	0.0000	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027
17	0.0000	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027
18	0.0000	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027
19	0.0000	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027
20	0.0000	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027
21	0.0000	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027
22	0.0000	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027
23	0.0000	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027
24	0.0000	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027
25	0.0000	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027
26	0.0000	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027
27	0.0000	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027
28	0.0000	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027
29	0.0000	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027
30	0.0000	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027
31	0.0000	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027
32	0.0000	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027
33	0.0000	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027
34	0.0000	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027
35	0.0000	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027
36	0.0000	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027
37	0.0000	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027
38	0.0000	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027
39	0.0000	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027
40	0.0000	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027
41	0.0000	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027
42	0.0000	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027
43	0.0000	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027
44	0.0000	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027
45	0.0000	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027

M	N= 18	19	20	21	22	23	24	25	26	27	28	29	30	31	32
1	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
2	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027
3	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027
4	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027
5	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027
6	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027
7	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027
8	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027
9	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027
10	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027
11	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027
12	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027
13	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027
14	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027
15	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027
16	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027
17	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027
18	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027
19	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027
20	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027
21	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027
22	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027
23	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027
24	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027
25	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027
26	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027
27	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027
28	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027
29	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027
30	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027
31	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027
32	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027
33	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027
34	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027
35	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027
36	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027
37	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027
38	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027
39	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027
40	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027
41	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027
42	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027
43	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027
44	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027
45	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027	0.0027

TIME PARAMETERS:

DURATION OF THE DISPOSAL, TREL = 30.00 SECONDS

DURATION OF THE SIMULATION, TSTOP = 3600.00 SECONDS

LONG-TERM TIME STEP USED IN THE SIMULATION, DTL = 300.00 SECONDS

BARGE DESCRIPTION:

LENGTH OF BARGE, BARGL = 60. FT

WIDTH OF BARGE, BARGW = 30. FT

DRAFT OF LOADED BARGE, DREL1 = 6.00 FT

DRAFT OF UNLOADED BARGE, DREL2 = 3.50 FT

MODEL COEFFICIENTS READ FROM INPUT:

TURBULENT THERMAL ENTRAINMENT	ALPHA0	=	0.2350
SETTLING COEFFICIENT	BETA	=	0.0000
APPARENT MASS COEFFICIENT	CM	=	1.0000
DRAG COEFFICIENT FOR A SPHERE	CD	=	0.5000
RATIO--CLOUD/AMBIENT DENSITY GRADIENTS	GAMA	=	0.2500
FORM DRAG FOR COLLAPSING CLOUD	CDRAG	=	1.0000
SKIN FRICTION FOR COLLAPSING CLOUD	CFRIC	=	0.0100
DRAG FOR AN ELLIPSOIDAL WEDGE	CD3	=	0.1000
DRAG FOR A PLATE	CD4	=	1.0000
ENTRAINMENT IN COLLAPSE	ALPHAC	=	0.1000
FRICTION BETWEEN CLOUD AND BOTTOM	FRICTN	=	0.0100
4/3 LAW HORIZ. DIFF. DISSIPATION FACTOR	ALAMDA	=	0.0010
UNSTRATIFIED WATER VERT. DIFF. COEF.	AKY0	=	0.0250
STRIPPING COEF. OF FINES DURING CONVERTIVE DESCENT		=	0.0030

MATERIAL DESCRIPTION: 4 SOLIDS FRACTIONS

L A Y E R 1

DESCRIPTION	SPEC. GRAV. OR DENSITY (GM/CC)	VOLUMETRIC CONCENTRATION (VOL/VOL)	FALL VELOCITY (FPS)	DEPOSITIONAL VOID RATIO	CHARACTER
GRAVEL	2.700	0.1500E-02	1.00000	0.5000	NONCOHESIVE
	CRITICAL SHEAR STRESS FOR DEPOSITION = 99.00 LBS/SQ. FT.				
	SEDIMENT FRACTION WILL NOT BE STRIPPED DURING CONVECTIVE DESCENT.				
SAND	2.700	0.6950E-01	0.10000	0.6000	NONCOHESIVE
	CRITICAL SHEAR STRESS FOR DEPOSITION = 0.2500E-01 LBS/SQ. FT.				
	SEDIMENT FRACTION WILL BE STRIPPED DURING CONVECTIVE DESCENT.				
SILT	2.650	0.4153	0.01000	5.000	COHESIVE
	CRITICAL SHEAR STRESS FOR DEPOSITION = 0.8000E-02 LBS/SQ. FT.				
	SEDIMENT FRACTION WILL BE STRIPPED DURING CONVECTIVE DESCENT.				
CLAY	2.650	0.1384	0.00200	8.000	COHESIVE
	CRITICAL SHEAR STRESS FOR DEPOSITION = 0.1000E-02 LBS/SQ. FT.				
	SEDIMENT FRACTION WILL BE STRIPPED DURING CONVECTIVE DESCENT.				

TOXICITY ANALYSIS DATA:

CONCENTRATIONS OF FLUID IN TERMS OF PERCENT OF THE DREDGED MATERIAL
FOLLOWING INITIAL MIXING ARE COMPUTED FOR WATER QUALITY EVALUATIONS.

THE INITIAL CONCENTRATION OF FLUID IS 100. PERCENT
AND ITS BACKGROUND CONCENTRATION IS 0.000E+00 PERCENT.

THE DILUTION REQUIRED TO MEET TOXICITY STANDARD IS 0.422000 PERCENT.
(TYPICALLY, 1 PERCENT OF THE LC50)

DESCRIPTION	SPEC. GRAV. OR DENSITY (GM/CC)	VOLUMETRIC CONCENTRATION (VOL/VOL)
FLUID	1.020	0.3753

DISCHARGE PARAMETERS:

VOLUME OF LAYER 1 = 500.0 CU YD

INITIAL RADIUS OF CLOUD, RB = 18.61052 FT

INITIAL DEPTH OF CLOUD CENTROID, DREL = 11.73 FT

INITIAL CLOUD VELOCITIES...

X-DIRECTION (FROM TOP TO BOTTOM OF GRID), CU(1) = 1.500 FPS

Y-DIRECTION (FROM SURFACE TO BOTTOM), CV(1) = 0.8333E-01 FPS

Z-DIRECTION (FROM LEFT TO RIGHT OF GRID), CW(1) = 0.0000E+00 FPS

BULK PARAMETERS:

BULK DENSITY, ROO = 2.041811 G/CC

AGGREGATE OR BULK VOIDS RATIO, BVOID = 5.164

CONVECTIVE DESCENT PHASE:

IN TRIAL #1 THE DESCENT PHASE TIME STEP (DT) WAS 0.24027357E-01 SECONDS.

THE TOTAL NUMBER OF INTEGRATION TIME STEPS (ISTEP) WAS 278.

THE BOTTOM WAS ENCOUNTERED DURING CONVECTIVE DESCENT.

THE DISCHARGE DID NOT OBTAIN A NEUTRALLY BUOYANT CONDITION DURING CONVECTIVE DESCENT.

CLOUD COLLAPSE PHASE:

IN TRIAL #1 THE COLLAPSE PHASE TIME STEP (DT) WAS 0.24027357E-01 SECONDS.
THE TOTAL NUMBER OF INTEGRATION TIME STEPS (ISTEP) FOR CONVECTIVE DESCENT AND COLAPSE WAS 1040.
THE INTEGRATION TIME STEP NUMBER WHEN THE BED WAS ENCOUNTERED (IBED) WAS 278.
THE BOTTOM WAS ENCOUNTERED DURING CONVECTIVE DESCENT.
DIFFUSION OF THE DISCHARGE IS GREATER THAN DYNAMIC SPREADING FROM THE COLLAPSE.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID X-LOCATION (FT)	CLOUD CENTROID Z-LOCATION (FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	T O T A L M A S S (CU FT)	ENTRAINED MASS (CU FT)	TIME STEP WHEN THIS CLOUD WAS CREATED	TIME STEP WHEN PREVIOUS CLOUD WAS CREATED
NEW CLOUD CREATED, NTCLD(K) (K = 1) = 1									
37.50	453.6	300.0	93.58	120.0	0.1000E-02	0.7607	0.0000E+00	313	278
NEW CLOUD CREATED, NTCLD(K) (K = 1) = 2									
40.00	456.1	300.0	162.9	120.0	0.1000E-02	4.092	0.0000E+00	417	313
NEW CLOUD CREATED, NTCLD(K) (K = 1) = 3									
42.49	458.4	300.0	217.1	120.0	0.1000E-02	5.132	0.0000E+00	521	417
NEW CLOUD CREATED, NTCLD(K) (K = 1) = 4									
44.99	460.6	300.0	251.2	120.0	0.1000E-02	4.164	0.0000E+00	625	521
NEW CLOUD CREATED, NTCLD(K) (K = 1) = 5									
47.49	462.8	300.0	274.2	120.0	0.1000E-02	2.727	0.0000E+00	729	625
NEW CLOUD CREATED, NTCLD(K) (K = 1) = 6									
49.99	464.9	300.0	292.0	120.0	0.1000E-02	1.602	0.0000E+00	833	729
NEW CLOUD CREATED, NTCLD(K) (K = 1) = 7									
52.49	466.9	300.0	307.0	120.0	0.1000E-02	0.8789	0.0000E+00	937	833
NEW CLOUD CREATED, NTCLD(K) (K = 1) = 8									
54.97	468.9	300.0	320.1	114.9	5.106	0.8932	0.0000E+00	1040	937

NOTE -- When all solid material has settled from a cloud, the cloud is erased and
the remaining clouds for this solids type are renumbered.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID X-LOCATION (FT)	CLOUD CENTROID Z-LOCATION (FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	T O T A L M A S S (CU FT)	ENTRAINED MASS (CU FT)	TIME STEP WHEN THIS CLOUD WAS CREATED	TIME STEP WHEN PREVIOUS CLOUD WAS CREATED
NEW CLOUD CREATED, NTCLD(K) (K = 2) = 1									
32.50	448.4	300.0	46.26	4.750	32.08	12.20	0.0000E+00	105	1
NEW CLOUD CREATED, NTCLD(K) (K = 2) = 2									
35.00	451.1	300.0	62.64	36.83	39.52	10.76	0.0000E+00	209	105
NEW CLOUD CREATED, NTCLD(K) (K = 2) = 3									
37.50	453.6	300.0	93.58	76.35	14.46	14.92	0.0000E+00	313	278
NEW CLOUD CREATED, NTCLD(K) (K = 2) = 4									
40.00	456.1	300.0	162.9	90.82	14.56	18.92	0.0000E+00	417	313
NEW CLOUD CREATED, NTCLD(K) (K = 2) = 5									
42.49	458.4	300.0	217.1	105.4	3.481	8.222	0.0000E+00	521	417
NEW CLOUD CREATED, NTCLD(K) (K = 2) = 6									
44.99	460.6	300.0	251.2	108.9	1.250	3.839	0.0000E+00	625	521
NEW CLOUD CREATED, NTCLD(K) (K = 2) = 7									
47.49	462.8	300.0	274.2	110.1	0.6355	2.223	0.0000E+00	729	625
NEW CLOUD CREATED, NTCLD(K) (K = 2) = 8									
49.99	464.9	300.0	292.0	110.7	0.4105	1.558	0.0000E+00	833	729
NEW CLOUD CREATED, NTCLD(K) (K = 2) = 9									
52.49	466.9	300.0	307.0	111.1	0.3031	1.222	0.0000E+00	937	833
NEW CLOUD CREATED, NTCLD(K) (K = 2) = 10									
54.97	468.9	300.0	320.1	114.9	5.106	864.4	0.0000E+00	1040	937

NOTE -- When all solid material has settled from a cloud, the cloud is erased and
the remaining clouds for this solids type are renumbered.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID X-LOCATION (FT)	CLOUD CENTROID Z-LOCATION (FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	T O T A L M A S S (CU FT)	ENTRAINED MASS (CU FT)	TIME STEP WHEN THIS CLOUD WAS CREATED	TIME STEP WHEN PREVIOUS CLOUD WAS CREATED
NEW CLOUD CREATED, NTCLD(K) (K = 3) = 1									
32.50	448.4	300.0	46.26	4.750	32.08	72.89	0.0000E+00	105	1
NEW CLOUD CREATED, NTCLD(K) (K = 3) = 2									
35.00	451.1	300.0	62.64	36.83	39.52	64.30	0.0000E+00	209	105
NEW CLOUD CREATED, NTCLD(K) (K = 3) = 3									
37.50	453.6	300.0	93.58	76.35	14.46	89.15	0.0000E+00	313	278
NEW CLOUD CREATED, NTCLD(K) (K = 3) = 4									
40.00	456.1	300.0	162.9	90.82	14.56	113.1	0.0000E+00	417	313
NEW CLOUD CREATED, NTCLD(K) (K = 3) = 5									
42.49	458.4	300.0	217.1	105.4	3.481	49.13	0.0000E+00	521	417
NEW CLOUD CREATED, NTCLD(K) (K = 3) = 6									
44.99	460.6	300.0	251.2	108.9	1.250	22.94	0.0000E+00	625	521
NEW CLOUD CREATED, NTCLD(K) (K = 3) = 7									
47.49	462.8	300.0	274.2	110.1	0.6355	13.28	0.0000E+00	729	625
NEW CLOUD CREATED, NTCLD(K) (K = 3) = 8									
49.99	464.9	300.0	292.0	110.7	0.4105	9.306	0.0000E+00	833	729
NEW CLOUD CREATED, NTCLD(K) (K = 3) = 9									
52.49	466.9	300.0	307.0	111.1	0.3031	7.298	0.0000E+00	937	833
NEW CLOUD CREATED, NTCLD(K) (K = 3) = 10									
54.97	468.9	300.0	320.1	114.9	5.106	5165.	0.0000E+00	1040	937

NOTE -- When all solid material has settled from a cloud, the cloud is erased and
the remaining clouds for this solids type are renumbered.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID X-LOCATION (FT)	CLOUD CENTROID Z-LOCATION (FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	T O T A L M A S S (CU FT)	ENTRAINED MASS (CU FT)	TIME STEP WHEN THIS CLOUD WAS CREATED	TIME STEP WHEN PREVIOUS CLOUD WAS CREATED
NEW CLOUD CREATED, NTCLD(K) (K = 4) = 1									
32.50	448.4	300.0	46.26	4.750	32.08	24.29	0.0000E+00	105	1
NEW CLOUD CREATED, NTCLD(K) (K = 4) = 2									
35.00	451.1	300.0	62.64	36.83	39.52	21.43	0.0000E+00	209	105
NEW CLOUD CREATED, NTCLD(K) (K = 4) = 3									
37.50	453.6	300.0	93.58	76.35	14.46	29.71	0.0000E+00	313	278
NEW CLOUD CREATED, NTCLD(K) (K = 4) = 4									
40.00	456.1	300.0	162.9	90.82	14.56	37.68	0.0000E+00	417	313
NEW CLOUD CREATED, NTCLD(K) (K = 4) = 5									
42.49	458.4	300.0	217.1	105.4	3.481	16.37	0.0000E+00	521	417
NEW CLOUD CREATED, NTCLD(K) (K = 4) = 6									
44.99	460.6	300.0	251.2	108.9	1.250	7.644	0.0000E+00	625	521
NEW CLOUD CREATED, NTCLD(K) (K = 4) = 7									
47.49	462.8	300.0	274.2	110.1	0.6355	4.425	0.0000E+00	729	625
NEW CLOUD CREATED, NTCLD(K) (K = 4) = 8									
49.99	464.9	300.0	292.0	110.7	0.4105	3.103	0.0000E+00	833	729
NEW CLOUD CREATED, NTCLD(K) (K = 4) = 9									
52.49	466.9	300.0	307.0	111.1	0.3031	2.432	0.0000E+00	937	833
NEW CLOUD CREATED, NTCLD(K) (K = 4) = 10									
54.97	468.9	300.0	320.1	114.9	5.106	1721.	0.0000E+00	1040	937

NOTE -- When all solid material has settled from a cloud, the cloud is erased and
the remaining clouds for this solids type are renumbered.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID X-LOCATION (FT)	CLOUD CENTROID Z-LOCATION (FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	T O T A L M A S S (CU FT)	ENTRAINED MASS (CU FT)	TIME STEP WHEN THIS CLOUD WAS CREATED	TIME STEP WHEN PREVIOUS CLOUD WAS CREATED
NEW CLOUD CREATED, NTCLD(K) (K = 5) = 1									
54.97	468.9	300.0	320.1	114.9	5.106	5067.	0.0000E+00	1040	1

NOTE -- When all solid material has settled from a cloud, the cloud is erased and the remaining clouds for this solids type are renumbered.

LONG TERM DIFFUSION RESULTS:

BEGIN LONG TERM SIMULATION OF FATE OF GRAVEL

SUMMARY OF GRAVEL DISTRIBUTIONS AFTER 300.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.00000E+00
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 20.250

COMPUTATIONS FOR GRAVEL TERMINATED AT 300.00 SEC. ELAPSED TIME...MATERIAL SETTLED TO BOTTOM

BOTTOM ACCUMULATION OF GRAVEL (CU FT/GRID SQUARE) , 300.00 SECONDS AFTER DUMP

...MULTIPLY DISPLAYED VALUES BY 1.000 (LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)

M N=	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31
2	000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000																													
3	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		00000
4	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		00000
5	0000	0	0	0	0	0	0	0	0	+	+	+	+	+	0	0	0	0	0	0	0	0	0	0	0	0	0	0		00000
6	0000	0	0	0	0	0	0	0	+	.13	3.7	11	3.7	.13	+	0	0	0	0	0	0	0	0	0	0	0	0	0		00000
7	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		00000
8	0000	0	0	0	0	0	0	0	.	+	.17	.53	.17	+	.	0	0	0	0	0	0	0	0	0	0	0	0	0		00000
9	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		00000
10	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		00000
11	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		00000
12	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		00000
13	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		00000
14	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		00000
15	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		00000
16	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		00000
17	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		00000
18	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		00000
19	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		00000
20	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		00000
21	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		00000
22	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		00000
23	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		00000
24	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		00000
25	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		00000
26	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		00000
27	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		00000
28	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		00000
29	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		00000
30	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		00000
31	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		00000
32	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		00000
33	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		00000
34	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		00000
35	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		00000
36	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		00000
37	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		00000
38	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		00000
39	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		00000
40	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		00000
41	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		00000
42	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		00000
43	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		00000
44	000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000																													

THICKNESS (FT) OF GRAVEL ACCUMULATED ON BOTTOM, 300.00 SECONDS AFTER DUMP
...MULTIPLY DISPLAYED VALUES BY 0.1000E-02 (LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)

M N=	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31
2	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O
3	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
4	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
5	O	0	0	0	0	0	0	0	.	+	+	+	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
6	O	0	0	0	0	0	0	+	.08	2.2	6.8	2.2	.08	+	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
7	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
8	O	0	0	0	0	0	0	.	+	.10	.31	.10	+	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
9	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
10	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
11	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
12	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
13	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
14	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
15	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
16	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
17	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
18	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
19	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
20	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
21	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
22	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
23	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
24	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
25	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
26	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
27	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
28	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
29	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
30	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
31	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
32	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
33	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
34	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
35	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
36	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
37	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
38	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
39	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
40	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
41	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
42	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
43	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
44	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O

BEGIN LONG TERM SIMULATION OF FATE OF SAND

SUMMARY OF SAND DISTRIBUTIONS AFTER 300.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 43.344
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 893.27

SUMMARY OF SAND DISTRIBUTIONS AFTER 600.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 21.424
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 915.19

SUMMARY OF SAND DISTRIBUTIONS AFTER 900.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 12.014
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 924.60

CONCENTRATIONS ABOVE BACKGROUND OF SAND (MG/L) IN THE CLOUD 900.00 SECONDS AFTER DUMP

60.00 FT BELOW THE WATER SURFACE

...MULTIPLY DISPLAYED VALUES BY 1.000 (LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)

M N=	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	0	0	0	0	0	0	.	.	.	.	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	0	0	0	.	.	+	.02	.25	1.4	4.2	6.1	4.2	1.4	.25	.02	+	.	.	0	0	0	0	0	0	0	0	0	0	0	0
14	0	0	0	.	+	+	.06	.67	4.0	12	18	12	4.0	.67	.06	+	+	.	0	0	0	0	0	0	0	0	0	0	0	0
15	0	0	0	0	0	.	.	.	+	+	+	+	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
18	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
19	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
20	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
21	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
22	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
23	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
24	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
25	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
26	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
27	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
28	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
29	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
30	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
31	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
32	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
33	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
34	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
35	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
36	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
37	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
38	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
39	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
40	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
41	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
42	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
43	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
44	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0

CONCENTRATIONS ABOVE BACKGROUND OF SAND (MG/L) IN THE CLOUD 900.00 SECONDS AFTER DUMP

119.00 FT BELOW THE WATER SURFACE

...MULTIPLY DISPLAYED VALUES BY 1.000 (LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)

M N=	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	.	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0	0	0
12	.	+	+	+	+	+	.01	.02	.03	.04	.04	.04	.03	.02	.01	+	+	+	+	+	0	0	0	0	0	0	0	0	0	0
13	+	+	+	.01	.04	.10	.24	.58	1.4	2.9	3.7	2.9	1.4	.58	.24	.10	.04	.01	+	+	0	0	0	0	0	0	0	0	0	0
14	+	+	+	.02	.05	.14	.34	.95	2.8	6.5	8.8	6.5	2.8	.95	.34	.14	.05	.02	+	+	0	0	0	0	0	0	0	0	0	0
15	.	+	+	+	+	.01	.02	.04	.07	.09	.10	.09	.07	.04	.02	.01	+	+	+	+	0	0	0	0	0	0	0	0	0	0
16	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	0	0	0	0	0	0	0	0	0
17	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
18	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
19	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
20	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
21	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
22	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
23	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
24	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
25	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
26	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
27	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
28	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
29	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
30	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
31	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
32	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
33	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
34	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
35	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
36	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
37	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
38	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
39	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
40	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
41	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
42	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
43	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
44	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0

```
BOTTOM ACCUMULATION OF SAND     (CU FT/GRID SQUARE) ,    900.00 SECONDS AFTER DUMP
...MULTIPLY DISPLAYED VALUES BY   1.000         (LEGEND... + = .LT. .01   . = .LT. .0001   0 = .LT. .000001)
M N=  2   3   4   5   6   7   8   9  10  11  12  13  14  15  16  17  18  19  20  21  22  23  24  25  26  27  28  29  30  31
 2 OOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOO
 3 OOOO   .   .   .   .   .   .   .   .   .   .   .   .   .   .   .   .   .   .   .   .   .   .   0   0   0   0   0   00000
 4 OOOO   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   .   .   .   .   .   00000
 5 OOOO .01 .02 .04 .06 .10 .14 .19 .24 .29 .32 .33 .32 .29 .24 .19 .14 .10 .06 .04 .02 .01   +   +   +   +   +   .   .0000
 6 OOOO .16 .31 .55 .91 1.4 2.0 2.7 3.4 4.0 4.4 4.6 4.4 4.0 3.4 2.7 2.0 1.4 .91 .55 .31 .16 .08 .03 .01   +   +   +   +0000
 7 OOOO .81 1.5 2.6 4.3 6.7  10  13  17  20  22  23  22  20  17  13  10 6.7 4.3 2.6 1.5 .81 .40 .18 .08 .03 .01   +   +0000
 8 OOOO 1.3 2.5 4.4 7.2  11  16  22  28  34  39  41  39  34  28  22  16  11 7.2 4.4 2.5 1.3 .67 .31 .13 .05 .02   +   +0000
 9 OOOO .77 1.4 2.5 4.1 6.4 9.3  13  16  19  21  22  21  19  16  13 9.3 6.4 4.1 2.5 1.4 .77 .38 .18 .07 .03 .01   +   +0000
10 OOOO .15 .29 .51 .84 1.3 1.9 2.6 3.3 4.0 4.6 4.8 4.6 4.0 3.3 2.6 1.9 1.3 .84 .51 .29 .15 .07 .03 .01   +   +   +   +0000
11 OOOO .01 .02 .04 .07 .14 .25 .45 .89 1.8 3.7 5.0 3.7 1.8 .89 .45 .25 .14 .07 .04 .02 .01   +   +   +   +   +   .   .0000
12 OOOO   +   +   +   + .01 .02 .05 .08 .12 .15 .16 .15 .12 .08 .05 .02 .01   +   +   +   +   +   +   .   .   .   .   .0000
13 OOOO   +   +   +   + .01 .02 .05 .12 .29 .59 .77 .59 .29 .12 .05 .02 .01   +   +   +   +   .   .   .   .   .   0   00000
14 OOOO   +   +   +   + .01 .02 .07 .19 .57 1.3 1.8 1.3 .57 .19 .07 .02 .01   +   +   +   +   .   .   .   .   0   0   00000
15 OOOO   .   .   +   +   +   +   + .01 .01 .01 .02 .01 .01 .01   +   +   +   +   +   .   .   .   .   .   0   0   0   00000
16 OOOO   .   .   .   .   .   .   +   +   +   +   +   +   +   +   +   .   .   .   .   .   .   0   0   0   0   0   0   00000
17 OOOO   0   0   0   0   0   0   .   .   .   .   .   .   .   .   .   0   0   0   0   0   0   0   0   0   0   0   0   00000
18 OOOO   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   00000
19 OOOO   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   00000
20 OOOO   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   00000
21 OOOO   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   00000
22 OOOO   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   00000
23 OOOO   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   00000
24 OOOO   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   00000
25 OOOO   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   00000
26 OOOO   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   00000
27 OOOO   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   00000
28 OOOO   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   00000
29 OOOO   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   00000
30 OOOO   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   00000
31 OOOO   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   00000
32 OOOO   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   00000
33 OOOO   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   00000
34 OOOO   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   00000
35 OOOO   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   00000
36 OOOO   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   00000
37 OOOO   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   00000
38 OOOO   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   00000
39 OOOO   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   00000
40 OOOO   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   00000
41 OOOO   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   00000
42 OOOO   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   00000
43 OOOO   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   00000
44 OOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOO
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SMALL CLOUDS AT 900.00 SECONDS ELAPSED TIME FOR SAND

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID	LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	1259.	300.0	6.974	0.0000E+00	96.85	45.01	74.99	0.100000
2	1259.	300.0	4.259	0.0000E+00	117.6	54.61	65.39	0.100000
3	1259.	300.0	0.3379	0.0000E+00	155.1	104.9	15.14	0.100000
4	1259.	300.0	0.4428	0.0000E+00	235.3	102.6	17.40	0.100000
5	1259.	300.0	0.7339E-03	0.0000E+00	296.0	114.2	5.840	0.100000
6	1259.	300.0	0.1295E-04	0.0000E+00	333.5	116.2	3.838	0.100000
7	1259.	300.0	0.2391E-05	0.0000E+00	358.6	116.6	3.387	0.100000
8	1259.	300.0	0.8961E-06	0.0000E+00	377.8	116.8	3.165	0.100000
9	1259.	300.0	0.3717E-06	0.0000E+00	393.8	117.0	2.952	0.100000

SUMMARY OF SAND DISTRIBUTIONS AFTER 1200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 7.3795
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 929.23

SUMMARY OF SAND DISTRIBUTIONS AFTER 1500.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 4.6301
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 931.98

SUMMARY OF SAND DISTRIBUTIONS AFTER 1800.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 2.8773
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 933.73

CONCENTRATIONS ABOVE BACKGROUND OF SAND (MG/L) IN THE CLOUD 1800.00 SECONDS AFTER DUMP

60.00 FT BELOW THE WATER SURFACE

...MULTIPLY DISPLAYED VALUES BY 1.000 (LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)

M N=	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
18	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
19	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
20	0	0	0	.	.	.	.	+	+	+	+	+	+	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0
21	0	.	.	+	+	+	.02	.07	.15	.24	.27	.24	.15	.07	.02	+	+	+	.	0	0	0	0	0	0	0	0	0	0	0
22	.	.	+	+	.01	.07	.27	.74	1.5	2.3	2.7	2.3	1.5	.74	.27	.07	.01	+	+	0	0	0	0	0	0	0	0	0	0	0
23	0	.	.	+	+	+	.02	.07	.15	.23	.27	.23	.15	.07	.02	+	+	+	.	0	0	0	0	0	0	0	0	0	0	0
24	0	0	0	.	.	.	.	+	+	+	+	+	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0
25	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
26	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
27	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
28	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
29	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
30	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
31	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
32	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
33	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
34	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
35	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
36	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
37	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
38	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
39	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
40	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
41	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
42	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
43	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
44	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0

CONCENTRATIONS ABOVE BACKGROUND OF SAND (MG/L) IN THE CLOUD 1800.00 SECONDS AFTER DUMP

119.00 FT BELOW THE WATER SURFACE

...MULTIPLY DISPLAYED VALUES BY 1.000 (LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)

M N=	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
18	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
19	0	0	0	0	.	.	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0
20	0	.	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0
21	0	.	.	+	+	+	+	.03	.07	.14	.21	.24	.21	.14	.07	.03	+	+	+	+	0	0	0	0	0	0	0	0	0	0
22	0	.	+	+	+	.01	.07	.24	.61	1.2	1.8	2.1	1.8	1.2	.61	.24	.07	.01	+	+	0	0	0	0	0	0	0	0	0	0
23	0	.	.	+	+	+	+	.02	.07	.14	.20	.23	.20	.14	.07	.02	+	+	+	+	0	0	0	0	0	0	0	0	0	0
24	0	.	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0
25	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
26	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
27	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
28	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
29	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
30	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
31	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
32	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
33	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
34	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
35	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
36	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
37	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
38	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
39	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
40	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
41	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
42	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
43	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
44	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0

BOTTOM ACCUMULATION OF SAND (CU FT/GRID SQUARE) , 1800.00 SECONDS AFTER DUMP

...MULTIPLY DISPLAYED VALUES BY 1.000 (LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)

M N=	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30 31
2	0000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000																												
3	0000	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0	0	00000
4	0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	00000
5	0000	.01	.02	.04	.06	.10	.14	.19	.24	.29	.32	.33	.32	.29	.24	.19	.14	.10	.06	.04	.02	.01	+	+	+	+	+	.	.0000
6	0000	.16	.31	.55	.91	1.4	2.0	2.7	3.4	4.0	4.4	4.6	4.4	4.0	3.4	2.7	2.0	1.4	.91	.55	.31	.16	.08	.03	.01	+	+	+	+0000
7	0000	.81	1.5	2.6	4.3	6.7	10	13	17	20	22	23	22	20	17	13	10	6.7	4.3	2.6	1.5	.81	.40	.18	.08	.03	.01	+	+0000
8	0000	1.3	2.5	4.4	7.2	11	16	22	28	34	39	41	39	34	28	22	16	11	7.2	4.4	2.5	1.3	.67	.31	.13	.05	.02	+	+0000
9	0000	.77	1.4	2.5	4.1	6.4	9.3	13	16	19	21	22	21	19	16	13	9.3	6.4	4.1	2.5	1.4	.77	.38	.18	.07	.03	.01	+	+0000
10	0000	.15	.29	.51	.84	1.3	1.9	2.6	3.3	4.0	4.6	4.8	4.6	4.0	3.3	2.6	1.9	1.3	.84	.51	.29	.15	.07	.03	.01	+	+	+	+0000
11	0000	.01	.02	.04	.07	.14	.25	.45	.89	1.8	3.7	5.0	3.7	1.8	.89	.45	.25	.14	.07	.04	.02	.01	+	+	+	+	+	.	.0000
12	0000	+	+	+	+	.01	.02	.05	.08	.12	.15	.16	.15	.12	.08	.05	.02	.01	+	+	+	+	+	+	.	.	.	.	.0000
13	0000	+	+	+	+	.01	.02	.05	.12	.29	.59	.77	.59	.29	.12	.05	.02	.01	+	+	+	+	.	.	.	.	.	0	00000
14	0000	+	+	+	+	.01	.02	.07	.19	.57	1.3	1.8	1.3	.57	.19	.07	.02	.01	+	+	+	+	.	.	.	.	0	0	00000
15	0000	.	+	+	+	+	+	+	.01	.01	.02	.02	.02	.01	.01	+	+	+	+	+	+	.	.	.	.	0	0	0	00000
16	0000	.	+	+	+	+	+	.03	.10	.32	.66	.84	.66	.32	.10	.03	+	+	+	+	+	.	.	.	.	0	0	0	00000
17	0000	.	+	+	+	+	+	.01	.05	.15	.29	.36	.29	.15	.05	.01	+	+	+	+	+	.	.	.	.	0	0	0	00000
18	0000	.	.	+	+	+	+	+	+	+	.01	.01	.01	+	+	+	+	+	+	+	.	.	.	.	0	0	0	0	00000
19	0000	.	.	+	+	+	+	.03	.10	.26	.45	.54	.45	.26	.10	.03	+	+	+	+	.	.	.	.	.	0	0	0	00000
20	0000	.	.	+	+	+	+	+	.02	.04	.07	.09	.07	.04	.02	+	+	+	+	+	.	.	.	.	0	0	0	0	00000
21	0000	.	.	.	+	+	+	+	.01	.02	.03	.03	.03	.02	.01	+	+	+	+	.	.	.	.	.	0	0	0	0	00000
22	0000	.	.	+	+	+	.01	.03	.08	.17	.25	.29	.25	.17	.08	.03	.01	+	+	+	.	.	.	.	0	0	0	0	00000
23	0000	.	.	.	.	+	+	+	.01	.01	.02	.03	.02	.01	.01	+	+	+	.	.	.	.	.	0	0	0	0	0	00000
24	0000	0	.	.	.	.	.	.	.	.	.	+	.	.	.	.	.	.	.	.	.	0	0	0	0	0	0	0	00000
25	0000	0	0	0	0	0	0	0	0	.	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
26	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
27	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
28	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
29	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
30	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
31	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
32	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
33	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
34	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
35	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
36	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
37	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
38	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
39	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
40	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
41	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
42	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
43	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
44	0000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000																												

SMALL CLOUDS AT 1800.00 SECONDS ELAPSED TIME FOR SAND

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID	LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	2100.	300.0	1.913	0.0000E+00	161.8	54.54	65.46	0.100000
2	2100.	300.0	0.9638	0.0000E+00	186.4	63.26	56.74	0.100000
3	2100.	300.0	0.5959E-04	0.0000E+00	229.9	112.7	7.256	0.100000
4	2100.	300.0	0.3912E-03	0.0000E+00	320.4	110.4	9.553	0.100000

SUMMARY OF SAND DISTRIBUTIONS AFTER 2100.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 1.7548
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 934.86

SUMMARY OF SAND DISTRIBUTIONS AFTER 2400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 1.0475
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 935.56

SUMMARY OF SAND DISTRIBUTIONS AFTER 2700.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.61107
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 936.00

MAX CONC IS 0.00000004 OUTPUT SUPPRESSED AT 60.00 FT

MAX CONC IS 0.00000008 OUTPUT SUPPRESSED AT 119.00 FT

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BOTTOM ACCUMULATION OF SAND     (CU FT/GRID SQUARE) ,   2700.00 SECONDS AFTER DUMP
...MULTIPLY DISPLAYED VALUES BY   1.000         (LEGEND... + = .LT. .01   . = .LT. .0001   0 = .LT. .000001)
M N=  2   3   4   5   6   7   8   9  10  11  12  13  14  15  16  17  18  19  20  21  22  23  24  25  26  27  28  29  30  31
 2 00000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000
 3 0000   .   .   .   .   .   .   .   .   .   .   .   .   .   .   .   .   .   .   .   .   .   .   0   0   0   0   0  00000
 4 0000   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   .   .   .   .   .  00000
 5 0000 .01 .02 .04 .06 .10 .14 .19 .24 .29 .32 .33 .32 .29 .24 .19 .14 .10 .06 .04 .02 .01   +   +   +   +   +   .  .0000
 6 0000 .16 .31 .55 .91 1.4 2.0 2.7 3.4 4.0 4.4 4.6 4.4 4.0 3.4 2.7 2.0 1.4 .91 .55 .31 .16 .08 .03 .01   +   +   +  +0000
 7 0000 .81 1.5 2.6 4.3 6.7  10  13  17  20  22  23  22  20  17  13  10 6.7 4.3 2.6 1.5 .81 .40 .18 .08 .03 .01   +  +0000
 8 0000 1.3 2.5 4.4 7.2  11  16  22  28  34  39  41  39  34  28  22  16  11 7.2 4.4 2.5 1.3 .67 .31 .13 .05 .02   +  +0000
 9 0000 .77 1.4 2.5 4.1 6.4 9.3  13  16  19  21  22  21  19  16  13 9.3 6.4 4.1 2.5 1.4 .77 .38 .18 .07 .03 .01   +  +0000
10 0000 .15 .29 .51 .84 1.3 1.9 2.6 3.3 4.0 4.6 4.8 4.6 4.0 3.3 2.6 1.9 1.3 .84 .51 .29 .15 .07 .03 .01   +   +   +  +0000
11 0000 .01 .02 .04 .07 .14 .25 .45 .89 1.8 3.7 5.0 3.7 1.8 .89 .45 .25 .14 .07 .04 .02 .01   +   +   +   +   +   .  .0000
12 0000   +   +   +   + .01 .02 .05 .08 .12 .15 .16 .15 .12 .08 .05 .02 .01   +   +   +   +   +   +   .   .   .   .  .0000
13 0000   +   +   +   + .01 .02 .05 .12 .29 .59 .77 .59 .29 .12 .05 .02 .01   +   +   +   +   .   .   .   .   .   0  00000
14 0000   +   +   +   + .01 .02 .07 .19 .57 1.3 1.8 1.3 .57 .19 .07 .02 .01   +   +   +   +   .   .   .   .   0   0  00000
15 0000   .   +   +   +   +   +   + .01 .01 .02 .02 .02 .01 .01   +   +   +   +   +   +   .   .   .   .   0   0   0  00000
16 0000   .   +   +   +   +   + .03 .10 .32 .66 .84 .66 .32 .10 .03   +   +   +   +   +   .   .   .   .   0   0   0  00000
17 0000   .   +   +   +   +   + .01 .05 .15 .29 .36 .29 .15 .05 .01   +   +   +   +   +   .   .   .   .   0   0   0  00000
18 0000   .   .   +   +   +   +   +   +   + .01 .01 .01   +   +   +   +   +   +   +   .   .   .   .   0   0   0   0  00000
19 0000   .   .   +   +   +   + .03 .10 .26 .45 .54 .45 .26 .10 .03   +   +   +   +   .   .   .   .   .   0   0   0  00000
20 0000   .   .   +   +   +   +   + .02 .04 .07 .09 .07 .04 .02   +   +   +   +   +   .   .   .   .   0   0   0   0  00000
21 0000   .   .   .   +   +   +   + .01 .02 .03 .03 .03 .02 .01   +   +   +   +   .   .   .   .   .   0   0   0   0  00000
22 0000   .   .   +   +   + .01 .03 .08 .17 .25 .29 .25 .17 .08 .03 .01   +   +   +   .   .   .   .   0   0   0   0  00000
23 0000   .   .   .   +   +   +   + .01 .02 .02 .03 .02 .02 .01   +   +   +   +   .   .   .   .   0   0   0   0   0  00000
24 0000   .   .   .   +   +   +   + .02 .03 .04 .05 .04 .03 .02   +   +   +   +   .   .   .   0   0   0   0   0   0  00000
25 0000   .   .   +   +   + .01 .02 .05 .09 .12 .13 .12 .09 .05 .02 .01   +   +   +   .   .   .   0   0   0   0   0  00000
26 0000   .   .   .   +   +   +   +   + .01 .01 .01 .01 .01   +   +   +   +   +   .   .   .   0   0   0   0   0   0  00000
27 0000   .   .   +   +   +   + .01 .02 .03 .04 .04 .04 .03 .02 .01   +   +   +   +   .   .   .   0   0   0   0   0  00000
28 0000   .   +   +   +   +   + .01 .02 .04 .05 .05 .05 .04 .02 .01   +   +   +   +   +   .   .   0   0   0   0   0  00000
29 0000   .   .   +   +   +   +   +   +   +   + .01   +   +   +   +   +   +   +   +   .   .   .   0   0   0   0   0  00000
30 0000   .   +   +   +   +   + .01 .01 .02 .02 .03 .02 .02 .01 .01   +   +   +   +   +   .   .   .   0   0   0   0  00000
31 0000   .   +   +   +   +   +   + .01 .01 .02 .02 .02 .01 .01   +   +   +   +   +   +   .   .   .   0   0   0   0  00000
32 0000   .   .   .   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   .   .   .   .   0   0   0   0   0  00000
33 0000   0   0   0   .   .   .   .   .   .   .   .   .   .   .   .   .   .   .   0   0   0   0   0   0   0   0   0  00000
34 0000   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0  00000
35 0000   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0  00000
36 0000   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0  00000
37 0000   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0  00000
38 0000   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0  00000
39 0000   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0  00000
40 0000   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0  00000
41 0000   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0  00000
42 0000   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0  00000
43 0000   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0  00000
44 00000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000
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SMALL CLOUDS AT 2700.00 SECONDS ELAPSED TIME FOR SAND

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID	LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	2940.	300.0	0.4380	0.0000E+00	237.6	62.56	57.44	0.100000
2	2941.	300.0	0.1731	0.0000E+00	265.5	71.13	48.87	0.100000
3	2941.	300.0	0.1822E-12	0.0000E+00	414.1	118.3	1.711	0.100000

SUMMARY OF SAND DISTRIBUTIONS AFTER 3000.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.34771
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 936.26

SUMMARY OF SAND DISTRIBUTIONS AFTER 3300.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.19255
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 936.42

SUMMARY OF SAND DISTRIBUTIONS AFTER 3600.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.10350
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 936.51

MAX CONC IS 0.00000000 OUTPUT SUPPRESSED AT 60.00 FT

MAX CONC IS 0.00000001 OUTPUT SUPPRESSED AT 119.00 FT

BOTTOM ACCUMULATION OF SAND (CU FT/GRID SQUARE) , 3600.00 SECONDS AFTER DUMP

...MULTIPLY DISPLAYED VALUES BY 1.000 (LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)

M N=	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31
2	0																													
3	0																						0	0	0	0	0	0	0	
4	0	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	0	
5	0	.01	.02	.04	.06	.10	.14	.19	.24	.29	.32	.33	.32	.29	.24	.19	.14	.10	.06	.04	.02	.01	+	+	+	+	+	.	.	0
6	0	.16	.31	.55	.91	1.4	2.0	2.7	3.4	4.0	4.4	4.6	4.4	4.0	3.4	2.7	2.0	1.4	.91	.55	.31	.16	.08	.03	.01	+	+	+	+	0
7	0	.81	1.5	2.6	4.3	6.7	10	13	17	20	22	23	22	20	17	13	10	6.7	4.3	2.6	1.5	.81	.40	.18	.08	.03	.01	+	+	0
8	0	1.3	2.5	4.4	7.2	11	16	22	28	34	39	41	39	34	28	22	16	11	7.2	4.4	2.5	1.3	.67	.31	.13	.05	.02	+	+	0
9	0	.77	1.4	2.5	4.1	6.4	9.3	13	16	19	21	22	21	19	16	13	9.3	6.4	4.1	2.5	1.4	.77	.38	.18	.07	.03	.01	+	+	0
10	0	.15	.29	.51	.84	1.3	1.9	2.6	3.3	4.0	4.6	4.8	4.6	4.0	3.3	2.6	1.9	1.3	.84	.51	.29	.15	.07	.03	.01	+	+	+	+	0
11	0	.01	.02	.04	.07	.14	.25	.45	.89	1.8	3.7	5.0	3.7	1.8	.89	.45	.25	.14	.07	.04	.02	.01	+	+	+	+	+	.	.	0
12	0	+	+	+	+	.01	.02	.05	.08	.12	.15	.16	.15	.12	.08	.05	.02	.01	+	+	+	+	+	+	.	.	.	.	.	0
13	0	+	+	+	+	.01	.02	.05	.12	.29	.59	.77	.59	.29	.12	.05	.02	.01	+	+	+	+	.	.	.	.	.	0	0	0
14	0	+	+	+	+	.01	.02	.07	.19	.57	1.3	1.8	1.3	.57	.19	.07	.02	.01	+	+	+	+	.	.	.	.	0	0	0	0
15	0	.	+	+	+	+	+	+	.01	.01	.02	.02	.02	.01	.01	+	+	+	+	+	+	+	.	.	.	.	0	0	0	0
16	0	.	+	+	+	+	+	.03	.10	.32	.66	.84	.66	.32	.10	.03	+	+	+	+	+	+	.	.	.	.	0	0	0	0
17	0	.	+	+	+	+	+	.01	.05	.15	.29	.36	.29	.15	.05	.01	+	+	+	+	+	+	.	.	.	.	0	0	0	0
18	0	.	.	+	+	+	+	+	+	+	.01	.01	.01	+	+	+	+	+	+	+	+	+	.	.	.	.	0	0	0	0
19	0	.	.	+	+	+	+	.03	.10	.26	.45	.54	.45	.26	.10	.03	+	+	+	+	+	+	.	.	.	.	.	0	0	0
20	0	.	.	+	+	+	+	+	.02	.04	.07	.09	.07	.04	.02	+	+	+	+	+	+	+	.	.	.	.	0	0	0	0
21	0	.	.	.	+	+	+	+	.01	.02	.03	.03	.03	.02	.01	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0
22	0	.	.	+	+	+	.01	.03	.08	.17	.25	.29	.25	.17	.08	.03	.01	+	+	+	+	.	.	.	.	0	0	0	0	0
23	0	.	.	.	+	+	+	+	.01	.02	.02	.03	.02	.02	.01	+	+	+	+	.	.	.	.	0	0	0	0	0	0	0
24	0	.	.	.	+	+	+	+	.02	.03	.04	.05	.04	.03	.02	+	+	+	+	.	.	.	0	0	0	0	0	0	0	0
25	0	.	.	+	+	+	.01	.02	.05	.09	.12	.13	.12	.09	.05	.02	.01	+	+	+	.	.	.	0	0	0	0	0	0	0
26	0	.	.	.	+	+	+	+	+	.01	.01	.01	.01	.01	+	+	+	+	+	.	.	.	0	0	0	0	0	0	0	0
27	0	.	.	+	+	+	+	.01	.02	.03	.04	.04	.04	.03	.02	.01	+	+	+	+	.	.	.	0	0	0	0	0	0	0
28	0	.	+	+	+	+	+	.01	.02	.04	.05	.05	.05	.04	.02	.01	+	+	+	+	+	.	.	0	0	0	0	0	0	0
29	0	.	.	+	+	+	+	+	+	+	+	.01	+	+	+	+	+	+	+	+	+	.	.	.	0	0	0	0	0	0	0
30	0	.	+	+	+	+	+	.01	.01	.02	.02	.03	.02	.02	.01	.01	+	+	+	+	+	.	.	.	0	0	0	0	0	0
31	0	.	+	+	+	+	+	+	.01	.01	.02	.02	.02	.01	.01	+	+	+	+	+	+	.	.	.	0	0	0	0	0	0
32	0	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	0	0	0	0
33	0	.	+	+	+	+	+	+	.01	.01	.01	.01	.01	.01	.01	+	+	+	+	+	+	.	.	.	.	0	0	0	0	0
34	0	.	+	+	+	+	+	+	+	+	.01	.01	.01	+	+	+	+	+	+	+	+	.	.	.	.	0	0	0	0	0
35	0	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	0	0	0	0
36	0	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	0	0	0	0
37	0	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	0	0	0	0
38	0	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	0	0	0
39	0	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	0	0	0
40	0	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	0	0	0	0
41	0	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	0	0	0	0	0	0
42	0	0	0	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0	0	0	0	0	0	0
43	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
44	0																													

SMALL CLOUDS AT 3600.00 SECONDS ELAPSED TIME FOR SAND

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID	LOCATION OF CLOUD CENTROID DISTANCE FROM LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	3781.	300.0	0.8053E-01	0.0000E+00	322.9	70.40	49.60	0.100000
2	3781.	300.0	0.2297E-01	0.0000E+00	353.8	78.97	41.03	0.100000

BOTTOM ACCUMULATION OF SAND (CU FT/GRID SQUARE) , 3600.00 SECONDS AFTER DUMP

...MULTIPLY DISPLAYED VALUES BY 1.000 (LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)

M N=	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31
2	0																													
3	0																						0	0	0	0	0	0	0	
4	0	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	0	
5	0	.01	.02	.04	.06	.10	.14	.19	.24	.29	.32	.33	.32	.29	.24	.19	.14	.10	.06	.04	.02	.01	+	+	+	+	+	.	.	0
6	0	.16	.31	.55	.91	1.4	2.0	2.7	3.4	4.0	4.4	4.6	4.4	4.0	3.4	2.7	2.0	1.4	.91	.55	.31	.16	.08	.03	.01	+	+	+	+	0
7	0	.81	1.5	2.6	4.3	6.7	10	13	17	20	22	23	22	20	17	13	10	6.7	4.3	2.6	1.5	.81	.40	.18	.08	.03	.01	+	+	0
8	0	1.3	2.5	4.4	7.2	11	16	22	28	34	39	41	39	34	28	22	16	11	7.2	4.4	2.5	1.3	.67	.31	.13	.05	.02	+	+	0
9	0	.77	1.4	2.5	4.1	6.4	9.3	13	16	19	21	22	21	19	16	13	9.3	6.4	4.1	2.5	1.4	.77	.38	.18	.07	.03	.01	+	+	0
10	0	.15	.29	.51	.84	1.3	1.9	2.6	3.3	4.0	4.6	4.8	4.6	4.0	3.3	2.6	1.9	1.3	.84	.51	.29	.15	.07	.03	.01	+	+	+	+	0
11	0	.01	.02	.04	.07	.14	.25	.45	.89	1.8	3.7	5.0	3.7	1.8	.89	.45	.25	.14	.07	.04	.02	.01	+	+	+	+	+	.	.	0
12	0	+	+	+	+	.01	.02	.05	.08	.12	.15	.16	.15	.12	.08	.05	.02	.01	+	+	+	+	+	+	.	.	.	.	.	0
13	0	+	+	+	+	.01	.02	.05	.12	.29	.59	.77	.59	.29	.12	.05	.02	.01	+	+	+	+	.	.	.	.	.	0	0	0
14	0	+	+	+	+	.01	.02	.07	.19	.57	1.3	1.8	1.3	.57	.19	.07	.02	.01	+	+	+	+	.	.	.	.	0	0	0	0
15	0	.	+	+	+	+	+	+	.01	.01	.02	.02	.02	.01	.01	+	+	+	+	+	+	+	.	.	.	.	0	0	0	0
16	0	.	+	+	+	+	+	.03	.10	.32	.66	.84	.66	.32	.10	.03	+	+	+	+	+	+	.	.	.	.	0	0	0	0
17	0	.	+	+	+	+	+	.01	.05	.15	.29	.36	.29	.15	.05	.01	+	+	+	+	+	+	.	.	.	.	0	0	0	0
18	0	.	.	+	+	+	+	+	+	+	.01	.01	.01	+	+	+	+	+	+	+	+	+	.	.	.	.	0	0	0	0
19	0	.	.	+	+	+	+	.03	.10	.26	.45	.54	.45	.26	.10	.03	+	+	+	+	+	+	.	.	.	.	.	0	0	0
20	0	.	.	+	+	+	+	+	.02	.04	.07	.09	.07	.04	.02	+	+	+	+	+	+	+	.	.	.	.	0	0	0	0
21	0	.	.	.	+	+	+	+	.01	.02	.03	.03	.03	.02	.01	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0
22	0	.	.	+	+	+	.01	.03	.08	.17	.25	.29	.25	.17	.08	.03	.01	+	+	+	+	.	.	.	.	0	0	0	0	0
23	0	.	.	.	+	+	+	+	.01	.02	.02	.03	.02	.02	.01	+	+	+	+	.	.	.	.	0	0	0	0	0	0	0
24	0	.	.	.	+	+	+	+	.02	.03	.04	.05	.04	.03	.02	+	+	+	+	.	.	.	0	0	0	0	0	0	0	0
25	0	.	.	+	+	+	.01	.02	.05	.09	.12	.13	.12	.09	.05	.02	.01	+	+	+	.	.	.	0	0	0	0	0	0	0
26	0	.	.	.	+	+	+	+	+	.01	.01	.01	.01	.01	+	+	+	+	+	.	.	.	0	0	0	0	0	0	0	0
27	0	.	.	+	+	+	+	.01	.02	.03	.04	.04	.04	.03	.02	.01	+	+	+	+	.	.	.	0	0	0	0	0	0	0
28	0	.	+	+	+	+	+	.01	.02	.04	.05	.05	.05	.04	.02	.01	+	+	+	+	+	.	.	0	0	0	0	0	0	0
29	0	.	.	+	+	+	+	+	+	+	+	.01	+	+	+	+	+	+	+	+	+	.	.	.	0	0	0	0	0	0	0
30	0	.	+	+	+	+	+	.01	.01	.02	.02	.03	.02	.02	.01	.01	+	+	+	+	+	.	.	.	0	0	0	0	0	0
31	0	.	+	+	+	+	+	+	.01	.01	.02	.02	.02	.01	.01	+	+	+	+	+	+	.	.	.	0	0	0	0	0	0
32	0	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	0	0	0	0
33	0	.	+	+	+	+	+	+	.01	.01	.01	.01	.01	.01	.01	+	+	+	+	+	+	.	.	.	.	0	0	0	0	0
34	0	.	+	+	+	+	+	+	+	+	.01	.01	.01	+	+	+	+	+	+	+	+	.	.	.	.	0	0	0	0	0
35	0	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	0	0	0	0
36	0	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	0	0	0	0
37	0	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	0	0	0	0
38	0	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	0	0	0
39	0	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	0	0	0
40	0	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	0	0	0	0
41	0	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	0	0	0	0	0	0
42	0	0	0	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0	0	0	0	0	0	0
43	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
44	0																													

THICKNESS (FT) OF SAND ACCUMULATED ON BOTTOM, 3600.00 SECONDS AFTER DUMP

...MULTIPLY DISPLAYED VALUES BY 0.1000E-01 (LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)

M N=	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31
2	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O
3	O	0	0	0	0	.	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0
4	O	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0	0
5	O	+	+	+	+	+	+	.01	.01	.01	.02	.02	.02	.01	.01	.01	+	+	+	+	+	+	+	+	.	.	.	.	.	0
6	O	.01	.02	.03	.05	.09	.12	.17	.22	.26	.28	.29	.28	.26	.22	.17	.12	.09	.05	.03	.02	.01	+	+	+	+	+	.	.	0
7	O	.05	.09	.17	.28	.43	.62	.84	1.0	1.2	1.3	1.4	1.3	1.2	1.0	.84	.62	.43	.28	.17	.09	.05	.02	.01	+	+	+	+	+	0
8	O	.08	.16	.28	.46	.71	1.0	1.4	1.8	2.1	2.4	2.6	2.4	2.1	1.8	1.4	1.0	.71	.46	.28	.16	.08	.04	.02	+	+	+	+	+	0
9	O	.04	.09	.16	.26	.41	.59	.80	1.0	1.2	1.3	1.3	1.3	1.2	1.0	.80	.59	.41	.26	.16	.09	.04	.02	.01	+	+	+	+	.	0
10	O	+	.01	.03	.05	.08	.12	.16	.21	.26	.29	.31	.29	.26	.21	.16	.12	.08	.05	.03	.01	+	+	+	+	+	+	.	.	0
11	O	+	+	+	+	+	.01	.02	.05	.12	.24	.32	.24	.12	.05	.02	.01	+	+	+	+	+	+	+	.	.	.	.	.	0
12	O	.	+	+	+	+	+	+	+	+	+	.01	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	0	0	0
13	O	.	.	+	+	+	+	+	+	.01	.03	.04	.03	.01	+	+	+	+	+	+	.	.	.	.	0	0	0	0	0	0
14	O	.	.	+	+	+	+	+	.01	.03	.08	.11	.08	.03	.01	+	+	+	+	+	.	.	.	0	0	0	0	0	0	0
15	O	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0
16	O	.	.	.	+	+	+	+	+	.02	.04	.05	.04	.02	+	+	+	+	+	.	.	.	.	0	0	0	0	0	0	0
17	O	.	.	.	.	+	+	+	+	+	.01	.02	.01	+	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0
18	O	.	.	.	.	.	.	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0	0	0	0	0
19	O	.	.	.	.	+	+	+	+	.01	.02	.03	.02	.01	+	+	+	+	.	.	.	.	0	0	0	0	0	0	0	0
20	O	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	0	0	0	0	0	0	0	0
21	O	0	.	.	.	.	.	+	+	+	+	+	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0	0	0
22	O	0	.	.	.	+	+	+	+	.01	.01	.01	.01	.01	+	+	+	+	.	.	.	0	0	0	0	0	0	0	0	0
23	O	0	0	.	.	.	.	+	+	+	+	+	+	+	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0
24	O	0	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0
25	O	0	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	0	0	0	0	0	0	0	0	0
26	O	0	0	.	.	.	.	+	+	+	+	+	+	+	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0
27	O	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	0	0	0	0	0	0	0	0
28	O	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	0	0	0	0	0	0	0	0
29	O	0	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	0	0	0	0	0	0	0	0	0
30	O	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	0	0	0	0	0	0	0	0
31	O	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	0	0	0	0	0	0	0	0
32	O	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	0	0	0	0	0	0	0	0
33	O	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0
34	O	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0
35	O	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0
36	O	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0	0	0
37	O	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0
38	O	.	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0	0	0
39	O	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0	0	0
40	O	.	.	.	.	.	.	.	.	+	+	+	+	+	.	.	.	.	.	.	.	.	.	0	0	0	0	0	0	0
41	O	0	0	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0	0	0	0	0	0	0
42	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
43	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
44	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O

BEGIN LONG TERM SIMULATION OF FATE OF SILT

SUMMARY OF SILT DISTRIBUTIONS AFTER 300.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 3956.8
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 1646.6

SUMMARY OF SILT DISTRIBUTIONS AFTER 600.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 2134.6
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 3462.9

SUMMARY OF SILT DISTRIBUTIONS AFTER 900.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 658.99
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 4931.0

CONCENTRATIONS ABOVE BACKGROUND OF SILT (MG/L) IN THE CLOUD 900.00 SECONDS AFTER DUMP

60.00 FT BELOW THE WATER SURFACE

...MULTIPLY DISPLAYED VALUES BY 1.000 (LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)

M N=	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31
2	000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000																													
3	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		00000
4	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		00000
5	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		00000
6	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		00000
7	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		00000
8	0000	0	0	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0	0	0	0	0		00000
9	0000	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	0	0	0	0	0	0		00000
10	0000	+	+	+	+	+	+	.01	.01	.01	.01	.02	.01	.01	.01	.01	+	+	+	+	+	+	0	0	0	0	0	0		00000
11	0000	.01	.03	.05	.08	.13	.18	.24	.30	.36	.39	.41	.39	.36	.30	.24	.18	.13	.08	.05	.03	.01	0	0	0	0	0	0		00000
12	0000	.14	.26	.45	.73	1.1	1.6	2.2	2.8	3.3	3.7	3.8	3.7	3.3	2.8	2.2	1.6	1.1	.73	.45	.26	.14	0	0	0	0	0	0		00000
13	0000	.43	.81	1.4	2.3	3.7	5.5	8.5	17	46	107	145	107	46	17	8.5	5.5	3.7	2.3	1.4	.81	.43	0	0	0	0	0	0		00000
14	0000	.48	.89	1.5	2.6	4.1	6.3	11	29	103	265	371	265	103	29	11	6.3	4.1	2.6	1.5	.89	.48	0	0	0	0	0	0		00000
15	0000	.19	.34	.60	.98	1.5	2.2	3.0	3.8	4.6	5.1	5.3	5.1	4.6	3.8	3.0	2.2	1.5	.98	.60	.34	.19	0	0	0	0	0	0		00000
16	0000	.02	.05	.08	.13	.20	.29	.39	.49	.58	.64	.66	.64	.58	.49	.39	.29	.20	.13	.08	.05	.02	0	0	0	0	0	0		00000
17	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		00000
18	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		00000
19	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		00000
20	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		00000
21	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		00000
22	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		00000
23	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		00000
24	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		00000
25	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		00000
26	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		00000
27	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		00000
28	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		00000
29	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		00000
30	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		00000
31	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		00000
32	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		00000
33	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		00000
34	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		00000
35	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		00000
36	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		00000
37	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		00000
38	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		00000
39	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		00000
40	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		00000
41	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		00000
42	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		00000
43	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		00000
44	000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000																													

CONCENTRATIONS ABOVE BACKGROUND OF SILT (MG/L) IN THE CLOUD 900.00 SECONDS AFTER DUMP

119.00 FT BELOW THE WATER SURFACE

...MULTIPLY DISPLAYED VALUES BY 1.000 (LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)

M N=	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
4	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
5	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
6	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
7	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
8	0000	0	0	0	.	.	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	00000
9	0000	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	0	0	0	0	0	0	0	0	00000
10	0000	+	+	+	+	+	+	.01	.01	.01	.01	.01	.01	.01	.01	.01	+	+	+	+	+	+	0	0	0	0	0	0	0	00000
11	0000	.01	.03	.05	.08	.12	.18	.25	.32	.38	.43	.44	.43	.38	.32	.25	.18	.12	.08	.05	.03	.01	0	0	0	0	0	0	0	00000
12	0000	.14	.27	.50	.89	1.5	2.4	3.7	5.3	6.9	8.1	8.6	8.1	6.9	5.3	3.7	2.4	1.5	.89	.50	.27	.14	0	0	0	0	0	0	0	00000
13	0000	.48	1.0	2.0	4.1	8.1	15	28	49	80	114	131	114	80	49	28	15	8.1	4.1	2.0	1.0	.48	0	0	0	0	0	0	0	00000
14	0000	.53	1.1	2.3	4.8	10	19	35	65	114	175	207	175	114	65	35	19	10	4.8	2.3	1.1	.53	0	0	0	0	0	0	0	00000
15	0000	.19	.37	.70	1.2	2.2	3.7	5.9	8.6	11	14	15	14	11	8.6	5.9	3.7	2.2	1.2	.70	.37	.19	0	0	0	0	0	0	0	00000
16	0000	.02	.04	.08	.13	.21	.31	.42	.55	.67	.75	.78	.75	.67	.55	.42	.31	.21	.13	.08	.04	.02	0	0	0	0	0	0	0	00000
17	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
18	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
19	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
20	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
21	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
22	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
23	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
24	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
25	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
26	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
27	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
28	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
29	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
30	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
31	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
32	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
33	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
34	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
35	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
36	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
37	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
38	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
39	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
40	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
41	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
42	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
43	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
44	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0

```
BOTTOM ACCUMULATION OF SILT     (CU FT/GRID SQUARE) ,    900.00 SECONDS AFTER DUMP
...MULTIPLY DISPLAYED VALUES BY   1.000          (LEGEND... + = .LT. .01   . = .LT. .0001   0 = .LT. .000001)
M N=  2   3   4   5   6   7   8   9  10  11  12  13  14  15  16  17  18  19  20  21  22  23  24  25  26  27  28  29  30  31
 2 00000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000
 3 0000   .   .   .   .   .   .   .   +   +   +   +   +   +   +   .   .   .   .   .   .   .   .   .   0   0   0   0   00000
 4 0000   +   +   +   +   +   +   + .01 .01 .01 .01 .01 .01 .01   +   +   +   +   +   +   +   +   +   .   .   .   .   .0000
 5 0000 .02 .04 .07 .12 .19 .28 .37 .47 .56 .61 .63 .61 .56 .47 .37 .28 .19 .12 .07 .04 .02 .01   +   +   +   +   +   .0000
 6 0000 .32 .60 1.0 1.7 2.6 3.8 5.1 6.5 7.6 8.5 8.7 8.5 7.6 6.5 5.1 3.8 2.6 1.7 1.0 .60 .32 .16 .07 .03 .01   +   +   +0000
 7 0000 1.5 2.8 5.0 8.3  13  18  25  31  37  41  42  41  37  31  25  18  13 8.3 5.0 2.8 1.5 .77 .36 .15 .06 .02   +   +0000
 8 0000 2.6 4.9 8.7  14  22  31  42  53  63  69  72  69  63  53  42  31  22  14 8.7 4.9 2.6 1.3 .63 .28 .11 .04 .01   +0000
 9 0000 2.4 4.4 7.4  12  18  25  34  42  49  54  56  54  49  42  34  25  18  12 7.4 4.4 2.4 1.2 .63 .29 .12 .05 .02   +0000
10 0000 3.3 5.7 9.3  14  21  28  37  45  51  56  58  56  51  45  37  28  21  14 9.3 5.7 3.3 1.8 .98 .48 .22 .10 .04 .010000
11 0000 4.2 7.2  12  17  25  34  43  53  60  66  68  66  60  53  43  34  25  17  12 7.2 4.2 2.4 1.2 .64 .30 .13 .05 .020000
12 0000 3.7 6.0 9.4  14  20  26  33  40  46  49  51  49  46  40  33  26  20  14 9.4 6.0 3.7 2.1 1.1 .62 .31 .14 .06 .020000
13 0000 4.1 6.5  10  14  19  25  32  37  42  45  47  45  42  37  32  25  19  14  10 6.5 4.1 2.5 1.4 .79 .41 .20 .09 .040000
14 0000 3.9 6.2 9.3  13  18  23  29  34  39  41  42  41  39  34  29  23  18  13 9.3 6.2 3.9 2.4 1.4 .77 .41 .20 .09 .040000
15 0000 1.9 3.0 4.6 6.5 8.9  12  14  17  19  20  21  20  19  17  14  12 8.9 6.5 4.6 3.0 1.9 1.2 .69 .38 .20 .10 .04 .020000
16 0000 .46 .72 1.0 1.5 2.0 2.7 3.3 3.9 4.4 4.7 4.9 4.7 4.4 3.9 3.3 2.7 2.0 1.5 1.0 .72 .46 .28 .16 .09 .04 .02 .01   +0000
17 0000 .05 .08 .11 .17 .23 .30 .37 .43 .49 .52 .54 .52 .49 .43 .37 .30 .23 .17 .11 .08 .05 .03 .01 .01   +   +   +   +0000
18 0000   +   +   +   + .01 .01 .01 .02 .02 .02 .02 .02 .02 .02 .01 .01 .01   +   +   +   +   +   +   +   +   +   .   .0000
19 0000   .   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   .   .   .   .   .   .   .   00000
20 0000   0   .   .   .   .   .   .   .   .   .   .   .   .   .   .   .   .   .   .   .   0   0   0   0   0   0   0   00000
21 0000   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   00000
22 0000   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   00000
23 0000   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   00000
24 0000   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   00000
25 0000   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   00000
26 0000   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   00000
27 0000   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   00000
28 0000   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   00000
29 0000   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   00000
30 0000   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   00000
31 0000   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   00000
32 0000   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   00000
33 0000   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   00000
34 0000   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   00000
35 0000   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   00000
36 0000   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   00000
37 0000   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   00000
38 0000   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   00000
39 0000   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   00000
40 0000   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   00000
41 0000   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   00000
42 0000   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   00000
43 0000   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   00000
44 00000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000
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SMALL CLOUDS AT 900.00 SECONDS ELAPSED TIME FOR SILT

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID	LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	1259.	300.0	72.89	0.0000E+00	96.85	5.811	113.8	0.447041E-03
2	1259.	300.0	64.20	0.0000E+00	117.6	21.63	98.37	0.230289E-03
3	1259.	300.0	88.59	0.0000E+00	155.1	76.40	43.60	0.357112E-03
4	1259.	300.0	112.0	0.0000E+00	235.3	80.18	39.82	0.248273E-03
5	1259.	300.0	48.58	0.0000E+00	296.0	63.08	56.92	0.560902E-04
6	1259.	300.0	22.72	0.0000E+00	333.5	58.92	61.08	0.340000E-04
7	1259.	300.0	13.17	0.0000E+00	358.6	57.66	62.34	0.340000E-04
8	1259.	300.0	9.241	0.0000E+00	377.8	57.44	62.56	0.340000E-04
9	1259.	300.0	7.246	0.0000E+00	393.8	57.38	62.62	0.340000E-04
10	1258.	300.0	220.4	0.0000E+00	407.8	119.6	0.3997	0.690000E-02

SUMMARY OF SILT DISTRIBUTIONS AFTER 1200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 438.32
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 5150.1

SUMMARY OF SILT DISTRIBUTIONS AFTER 1500.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 438.19
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 5150.2

SUMMARY OF SILT DISTRIBUTIONS AFTER 1800.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 438.12
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 5150.3

CONCENTRATIONS ABOVE BACKGROUND OF SILT (MG/L) IN THE CLOUD 1800.00 SECONDS AFTER DUMP

60.00 FT BELOW THE WATER SURFACE

...MULTIPLY DISPLAYED VALUES BY 1.000 (LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)

M N=	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	0	0	0	0	0
17	+	+	+	+	+	+	+	+	+	.01	.01	.01	.01	.01	+	+	+	+	+	+	+	+	+	+	+	0	0	0	0	0
18	.02	.03	.04	.06	.08	.10	.12	.14	.15	.16	.17	.16	.15	.14	.12	.10	.08	.06	.04	.03	.02	.01	.01	0	0	0	0	0	0	0
19	.22	.32	.46	.65	.86	1.1	1.3	1.6	1.8	1.9	2.0	1.9	1.8	1.6	1.3	1.1	.86	.65	.46	.32	.22	.14	.09	0	0	0	0	0	0	0
20	1.2	1.9	2.9	4.3	6.1	8.4	11	13	16	17	18	17	16	13	11	8.4	6.1	4.3	2.9	1.9	1.2	.77	.46	0	0	0	0	0	0	0
21	4.0	6.7	11	17	27	41	61	88	118	143	153	143	118	88	61	41	27	17	11	6.7	4.0	2.3	1.3	0	0	0	0	0	0	0
22	6.1	11	18	30	51	88	152	257	396	527	581	527	396	257	152	88	51	30	18	11	6.1	3.5	2.0	0	0	0	0	0	0	0
23	4.0	6.7	11	17	27	41	61	88	118	142	152	142	118	88	61	41	27	17	11	6.7	4.0	2.3	1.3	0	0	0	0	0	0	0
24	1.2	1.9	2.9	4.3	6.2	8.4	11	14	16	17	18	17	16	14	11	8.4	6.2	4.3	2.9	1.9	1.2	.77	.46	0	0	0	0	0	0	0
25	.22	.32	.46	.64	.86	1.1	1.3	1.6	1.8	1.9	2.0	1.9	1.8	1.6	1.3	1.1	.86	.64	.46	.32	.22	.14	.09	0	0	0	0	0	0	0
26	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
27	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
28	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
29	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
30	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
31	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
32	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
33	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
34	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
35	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
36	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
37	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
38	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
39	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
40	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
41	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
42	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
43	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
44	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0

CONCENTRATIONS ABOVE BACKGROUND OF SILT (MG/L) IN THE CLOUD 1800.00 SECONDS AFTER DUMP

119.00 FT BELOW THE WATER SURFACE

...MULTIPLY DISPLAYED VALUES BY 1.000 (LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)

M N=	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31
2	00000000000000000000000000000000000000000000000000000000000000000000000000																													
3	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
4	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
5	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
6	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
7	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
8	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
9	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
10	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
11	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
12	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
13	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
14	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
15	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
16	0000	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0	00000	
17	0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	0	0	0	0	00000	
18	0000	+	+	+	+	.01	.01	.01	.02	.02	.02	.02	.02	.02	.02	.01	.01	.01	+	+	+	+	+	+	0	0	0	0	00000	
19	0000	.03	.04	.06	.09	.12	.16	.19	.23	.26	.28	.29	.28	.26	.23	.19	.16	.12	.09	.06	.04	.03	.02	.01	0	0	0	0	00000	
20	0000	.18	.28	.43	.63	.90	1.2	1.6	1.9	2.3	2.5	2.6	2.5	2.3	1.9	1.6	1.2	.90	.63	.43	.28	.18	.11	.06	0	0	0	0	00000	
21	0000	.58	.98	1.6	2.5	4.0	6.1	9.1	13	18	21	23	21	18	13	9.1	6.1	4.0	2.5	1.6	.98	.58	.34	.19	0	0	0	0	00000	
22	0000	.90	1.5	2.6	4.4	7.6	13	23	39	59	78	87	78	59	39	23	13	7.6	4.4	2.6	1.5	.90	.51	.29	0	0	0	0	00000	
23	0000	.59	.98	1.6	2.5	4.0	6.1	9.2	13	18	21	23	21	18	13	9.2	6.1	4.0	2.5	1.6	.98	.59	.34	.19	0	0	0	0	00000	
24	0000	.18	.28	.43	.63	.90	1.2	1.6	1.9	2.3	2.5	2.6	2.5	2.3	1.9	1.6	1.2	.90	.63	.43	.28	.18	.11	.06	0	0	0	0	00000	
25	0000	.03	.04	.06	.09	.12	.16	.19	.23	.26	.28	.29	.28	.26	.23	.19	.16	.12	.09	.06	.04	.03	.02	.01	0	0	0	0	00000	
26	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
27	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
28	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
29	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
30	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
31	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
32	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
33	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
34	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
35	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
36	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
37	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
38	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
39	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
40	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
41	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
42	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
43	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
44	00000000000000000000000000000000000000000000000000000000000000000000000000																													

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BOTTOM ACCUMULATION OF SILT     (CU FT/GRID SQUARE) ,   1800.00 SECONDS AFTER DUMP
...MULTIPLY DISPLAYED VALUES BY   1.000         (LEGEND... + = .LT. .01   . = .LT. .0001   0 = .LT. .000001)
M N=  2   3   4   5   6   7   8   9  10  11  12  13  14  15  16  17  18  19  20  21  22  23  24  25  26  27  28  29  30  31
 2 000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000
 3 0000   .   .   .   .   .   .   .   +   +   +   +   +   +   +   .   .   .   .   .   .   .   .   .   0   0   0   0   00000
 4 0000   +   +   +   +   +   +   + .01 .01 .01 .01 .01 .01 .01   +   +   +   +   +   +   +   +   +   .   .   .   .   .0000
 5 0000 .02 .04 .07 .12 .19 .28 .37 .47 .56 .61 .63 .61 .56 .47 .37 .28 .19 .12 .07 .04 .02 .01   +   +   +   +   +   .0000
 6 0000 .32 .60 1.0 1.7 2.6 3.8 5.1 6.5 7.6 8.5 8.7 8.5 7.6 6.5 5.1 3.8 2.6 1.7 1.0 .60 .32 .16 .07 .03 .01   +   +   +0000
 7 0000 1.5 2.8 5.0 8.3  13  18  25  31  37  41  42  41  37  31  25  18  13 8.3 5.0 2.8 1.5 .77 .36 .15 .06 .02   +   +0000
 8 0000 2.6 4.9 8.7  14  22  31  42  53  63  69  72  69  63  53  42  31  22  14 8.7 4.9 2.6 1.3 .63 .28 .11 .04 .01   +0000
 9 0000 2.4 4.4 7.4  12  18  25  34  42  49  54  56  54  49  42  34  25  18  12 7.4 4.4 2.4 1.2 .63 .29 .12 .05 .02   +0000
10 0000 3.3 5.7 9.3  14  21  28  37  45  51  56  58  56  51  45  37  28  21  14 9.3 5.7 3.3 1.8 .98 .48 .22 .10 .04 .010000
11 0000 4.2 7.2  12  17  25  34  43  53  60  66  68  66  60  53  43  34  25  17  12 7.2 4.2 2.4 1.2 .64 .30 .13 .06 .020000
12 0000 3.7 6.0 9.4  14  20  26  33  40  46  49  51  49  46  40  33  26  20  14 9.4 6.0 3.7 2.1 1.1 .62 .31 .14 .06 .020000
13 0000 4.1 6.5  10  14  20  25  32  37  42  46  47  46  42  37  32  25  20  14  10 6.5 4.1 2.5 1.4 .79 .41 .20 .09 .040000
14 0000 4.1 6.4  10  14  19  24  30  35  39  42  43  42  39  35  30  24  19  14  10 6.4 4.1 2.5 1.4 .80 .42 .21 .10 .040000
15 0000 2.3 3.6 5.4 7.7  10  13  17  19  22  23  24  23  22  19  17  13  10 7.7 5.4 3.6 2.3 1.4 .86 .48 .26 .13 .06 .030000
16 0000 1.1 1.7 2.5 3.5 4.7 6.0 7.3 8.5  10  10  10  10  10 8.5 7.3 6.0 4.7 3.5 2.5 1.7 1.1 .75 .46 .26 .15 .08 .04 .020000
17 0000 .72 1.0 1.5 2.0 2.6 3.3 4.0 4.6 5.1 5.5 5.6 5.5 5.1 4.6 4.0 3.3 2.6 2.0 1.5 1.0 .72 .47 .29 .17 .10 .05 .02 .010000
18 0000 .32 .48 .68 .92 1.2 1.5 1.8 2.0 2.3 2.4 2.4 2.4 2.3 2.0 1.8 1.5 1.2 .92 .68 .48 .32 .21 .13 .08 .04 .02 .01   +0000
19 0000 .08 .12 .17 .23 .30 .38 .45 .52 .58 .62 .64 .62 .58 .52 .45 .38 .30 .23 .17 .12 .08 .05 .03 .02 .01   +   +   +0000
20 0000 .01 .01 .02 .03 .04 .05 .06 .07 .08 .08 .08 .08 .08 .07 .06 .05 .04 .03 .02 .01 .01   +   +   +   +   +   +   +0000
21 0000   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   .   .   .0000
22 0000   .   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   .   .   .   .   .   .   .   .0000
23 0000   .   .   .   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   .   .   .   .   .   .   .   .   0   00000
24 0000   .   .   .   .   .   .   .   +   +   +   +   +   +   +   .   .   .   .   .   .   .   .   .   .   0   0   0   00000
25 0000   .   .   .   .   .   .   .   .   .   .   .   .   .   .   .   .   .   .   .   .   .   0   0   0   0   0   0   00000
26 0000   0   0   0   0   0   0   0   0   0   .   .   .   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   00000
27 0000   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   00000
28 0000   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   00000
29 0000   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   00000
30 0000   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   00000
31 0000   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   00000
32 0000   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   00000
33 0000   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   00000
34 0000   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   00000
35 0000   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   00000
36 0000   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   00000
37 0000   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   00000
38 0000   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   00000
39 0000   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   00000
40 0000   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   00000
41 0000   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   00000
42 0000   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   00000
43 0000   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   00000
44 000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000
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SMALL CLOUDS AT 1800.00 SECONDS ELAPSED TIME FOR SILT

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID	LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	2100.	300.0	72.82	0.0000E+00	161.8	0.0000E+00	120.0	0.808215E-04
2	2100.	300.0	64.16	0.0000E+00	186.4	0.0000E+00	120.0	0.550344E-04
3	2100.	300.0	88.39	0.0000E+00	229.9	20.90	99.10	0.724927E-04
4	2100.	300.0	111.8	0.0000E+00	320.4	12.69	107.3	0.462476E-04
5	2100.	300.0	48.56	0.0000E+00	387.4	0.0000E+00	120.0	0.340000E-04
6	2100.	300.0	22.71	0.0000E+00	428.4	0.0000E+00	120.0	0.340000E-04
7	2100.	300.0	13.17	0.0000E+00	455.6	0.0000E+00	120.0	0.340000E-04
8	2100.	300.0	9.238	0.0000E+00	476.4	0.0000E+00	120.0	0.340000E-04
9	2099.	300.0	7.244	0.0000E+00	493.8	0.0000E+00	120.0	0.340000E-04

SUMMARY OF SILT DISTRIBUTIONS AFTER 2100.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 438.07
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 5150.4

SUMMARY OF SILT DISTRIBUTIONS AFTER 2400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 438.03
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 5150.4

SUMMARY OF SILT DISTRIBUTIONS AFTER 2700.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 437.99
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 5150.4

CONCENTRATIONS ABOVE BACKGROUND OF SILT (MG/L) IN THE CLOUD 2700.00 SECONDS AFTER DUMP

60.00 FT BELOW THE WATER SURFACE

...MULTIPLY DISPLAYED VALUES BY 1.000 (LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)

M N=	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31
2	OOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOO																													
3	OOOO	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		OOOOO
4	OOOO	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		OOOOO
5	OOOO	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		OOOOO
6	OOOO	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		OOOOO
7	OOOO	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		OOOOO
8	OOOO	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		OOOOO
9	OOOO	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		OOOOO
10	OOOO	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		OOOOO
11	OOOO	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		OOOOO
12	OOOO	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		OOOOO
13	OOOO	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		OOOOO
14	OOOO	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		OOOOO
15	OOOO	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		OOOOO
16	OOOO	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		OOOOO
17	OOOO	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		OOOOO
18	OOOO	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		OOOOO
19	OOOO	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		OOOOO
20	OOOO	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		OOOOO
21	OOOO	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		OOOOO
22	OOOO	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		OOOOO
23	OOOO	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		OOOOO
24	OOOO	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	0	0		OOOOO
25	OOOO	.01	.01	.01	.02	.02	.03	.03	.03	.03	.04	.04	.04	.03	.03	.03	.03	.02	.02	.01	.01	.01	+	+	+	+	0	0		OOOOO
26	OOOO	.08	.11	.14	.17	.21	.25	.28	.31	.33	.35	.35	.35	.33	.31	.28	.25	.21	.17	.14	.11	.08	.06	.04	.03	.02	0	0		OOOOO
27	OOOO	.51	.68	.88	1.1	1.3	1.6	1.9	2.1	2.3	2.4	2.4	2.4	2.3	2.1	1.9	1.6	1.3	1.1	.88	.68	.51	.37	.27	.19	.13	0	0		OOOOO
28	OOOO	2.2	3.0	4.1	5.3	6.8	8.5	10	12	13	14	14	14	13	12	10	8.5	6.8	5.3	4.1	3.0	2.2	1.5	1.0	.74	.49	0	0		OOOOO
29	OOOO	6.4	9.4	13	19	26	35	46	57	68	75	78	75	68	57	46	35	26	19	13	9.4	6.4	4.4	2.9	1.9	1.2	0	0		OOOOO
30	OOOO	12	18	27	41	61	90	128	171	213	245	257	245	213	171	128	90	61	41	27	18	12	7.5	4.9	3.1	2.0	0	0		OOOOO
31	OOOO	11	16	25	37	55	81	113	151	187	213	223	213	187	151	113	81	55	37	25	16	11	7.1	4.6	3.0	1.9	0	0		OOOOO
32	OOOO	5.5	7.9	11	15	21	28	35	43	50	55	57	55	50	43	35	28	21	15	11	7.9	5.5	3.7	2.5	1.6	1.0	0	0		OOOOO
33	OOOO	1.7	2.3	3.1	4.1	5.2	6.4	7.6	8.7	10	10	10	10	10	8.7	7.6	6.4	5.2	4.1	3.1	2.3	1.7	1.2	.86	.59	.39	0	0		OOOOO
34	OOOO	.38	.50	.64	.81	.99	1.1	1.3	1.5	1.6	1.7	1.7	1.7	1.6	1.5	1.3	1.1	.99	.81	.64	.50	.38	.28	.20	.14	.09	0	0		OOOOO
35	OOOO	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		OOOOO
36	OOOO	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		OOOOO
37	OOOO	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		OOOOO
38	OOOO	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		OOOOO
39	OOOO	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		OOOOO
40	OOOO	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		OOOOO
41	OOOO	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		OOOOO
42	OOOO	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		OOOOO
43	OOOO	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		OOOOO
44	OOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOO																													

CONCENTRATIONS ABOVE BACKGROUND OF SILT (MG/L) IN THE CLOUD 2700.00 SECONDS AFTER DUMP

119.00 FT BELOW THE WATER SURFACE

...MULTIPLY DISPLAYED VALUES BY 1.000 (LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)

M N=	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31
2	000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000																													
3	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
4	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
5	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
6	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
7	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
8	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
9	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
10	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
11	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
12	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
13	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
14	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
15	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
16	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
17	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
18	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
19	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
20	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
21	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
22	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
23	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
24	0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	0	0	00000	
25	0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	0	0	00000	
26	0000	.01	.01	.02	.02	.03	.03	.04	.04	.04	.05	.05	.05	.04	.04	.04	.03	.03	.02	.02	.01	.01	+	+	+	+	0	0	00000	
27	0000	.07	.09	.12	.16	.19	.23	.27	.30	.33	.35	.35	.35	.33	.30	.27	.23	.19	.16	.12	.09	.07	.05	.03	.02	.01	0	0	00000	
28	0000	.31	.44	.59	.77	.99	1.2	1.4	1.7	1.8	2.0	2.0	2.0	1.8	1.7	1.4	1.2	.99	.77	.59	.44	.31	.22	.15	.10	.07	0	0	00000	
29	0000	.93	1.3	1.9	2.7	3.7	5.0	6.6	8.2	10	11	11	11	10	8.2	6.6	5.0	3.7	2.7	1.9	1.3	.93	.63	.42	.28	.18	0	0	00000	
30	0000	1.6	2.5	3.8	5.8	8.8	13	18	25	31	35	37	35	31	25	18	13	8.8	5.8	3.8	2.5	1.6	1.0	.71	.45	.29	0	0	00000	
31	0000	1.5	2.3	3.5	5.3	8.0	12	16	22	27	31	32	31	27	22	16	12	8.0	5.3	3.5	2.3	1.5	1.0	.67	.43	.27	0	0	00000	
32	0000	.79	1.1	1.6	2.2	3.0	3.9	5.0	6.2	7.2	8.0	8.2	8.0	7.2	6.2	5.0	3.9	3.0	2.2	1.6	1.1	.79	.54	.36	.24	.15	0	0	00000	
33	0000	.25	.34	.45	.59	.75	.92	1.1	1.2	1.3	1.4	1.5	1.4	1.3	1.2	1.1	.92	.75	.59	.45	.34	.25	.17	.12	.08	.05	0	0	00000	
34	0000	.05	.07	.09	.11	.14	.17	.19	.22	.23	.25	.25	.25	.23	.22	.19	.17	.14	.11	.09	.07	.05	.04	.02	.02	.01	0	0	00000	
35	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
36	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
37	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
38	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
39	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
40	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
41	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
42	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
43	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
44	000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000																													

BOTTOM ACCUMULATION OF SILT (CU FT/GRID SQUARE) , 2700.00 SECONDS AFTER DUMP

...MULTIPLY DISPLAYED VALUES BY 1.000 (LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)

M N=	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	.	.	.	.	.	.	.	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	0	0	0	0	0	0
4	0	+	+	+	+	+	+	+	.01	.01	.01	.01	.01	.01	.01	+	+	+	+	+	+	+	+	+	.	.	.	.	.	0
5	0	.02	.04	.07	.12	.19	.28	.37	.47	.56	.61	.63	.61	.56	.47	.37	.28	.19	.12	.07	.04	.02	.01	+	+	+	+	+	.	0
6	0	.32	.60	1.0	1.7	2.6	3.8	5.1	6.5	7.6	8.5	8.7	8.5	7.6	6.5	5.1	3.8	2.6	1.7	1.0	.60	.32	.16	.07	.03	.01	+	+	+	0
7	0	1.5	2.8	5.0	8.3	13	18	25	31	37	41	42	41	37	31	25	18	13	8.3	5.0	2.8	1.5	.77	.36	.15	.06	.02	+	+	0
8	0	2.6	4.9	8.7	14	22	31	42	53	63	69	72	69	63	53	42	31	22	14	8.7	4.9	2.6	1.3	.63	.28	.11	.04	.01	+	0
9	0	2.4	4.4	7.4	12	18	25	34	42	49	54	56	54	49	42	34	25	18	12	7.4	4.4	2.4	1.2	.63	.29	.12	.05	.02	+	0
10	0	3.3	5.7	9.3	14	21	28	37	45	51	56	58	56	51	45	37	28	21	14	9.3	5.7	3.3	1.8	.98	.48	.22	.10	.04	.01	0
11	0	4.2	7.2	12	17	25	34	43	53	60	66	68	66	60	53	43	34	25	17	12	7.2	4.2	2.4	1.2	.64	.30	.13	.06	.02	0
12	0	3.7	6.0	9.4	14	20	26	33	40	46	49	51	49	46	40	33	26	20	14	9.4	6.0	3.7	2.1	1.1	.62	.31	.14	.06	.02	0
13	0	4.1	6.5	10	14	20	25	32	37	42	46	47	46	42	37	32	25	20	14	10	6.5	4.1	2.5	1.4	.79	.41	.20	.09	.04	0
14	0	4.1	6.4	10	14	19	24	30	35	39	42	43	42	39	35	30	24	19	14	10	6.4	4.1	2.5	1.4	.80	.42	.21	.10	.04	0
15	0	2.3	3.6	5.4	7.7	10	13	17	19	22	23	24	23	22	19	17	13	10	7.7	5.4	3.6	2.3	1.4	.86	.48	.26	.13	.06	.03	0
16	0	1.1	1.7	2.5	3.5	4.7	6.0	7.3	8.5	10	10	10	10	10	8.5	7.3	6.0	4.7	3.5	2.5	1.7	1.1	.75	.46	.26	.15	.08	.04	.02	0
17	0	.72	1.0	1.5	2.0	2.6	3.3	4.0	4.6	5.1	5.5	5.6	5.5	5.1	4.6	4.0	3.3	2.6	2.0	1.5	1.0	.72	.47	.29	.17	.10	.05	.02	.01	0
18	0	.32	.48	.68	.92	1.2	1.5	1.8	2.0	2.3	2.4	2.4	2.4	2.3	2.0	1.8	1.5	1.2	.92	.68	.48	.32	.21	.13	.08	.04	.02	.01	+	0
19	0	.08	.12	.17	.23	.30	.38	.45	.52	.58	.62	.64	.62	.58	.52	.45	.38	.30	.23	.17	.12	.08	.05	.03	.02	.01	+	+	+	0
20	0	.01	.01	.02	.03	.04	.05	.06	.07	.08	.08	.08	.08	.08	.07	.06	.05	.04	.03	.02	.01	.01	+	+	+	+	+	+	+	0
21	0	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	0
22	0	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	0
23	0	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	0
24	0	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	0
25	0	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	0
26	0	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	0
27	0	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	0
28	0	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	0
29	0	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	0
30	0	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	0
31	0	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	0
32	0	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	0
33	0	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	0
34	0	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0	0	0
35	0	0	0	0	0	0	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0
36	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
37	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
38	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
39	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
40	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
41	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
42	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
43	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
44	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0

SMALL CLOUDS AT 2700.00 SECONDS ELAPSED TIME FOR SILT

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID	LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	2940.	300.0	72.80	0.0000E+00	237.6	0.0000E+00	120.0	0.415500E-04
2	2941.	300.0	64.14	0.0000E+00	265.5	0.0000E+00	120.0	0.340000E-04
3	2941.	300.0	88.36	0.0000E+00	314.4	0.0000E+00	120.0	0.340000E-04
4	2941.	300.0	111.8	0.0000E+00	414.1	0.0000E+00	120.0	0.340000E-04
5	2941.	300.0	48.55	0.0000E+00	486.9	0.0000E+00	120.0	0.340000E-04
6	2941.	300.0	22.70	0.0000E+00	531.1	0.0000E+00	120.0	0.340000E-04
7	2941.	300.0	13.17	0.0000E+00	560.3	0.0000E+00	120.0	0.340000E-04
8	2940.	300.0	9.236	0.0000E+00	582.6	0.0000E+00	120.0	0.340000E-04
9	2940.	300.0	7.242	0.0000E+00	601.2	0.0000E+00	120.0	0.340000E-04

SUMMARY OF SILT DISTRIBUTIONS AFTER 3000.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 437.96
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 5150.5

SUMMARY OF SILT DISTRIBUTIONS AFTER 3300.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 437.92
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 5150.5

SUMMARY OF SILT DISTRIBUTIONS AFTER 3600.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 437.88
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 5150.5

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CONCENTRATIONS ABOVE BACKGROUND OF SILT     (MG/L) IN THE CLOUD   3600.00 SECONDS AFTER DUMP

               60.00 FT BELOW THE WATER SURFACE
...MULTIPLY DISPLAYED VALUES BY   1.000          (LEGEND... + = .LT. .01   . = .LT. .0001   0 = .LT. .000001)
M N=  2   3   4   5   6   7   8   9  10  11  12  13  14  15  16  17  18  19  20  21  22  23  24  25  26  27  28  29  30  31
 2 00000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000
 3 0000   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0  00000
 4 0000   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0  00000
 5 0000   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0  00000
 6 0000   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0  00000
 7 0000   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0  00000
 8 0000   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0  00000
 9 0000   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0  00000
10 0000   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0  00000
11 0000   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0  00000
12 0000   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0  00000
13 0000   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0  00000
14 0000   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0  00000
15 0000   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0  00000
16 0000   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0  00000
17 0000   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0  00000
18 0000   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0  00000
19 0000   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0  00000
20 0000   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0  00000
21 0000   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0  00000
22 0000   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0  00000
23 0000   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0  00000
24 0000   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0  00000
25 0000   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0  00000
26 0000   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0  00000
27 0000   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0  00000
28 0000   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0  00000
29 0000   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0  00000
30 0000   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0  00000
31 0000   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +  +0000
32 0000   +   +   + .01 .01 .01 .01 .01 .01 .01 .01 .01 .01 .01 .01 .01 .01 .01   +   +   +   +   +   +   +   +   +  +0000
33 0000 .04 .04 .05 .06 .07 .08 .09 .09 .10 .10 .10 .10 .10 .09 .09 .08 .07 .06 .05 .04 .04 .03 .02 .02 .01 .01   +  +0000
34 0000 .21 .25 .30 .36 .41 .46 .50 .54 .57 .59 .60 .59 .57 .54 .50 .46 .41 .36 .30 .25 .21 .17 .13 .10 .08 .06 .04 .030000
35 0000 .91 1.1 1.3 1.6 1.8 2.1 2.4 2.6 2.7 2.8 2.9 2.8 2.7 2.6 2.4 2.1 1.8 1.6 1.3 1.1 .91 .72 .56 .43 .32 .24 .17 .120000
36 0000 3.1 4.0 5.0 6.1 7.3 8.6  10  11  12  12  13  12  12  11  10 8.6 7.3 6.1 5.0 4.0 3.1 2.4 1.8 1.3 1.0 .74 .53 .370000
37 0000 8.4  11  15  19  24  29  35  40  45  48  49  48  45  40  35  29  24  19  15  11 8.4 6.3 4.6 3.3 2.4 1.7 1.1 .820000
38 0000  16  23  31  42  55  71  88 104 117 126 130 126 117 104  88  71  55  42  31  23  16  12 8.2 5.8 4.0 2.8 1.9 1.30000
39 0000  19  27  38  52  69  90 112 133 151 164 168 164 151 133 112  90  69  52  38  27  19  14  10 6.6 4.6 3.2 2.1 1.40000
40 0000  13  18  25  33  43  54  66  78  88  94  97  94  88  78  66  54  43  33  25  18  13  10 6.9 4.9 3.5 2.4 1.6 1.10000
41 0000 6.0 7.9  10  13  16  19  22  25  28  30  30  30  28  25  22  19  16  13  10 7.9 6.0 4.5 3.4 2.5 1.8 1.3 .91 .640000
42 0000 2.0 2.5 3.1 3.8 4.5 5.2 5.9 6.5 7.0 7.3 7.4 7.3 7.0 6.5 5.9 5.2 4.5 3.8 3.1 2.5 2.0 1.6 1.2 .93 .69 .50 .36 .260000
43 0000 .54 .67 .80 .95 1.1 1.2 1.3 1.4 1.5 1.6 1.6 1.6 1.5 1.4 1.3 1.2 1.1 .95 .80 .67 .54 .43 .34 .26 .20 .15 .11 .080000
44 00000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000
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CONCENTRATIONS ABOVE BACKGROUND OF SILT (MG/L) IN THE CLOUD 3600.00 SECONDS AFTER DUMP

119.00 FT BELOW THE WATER SURFACE

...MULTIPLY DISPLAYED VALUES BY 1.000 (LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)

M N=	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30 31
2	000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000																												
3	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
4	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
5	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
6	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
7	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
8	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
9	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
10	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
11	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
12	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
13	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
14	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
15	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
16	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
17	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
18	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
19	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
20	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
21	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
22	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
23	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
24	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
25	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
26	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
27	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
28	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
29	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
30	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
31	0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.0000
32	0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+0000
33	0000	+	+	+	+	.01	.01	.01	.01	.01	.01	.01	.01	.01	.01	.01	.01	.01	+	+	+	+	+	+	+	+	+	+	+0000
34	0000	.03	.03	.04	.05	.05	.06	.07	.07	.08	.08	.08	.08	.08	.07	.07	.06	.05	.05	.04	.03	.03	.02	.01	.01	.01	+	+	+0000
35	0000	.13	.16	.19	.23	.27	.31	.34	.37	.40	.41	.42	.41	.40	.37	.34	.31	.27	.23	.19	.16	.13	.10	.08	.06	.04	.03	.02	.010000
36	0000	.45	.57	.72	.88	1.0	1.2	1.4	1.5	1.7	1.7	1.8	1.7	1.7	1.5	1.4	1.2	1.0	.88	.72	.57	.45	.35	.26	.20	.14	.10	.07	.050000
37	0000	1.2	1.6	2.1	2.7	3.4	4.2	5.0	5.8	6.4	6.8	7.0	6.8	6.4	5.8	5.0	4.2	3.4	2.7	2.1	1.6	1.2	.91	.66	.48	.34	.24	.17	.110000
38	0000	2.3	3.2	4.5	6.0	8.0	10	13	15	17	18	19	18	17	15	13	10	8.0	6.0	4.5	3.2	2.3	1.6	1.1	.84	.58	.40	.28	.190000
39	0000	2.8	3.9	5.5	7.5	10	13	16	19	22	24	24	24	22	19	16	13	10	7.5	5.5	3.9	2.8	1.9	1.3	.96	.67	.46	.31	.210000
40	0000	1.9	2.6	3.6	4.7	6.2	7.8	10	11	13	14	14	14	13	11	10	7.8	6.2	4.7	3.6	2.6	1.9	1.4	1.0	.71	.50	.35	.24	.160000
41	0000	.87	1.1	1.4	1.8	2.2	2.7	3.2	3.6	4.0	4.2	4.3	4.2	4.0	3.6	3.2	2.7	2.2	1.8	1.4	1.1	.87	.66	.49	.36	.26	.18	.13	.090000
42	0000	.29	.37	.45	.55	.65	.75	.85	.94	1.0	1.0	1.0	1.0	1.0	.94	.85	.75	.65	.55	.45	.37	.29	.23	.17	.13	.10	.07	.05	.030000
43	0000	.07	.09	.11	.13	.15	.18	.19	.21	.22	.23	.24	.23	.22	.21	.19	.18	.15	.13	.11	.09	.07	.06	.04	.03	.02	.02	.01	.010000
44	000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000																												

```
BOTTOM ACCUMULATION OF SILT     (CU FT/GRID SQUARE) ,   3600.00 SECONDS AFTER DUMP
...MULTIPLY DISPLAYED VALUES BY   1.000         (LEGEND... + = .LT. .01   . = .LT. .0001   0 = .LT. .000001)
M N=  2   3   4   5   6   7   8   9  10  11  12  13  14  15  16  17  18  19  20  21  22  23  24  25  26  27  28  29  30  31
 2 000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000
 3 0000   .   .   .   .   .   .   .   +   +   +   +   +   +   +   .   .   .   .   .   .   .   .   .   0   0   0   0   00000
 4 0000   +   +   +   +   +   +   + .01 .01 .01 .01 .01 .01 .01   +   +   +   +   +   +   +   +   +   .   .   .   .   .0000
 5 0000 .02 .04 .07 .12 .19 .28 .37 .47 .56 .61 .63 .61 .56 .47 .37 .28 .19 .12 .07 .04 .02 .01   +   +   +   +   +   .0000
 6 0000 .32 .60 1.0 1.7 2.6 3.8 5.1 6.5 7.6 8.5 8.7 8.5 7.6 6.5 5.1 3.8 2.6 1.7 1.0 .60 .32 .16 .07 .03 .01   +   +   +0000
 7 0000 1.5 2.8 5.0 8.3  13  18  25  31  37  41  42  41  37  31  25  18  13 8.3 5.0 2.8 1.5 .77 .36 .15 .06 .02   +   +0000
 8 0000 2.6 4.9 8.7  14  22  31  42  53  63  69  72  69  63  53  42  31  22  14 8.7 4.9 2.6 1.3 .63 .28 .11 .04 .01   +0000
 9 0000 2.4 4.4 7.4  12  18  25  34  42  49  54  56  54  49  42  34  25  18  12 7.4 4.4 2.4 1.2 .63 .29 .12 .05 .02   +0000
10 0000 3.3 5.7 9.3  14  21  28  37  45  51  56  58  56  51  45  37  28  21  14 9.3 5.7 3.3 1.8 .98 .48 .22 .10 .04 .010000
11 0000 4.2 7.2  12  17  25  34  43  53  60  66  68  66  60  53  43  34  25  17  12 7.2 4.2 2.4 1.2 .64 .30 .13 .06 .020000
12 0000 3.7 6.0 9.4  14  20  26  33  40  46  49  51  49  46  40  33  26  20  14 9.4 6.0 3.7 2.1 1.1 .62 .31 .14 .06 .020000
13 0000 4.1 6.5  10  14  20  25  32  37  42  46  47  46  42  37  32  25  20  14  10 6.5 4.1 2.5 1.4 .79 .41 .20 .09 .040000
14 0000 4.1 6.4  10  14  19  24  30  35  39  42  43  42  39  35  30  24  19  14  10 6.4 4.1 2.5 1.4 .80 .42 .21 .10 .040000
15 0000 2.3 3.6 5.4 7.7  10  13  17  19  22  23  24  23  22  19  17  13  10 7.7 5.4 3.6 2.3 1.4 .86 .48 .26 .13 .06 .030000
16 0000 1.1 1.7 2.5 3.5 4.7 6.0 7.3 8.5  10  10  10  10  10 8.5 7.3 6.0 4.7 3.5 2.5 1.7 1.1 .75 .46 .26 .15 .08 .04 .020000
17 0000 .72 1.0 1.5 2.0 2.6 3.3 4.0 4.6 5.1 5.5 5.6 5.5 5.1 4.6 4.0 3.3 2.6 2.0 1.5 1.0 .72 .47 .29 .17 .10 .05 .02 .010000
18 0000 .32 .48 .68 .92 1.2 1.5 1.8 2.0 2.3 2.4 2.4 2.4 2.3 2.0 1.8 1.5 1.2 .92 .68 .48 .32 .21 .13 .08 .04 .02 .01   +0000
19 0000 .08 .12 .17 .23 .30 .38 .45 .52 .58 .62 .64 .62 .58 .52 .45 .38 .30 .23 .17 .12 .08 .05 .03 .02 .01   +   +   +0000
20 0000 .01 .01 .02 .03 .04 .05 .06 .07 .08 .08 .08 .08 .08 .07 .06 .05 .04 .03 .02 .01 .01   +   +   +   +   +   +   +0000
21 0000   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   .   .   .0000
22 0000   .   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   .   .   .   .   .   .   .   .0000
23 0000   .   .   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   .   .   .   .   .   .   .   .   00000
24 0000   .   .   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   .   .   .   .   .   .   .   .   .0000
25 0000   .   .   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   .   .   .   .   .   .   .   .   .0000
26 0000   .   .   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   .   .   .   .   .   .   .   .   .0000
27 0000   .   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   .   .   .   .   .   .   .   .0000
28 0000   .   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   .   .   .   .   .   .   .   .0000
29 0000   .   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   .   .   .   .   .   .   .   .0000
30 0000   .   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   .   .   .   .   .   .   .   .0000
31 0000   .   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   .   .   .   .   .   .   .   .0000
32 0000   .   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   .   .   .   .   .   .   .   .0000
33 0000   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   .   .   .   .   .   .   .0000
34 0000   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   .   .   .   .   .   .   .0000
35 0000   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   .   .   .   .   .   .   .0000
36 0000   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   .   .   .   .   .   .   .0000
37 0000   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   .   .   .   .   .   .   .0000
38 0000   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   .   .   .   .   .   .0000
39 0000   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   .   .   .   .   .   .   .0000
40 0000   .   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   .   .   .   .   .   .   .   .0000
41 0000   .   .   .   .   +   +   +   +   +   +   +   +   +   +   +   +   +   .   .   .   .   .   .   .   .   .   .   .0000
42 0000   .   .   .   .   .   .   .   .   .   .   .   .   .   .   .   .   .   .   .   .   .   .   .   .   .   .   .   .0000
43 0000   .   .   .   .   .   .   .   .   .   .   .   .   .   .   .   .   .   .   .   .   .   .   .   .   .   0   0   00000
44 000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000
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SMALL CLOUDS AT 3600.00 SECONDS ELAPSED TIME FOR SILT

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID	LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	3781.	300.0	72.78	0.0000E+00	322.9	0.0000E+00	120.0	0.340000E-04
2	3781.	300.0	64.13	0.0000E+00	353.8	0.0000E+00	120.0	0.340000E-04
3	3782.	300.0	88.34	0.0000E+00	407.5	0.0000E+00	120.0	0.340000E-04
4	3782.	300.0	111.8	0.0000E+00	515.6	0.0000E+00	120.0	0.340000E-04
5	3782.	300.0	48.54	0.0000E+00	593.8	0.0000E+00	120.0	0.340000E-04
6	3782.	300.0	22.70	0.0000E+00	641.0	0.0000E+00	120.0	0.340000E-04
7	3781.	300.0	13.16	0.0000E+00	672.2	0.0000E+00	120.0	0.340000E-04
8	3781.	300.0	9.234	0.0000E+00	695.9	0.0000E+00	120.0	0.340000E-04
9	3781.	300.0	7.240	0.0000E+00	715.6	0.0000E+00	120.0	0.340000E-04

BOTTOM ACCUMULATION OF SILT (CU FT/GRID SQUARE) , 3600.00 SECONDS AFTER DUMP

...MULTIPLY DISPLAYED VALUES BY 1.000 (LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)

M N=	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31
2	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000
3	0000	.	.	.	.	.	.	.	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	0	0	0	0	0	0000
4	0000	+	+	+	+	+	+	+	.01	.01	.01	.01	.01	.01	.01	+	+	+	+	+	+	+	+	+	.	.	.	.	.	0000
5	0000	.02	.04	.07	.12	.19	.28	.37	.47	.56	.61	.63	.61	.56	.47	.37	.28	.19	.12	.07	.04	.02	.01	+	+	+	+	+	.	0000
6	0000	.32	.60	1.0	1.7	2.6	3.8	5.1	6.5	7.6	8.5	8.7	8.5	7.6	6.5	5.1	3.8	2.6	1.7	1.0	.60	.32	.16	.07	.03	.01	+	+	+	0000
7	0000	1.5	2.8	5.0	8.3	13	18	25	31	37	41	42	41	37	31	25	18	13	8.3	5.0	2.8	1.5	.77	.36	.15	.06	.02	+	+	0000
8	0000	2.6	4.9	8.7	14	22	31	42	53	63	69	72	69	63	53	42	31	22	14	8.7	4.9	2.6	1.3	.63	.28	.11	.04	.01	+	0000
9	0000	2.4	4.4	7.4	12	18	25	34	42	49	54	56	54	49	42	34	25	18	12	7.4	4.4	2.4	1.2	.63	.29	.12	.05	.02	+	0000
10	0000	3.3	5.7	9.3	14	21	28	37	45	51	56	58	56	51	45	37	28	21	14	9.3	5.7	3.3	1.8	.98	.48	.22	.10	.04	.01	0000
11	0000	4.2	7.2	12	17	25	34	43	53	60	66	68	66	60	53	43	34	25	17	12	7.2	4.2	2.4	1.2	.64	.30	.13	.06	.02	0000
12	0000	3.7	6.0	9.4	14	20	26	33	40	46	49	51	49	46	40	33	26	20	14	9.4	6.0	3.7	2.1	1.1	.62	.31	.14	.06	.02	0000
13	0000	4.1	6.5	10	14	20	25	32	37	42	46	47	46	42	37	32	25	20	14	10	6.5	4.1	2.5	1.4	.79	.41	.20	.09	.04	0000
14	0000	4.1	6.4	10	14	19	24	30	35	39	42	43	42	39	35	30	24	19	14	10	6.4	4.1	2.5	1.4	.80	.42	.21	.10	.04	0000
15	0000	2.3	3.6	5.4	7.7	10	13	17	19	22	23	24	23	22	19	17	13	10	7.7	5.4	3.6	2.3	1.4	.86	.48	.26	.13	.06	.03	0000
16	0000	1.1	1.7	2.5	3.5	4.7	6.0	7.3	8.5	10	10	10	10	10	8.5	7.3	6.0	4.7	3.5	2.5	1.7	1.1	.75	.46	.26	.15	.08	.04	.02	0000
17	0000	.72	1.0	1.5	2.0	2.6	3.3	4.0	4.6	5.1	5.5	5.6	5.5	5.1	4.6	4.0	3.3	2.6	2.0	1.5	1.0	.72	.47	.29	.17	.10	.05	.02	.01	0000
18	0000	.32	.48	.68	.92	1.2	1.5	1.8	2.0	2.3	2.4	2.4	2.4	2.3	2.0	1.8	1.5	1.2	.92	.68	.48	.32	.21	.13	.08	.04	.02	.01	+	0000
19	0000	.08	.12	.17	.23	.30	.38	.45	.52	.58	.62	.64	.62	.58	.52	.45	.38	.30	.23	.17	.12	.08	.05	.03	.02	.01	+	+	+	0000
20	0000	.01	.01	.02	.03	.04	.05	.06	.07	.08	.08	.08	.08	.08	.07	.06	.05	.04	.03	.02	.01	.01	+	+	+	+	+	+	+	0000
21	0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	0000
22	0000	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	0000
23	0000	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	0	0000
24	0000	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	0000
25	0000	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	0000
26	0000	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	0000
27	0000	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	0000
28	0000	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	0000
29	0000	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	0000
30	0000	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	0000
31	0000	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	0000
32	0000	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	0000
33	0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	0000
34	0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	0000
35	0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	0000
36	0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	0000
37	0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	0000
38	0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	0000
39	0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	0000
40	0000	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	0000
41	0000	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	0000
42	0000	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	0000
43	0000	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0000
44	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000

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THICKNESS (FT) OF SILT     ACCUMULATED ON BOTTOM,     3600.00 SECONDS AFTER DUMP
...MULTIPLY DISPLAYED VALUES BY   1.000          (LEGEND... + = .LT. .01   . = .LT. .0001   0 = .LT. .000001)
M N=  2   3   4   5   6   7   8   9  10  11  12  13  14  15  16  17  18  19  20  21  22  23  24  25  26  27  28  29  30  31
 2 000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000
 3 0000   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   00000
 4 0000   .   .   .   .   .   .   .   .   .   .   .   .   .   .   .   .   .   .   .   .   .   0   0   0   0   0   0   00000
 5 0000   .   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   .   .   .   .   .   0   0   00000
 6 0000   +   +   +   +   +   + .01 .01 .01 .02 .02 .02 .01 .01 .01   +   +   +   +   +   +   +   +   .   .   .   .   .0000
 7 0000   +   + .01 .01 .03 .04 .05 .07 .08 .09 .10 .09 .08 .07 .05 .04 .03 .01 .01   +   +   +   +   +   +   .   .   .0000
 8 0000   + .01 .02 .03 .05 .07 .10 .12 .15 .16 .17 .16 .15 .12 .10 .07 .05 .03 .02 .01   +   +   +   +   +   +   .   .0000
 9 0000   + .01 .01 .02 .04 .06 .08 .10 .11 .12 .13 .12 .11 .10 .08 .06 .04 .02 .01 .01   +   +   +   +   +   +   .   .0000
10 0000   + .01 .02 .03 .04 .06 .08 .10 .12 .13 .13 .13 .12 .10 .08 .06 .04 .03 .02 .01   +   +   +   +   +   +   +   .0000
11 0000 .01 .01 .02 .04 .05 .08 .10 .12 .14 .15 .16 .15 .14 .12 .10 .08 .05 .04 .02 .01 .01   +   +   +   +   +   +   .0000
12 0000   + .01 .02 .03 .04 .06 .07 .09 .10 .11 .12 .11 .10 .09 .07 .06 .04 .03 .02 .01   +   +   +   +   +   +   +   .0000
13 0000 .01 .01 .02 .03 .04 .06 .07 .08 .10 .10 .11 .10 .10 .08 .07 .06 .04 .03 .02 .01 .01   +   +   +   +   +   +   +0000
14 0000   + .01 .02 .03 .04 .05 .07 .08 .09 .10 .10 .10 .09 .08 .07 .05 .04 .03 .02 .01   +   +   +   +   +   +   +   +0000
15 0000   +   + .01 .01 .02 .03 .03 .04 .05 .05 .05 .05 .05 .04 .03 .03 .02 .01 .01   +   +   +   +   +   +   +   +   .0000
16 0000   +   +   +   + .01 .01 .01 .02 .02 .02 .02 .02 .02 .02 .01 .01 .01   +   +   +   +   +   +   +   +   +   +   .0000
17 0000   +   +   +   +   +   +   + .01 .01 .01 .01 .01 .01 .01   +   +   +   +   +   +   +   +   +   +   +   +   .   .0000
18 0000   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   .   .   .0000
19 0000   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   .   .   .   .   .   .0000
20 0000   .   .   .   .   .   +   +   +   +   +   +   +   +   +   +   +   .   .   .   .   .   .   .   .   .   .   .   00000
21 0000   .   .   .   .   .   .   .   .   .   .   .   .   .   .   .   .   .   .   .   .   .   .   0   0   0   0   0   00000
22 0000   0   0   0   0   .   .   .   .   .   .   .   .   .   .   .   .   .   0   0   0   0   0   0   0   0   0   0   00000
23 0000   0   0   0   0   0   .   .   .   .   .   .   .   .   .   .   .   0   0   0   0   0   0   0   0   0   0   0   00000
24 0000   0   0   0   0   0   .   .   .   .   .   .   .   .   .   .   .   0   0   0   0   0   0   0   0   0   0   0   00000
25 0000   0   0   0   0   .   .   .   .   .   .   .   .   .   .   .   .   .   0   0   0   0   0   0   0   0   0   0   00000
26 0000   0   0   0   0   0   0   .   .   .   .   .   .   .   .   .   0   0   0   0   0   0   0   0   0   0   0   0   00000
27 0000   0   0   0   0   0   .   .   .   .   .   .   .   .   .   .   .   0   0   0   0   0   0   0   0   0   0   0   00000
28 0000   0   0   0   0   0   .   .   .   .   .   .   .   .   .   .   .   0   0   0   0   0   0   0   0   0   0   0   00000
29 0000   0   0   0   0   0   .   .   .   .   .   .   .   .   .   .   .   0   0   0   0   0   0   0   0   0   0   0   00000
30 0000   0   0   0   0   .   .   .   .   .   .   .   .   .   .   .   .   .   0   0   0   0   0   0   0   0   0   0   00000
31 0000   0   0   0   0   .   .   .   .   .   .   .   .   .   .   .   .   .   0   0   0   0   0   0   0   0   0   0   00000
32 0000   0   0   0   0   0   .   .   .   .   .   .   .   .   .   .   .   0   0   0   0   0   0   0   0   0   0   0   00000
33 0000   0   0   0   0   .   .   .   .   .   .   .   .   .   .   .   .   .   0   0   0   0   0   0   0   0   0   0   00000
34 0000   0   0   0   0   .   .   .   .   .   .   .   .   .   .   .   .   .   0   0   0   0   0   0   0   0   0   0   00000
35 0000   0   0   0   0   .   .   .   .   .   .   .   .   .   .   .   .   .   0   0   0   0   0   0   0   0   0   0   00000
36 0000   0   0   0   0   .   .   .   .   .   .   .   .   .   .   .   .   .   0   0   0   0   0   0   0   0   0   0   00000
37 0000   0   0   0   0   .   .   .   .   .   .   .   .   .   .   .   .   .   0   0   0   0   0   0   0   0   0   0   00000
38 0000   0   0   0   0   .   .   .   .   .   .   .   .   .   .   .   .   .   0   0   0   0   0   0   0   0   0   0   00000
39 0000   0   0   0   0   .   .   .   .   .   .   .   .   .   .   .   .   .   0   0   0   0   0   0   0   0   0   0   00000
40 0000   0   0   0   0   0   0   .   .   .   .   .   .   .   .   .   0   0   0   0   0   0   0   0   0   0   0   0   00000
41 0000   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   00000
42 0000   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   00000
43 0000   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   00000
44 000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000
```

BEGIN LONG TERM SIMULATION OF FATE OF CLAY

SUMMARY OF CLAY DISTRIBUTIONS AFTER 300.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 1868.4
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 0.00000E+00

SUMMARY OF CLAY DISTRIBUTIONS AFTER 600.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 1868.4
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 0.00000E+00

SUMMARY OF CLAY DISTRIBUTIONS AFTER 900.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 1868.4
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 0.00000E+00

CONCENTRATIONS ABOVE BACKGROUND OF CLAY (MG/L) IN THE CLOUD 900.00 SECONDS AFTER DUMP

60.00 FT BELOW THE WATER SURFACE

...MULTIPLY DISPLAYED VALUES BY 1.000 (LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)

M N=	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30 31
2	000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000																												
3	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
4	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
5	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
6	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
7	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
8	0000	0	0	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0	0	0	0	0	00000
9	0000	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	0	0	0	0	0	0	00000
10	0000	+	+	+	+	+	+	.01	.01	.01	.01	.01	.01	.01	.01	.01	+	+	+	+	+	+	0	0	0	0	0	0	00000
11	0000	.01	.03	.05	.08	.13	.19	.25	.32	.38	.43	.44	.43	.38	.32	.25	.19	.13	.08	.05	.03	.01	0	0	0	0	0	0	00000
12	0000	.14	.27	.49	.85	1.4	2.2	3.3	4.6	5.8	6.8	7.2	6.8	5.8	4.6	3.3	2.2	1.4	.85	.49	.27	.14	0	0	0	0	0	0	00000
13	0000	.47	.96	1.8	3.6	6.8	13	22	39	68	105	125	105	68	39	22	13	6.8	3.6	1.8	.96	.47	0	0	0	0	0	0	00000
14	0000	.53	1.0	2.1	4.2	8.0	15	28	53	104	182	227	182	104	53	28	15	8.0	4.2	2.1	1.0	.53	0	0	0	0	0	0	00000
15	0000	.19	.37	.68	1.2	2.0	3.3	5.0	7.2	9.4	11	12	11	9.4	7.2	5.0	3.3	2.0	1.2	.68	.37	.19	0	0	0	0	0	0	00000
16	0000	.02	.05	.08	.14	.21	.31	.42	.54	.65	.73	.76	.73	.65	.54	.42	.31	.21	.14	.08	.05	.02	0	0	0	0	0	0	00000
17	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
18	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
19	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
20	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
21	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
22	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
23	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
24	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
25	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
26	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
27	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
28	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
29	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
30	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
31	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
32	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
33	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
34	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
35	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
36	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
37	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
38	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
39	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
40	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
41	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
42	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
43	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
44	000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000																												

CONCENTRATIONS ABOVE BACKGROUND OF CLAY (MG/L) IN THE CLOUD 900.00 SECONDS AFTER DUMP

119.00 FT BELOW THE WATER SURFACE

...MULTIPLY DISPLAYED VALUES BY 10.00 (LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)

M N=	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	0	0	0	0	0	0	0	0	0
9	.01	.02	.04	.06	.08	.11	.13	.16	.18	.19	.20	.19	.18	.16	.13	.11	.08	.06	.04	.02	.01	0	0	0	0	0	0	0	0	0
10	.41	.64	.96	1.3	1.8	2.4	2.9	3.5	3.9	4.2	4.3	4.2	3.9	3.5	2.9	2.4	1.8	1.3	.96	.64	.41	0	0	0	0	0	0	0	0	0
11	4.2	6.6	10	14	19	25	31	36	41	44	45	44	41	36	31	25	19	14	10	6.6	4.2	0	0	0	0	0	0	0	0	0
12	20	32	48	68	93	120	149	175	197	212	217	212	197	175	149	120	93	68	48	32	20	0	0	0	0	0	0	0	0	0
13	46	73	108	155	210	273	337	398	449	482	494	482	449	398	337	273	210	155	108	73	46	0	0	0	0	0	0	0	0	0
14	49	77	116	165	224	290	359	424	478	514	527	514	478	424	359	290	224	165	116	77	49	0	0	0	0	0	0	0	0	0
15	25	39	58	82	112	145	179	212	238	256	262	256	238	212	179	145	112	82	58	39	25	0	0	0	0	0	0	0	0	0
16	5.7	9.0	14	19	26	34	42	50	56	60	61	60	56	50	42	34	26	19	14	9.0	5.7	0	0	0	0	0	0	0	0	0
17	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
18	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
19	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
20	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
21	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
22	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
23	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
24	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
25	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
26	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
27	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
28	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
29	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
30	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
31	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
32	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
33	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
34	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
35	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
36	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
37	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
38	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
39	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
40	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
41	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
42	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
43	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
44	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0

SMALL CLOUDS AT 900.00 SECONDS ELAPSED TIME FOR CLAY

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID	LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	1259.	300.0	24.29	0.0000E+00	96.85	0.0000E+00	120.0	0.115465E-03
2	1259.	300.0	21.43	0.0000E+00	117.6	0.0000E+00	120.0	0.581638E-04
3	1259.	300.0	29.71	0.0000E+00	155.1	33.27	86.73	0.697250E-04
4	1259.	300.0	37.68	0.0000E+00	235.3	34.48	85.52	0.429446E-04
5	1259.	300.0	16.37	0.0000E+00	296.0	42.52	77.48	0.340000E-04
6	1259.	300.0	7.644	0.0000E+00	333.5	40.11	79.89	0.340000E-04
7	1259.	300.0	4.425	0.0000E+00	358.6	37.98	82.02	0.340000E-04
8	1259.	300.0	3.103	0.0000E+00	377.8	37.41	82.59	0.340000E-04
9	1259.	300.0	2.432	0.0000E+00	393.8	37.58	82.42	0.340000E-04
10	1258.	300.0	1721.	0.0000E+00	407.8	113.8	6.230	0.690000E-02

SUMMARY OF CLAY DISTRIBUTIONS AFTER 1200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 1868.4
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 0.00000E+00

SUMMARY OF CLAY DISTRIBUTIONS AFTER 1500.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 1868.4
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 0.00000E+00

SUMMARY OF CLAY DISTRIBUTIONS AFTER 1800.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 1868.4
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 0.00000E+00

CONCENTRATIONS ABOVE BACKGROUND OF CLAY (MG/L) IN THE CLOUD 1800.00 SECONDS AFTER DUMP

60.00 FT BELOW THE WATER SURFACE

...MULTIPLY DISPLAYED VALUES BY 1.000 (LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)

M	N= 2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30 31
2	00000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000																												
3	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
4	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
5	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
6	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
7	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
8	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
9	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
10	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
11	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
12	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
13	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
14	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
15	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
16	0000	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	0	0	0	0	00000
17	0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	0	0	0	0	00000
18	0000	+	.01	.01	.02	.02	.03	.04	.04	.05	.05	.05	.05	.05	.04	.04	.03	.02	.02	.01	.01	+	+	+	0	0	0	0	00000
19	0000	.07	.10	.15	.21	.28	.37	.45	.53	.60	.64	.66	.64	.60	.53	.45	.37	.28	.21	.15	.10	.07	.04	.03	0	0	0	0	00000
20	0000	.41	.64	.98	1.4	2.0	2.7	3.5	4.3	5.1	5.6	5.8	5.6	5.1	4.3	3.5	2.7	2.0	1.4	.98	.64	.41	.25	.15	0	0	0	0	00000
21	0000	1.3	2.2	3.5	5.6	8.7	13	20	28	38	46	49	46	38	28	20	13	8.7	5.6	3.5	2.2	1.3	.78	.45	0	0	0	0	00000
22	0000	2.0	3.4	5.8	10	16	28	49	83	128	170	188	170	128	83	49	28	16	10	5.8	3.4	2.0	1.1	.66	0	0	0	0	00000
23	0000	1.3	2.2	3.5	5.6	8.7	13	20	28	37	45	49	45	37	28	20	13	8.7	5.6	3.5	2.2	1.3	.78	.45	0	0	0	0	00000
24	0000	.41	.65	.98	1.4	2.0	2.7	3.5	4.4	5.1	5.6	5.8	5.6	5.1	4.4	3.5	2.7	2.0	1.4	.98	.65	.41	.25	.15	0	0	0	0	00000
25	0000	.07	.10	.15	.21	.28	.37	.45	.53	.60	.65	.66	.65	.60	.53	.45	.37	.28	.21	.15	.10	.07	.04	.03	0	0	0	0	00000
26	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
27	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
28	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
29	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
30	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
31	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
32	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
33	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
34	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
35	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
36	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
37	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
38	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
39	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
40	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
41	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
42	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
43	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
44	00000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000																												

CONCENTRATIONS ABOVE BACKGROUND OF CLAY   (MG/L) IN THE CLOUD   1800.00 SECONDS AFTER DUMP

119.00 FT BELOW THE WATER SURFACE

...MULTIPLY DISPLAYED VALUES BY   10.00   (LEGEND... + = .LT. .01   . = .LT. .0001   0 = .LT. .000001)

M N=	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30 31
2	000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000																												
3	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
4	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
5	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
6	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
7	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
8	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
9	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
10	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
11	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
12	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
13	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
14	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
15	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
16	0000	+	.01	.01	.02	.02	.02	.03	.03	.04	.04	.04	.04	.04	.03	.03	.02	.02	.02	.01	.01	+	+	+	0	0	0	0	00000
17	0000	.13	.18	.23	.29	.36	.42	.48	.54	.58	.61	.62	.61	.58	.54	.48	.42	.36	.29	.23	.18	.13	.09	.07	0	0	0	0	00000
18	0000	1.2	1.6	2.0	2.6	3.1	3.7	4.3	4.8	5.1	5.4	5.5	5.4	5.1	4.8	4.3	3.7	3.1	2.6	2.0	1.6	1.2	.87	.62	0	0	0	0	00000
19	0000	6.5	8.7	11	14	17	21	24	26	28	30	30	30	28	26	24	21	17	14	11	8.7	6.5	4.7	3.3	0	0	0	0	00000
20	0000	22	29	38	48	58	69	79	88	95	99	100	99	95	88	79	69	58	48	38	29	22	16	11	0	0	0	0	00000
21	0000	45	61	78	98	120	142	163	181	195	204	208	204	195	181	163	142	120	98	78	61	45	33	23	0	0	0	0	00000
22	0000	58	77	99	125	152	180	207	230	249	261	265	261	249	230	207	180	152	125	99	77	58	42	30	0	0	0	0	00000
23	0000	45	60	78	98	119	140	161	179	193	202	206	202	193	179	161	140	119	98	78	60	45	33	23	0	0	0	0	00000
24	0000	22	29	37	47	57	67	77	86	93	97	99	97	93	86	77	67	57	47	37	29	22	16	11	0	0	0	0	00000
25	0000	6.3	8.5	11	14	17	20	23	25	27	29	29	29	27	25	23	20	17	14	11	8.5	6.3	4.6	3.2	0	0	0	0	00000
26	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
27	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
28	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
29	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
30	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
31	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
32	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
33	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
34	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
35	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
36	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
37	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
38	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
39	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
40	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
41	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
42	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
43	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
44	000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000																												

SMALL CLOUDS AT 1800.00 SECONDS ELAPSED TIME FOR CLAY

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID	LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	2100.	300.0	24.29	0.0000E+00	161.8	0.0000E+00	120.0	0.359888E-04
2	2100.	300.0	21.43	0.0000E+00	186.4	0.0000E+00	120.0	0.340000E-04
3	2100.	300.0	29.71	0.0000E+00	229.9	0.0000E+00	120.0	0.340000E-04
4	2100.	300.0	37.68	0.0000E+00	320.4	0.0000E+00	120.0	0.340000E-04
5	2100.	300.0	16.37	0.0000E+00	387.4	0.0000E+00	120.0	0.340000E-04
6	2100.	300.0	7.644	0.0000E+00	428.4	0.0000E+00	120.0	0.340000E-04
7	2100.	300.0	4.425	0.0000E+00	455.6	0.0000E+00	120.0	0.340000E-04
8	2100.	300.0	3.103	0.0000E+00	476.4	0.0000E+00	120.0	0.340000E-04
9	2099.	300.0	2.432	0.0000E+00	493.8	0.0000E+00	120.0	0.340000E-04
10	2099.	300.0	1721.	0.0000E+00	508.9	112.6	7.392	0.662131E-02

SUMMARY OF CLAY DISTRIBUTIONS AFTER 2100.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 1868.4
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 0.00000E+00

SUMMARY OF CLAY DISTRIBUTIONS AFTER 2400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 1868.4
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 0.00000E+00

SUMMARY OF CLAY DISTRIBUTIONS AFTER 2700.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 1868.4
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 0.00000E+00

CONCENTRATIONS ABOVE BACKGROUND OF CLAY (MG/L) IN THE CLOUD 2700.00 SECONDS AFTER DUMP

60.00 FT BELOW THE WATER SURFACE

...MULTIPLY DISPLAYED VALUES BY 1.000 (LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)

M N=	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31
2	000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000																													
3	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		00000
4	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		00000
5	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		00000
6	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		00000
7	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		00000
8	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		00000
9	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		00000
10	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		00000
11	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		00000
12	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		00000
13	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		00000
14	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		00000
15	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		00000
16	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		00000
17	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		00000
18	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		00000
19	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		00000
20	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		00000
21	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		00000
22	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		00000
23	0000	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	0	0		00000
24	0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	0	0		00000
25	0000	+	+	+	+	+	.01	.01	.01	.01	.01	.01	.01	.01	.01	.01	.01	+	+	+	+	+	+	+	+	+	0	0		00000
26	0000	.02	.03	.04	.06	.07	.08	.09	.10	.11	.11	.12	.11	.11	.10	.09	.08	.07	.06	.04	.03	.02	.02	.01	.01	+	0	0		00000
27	0000	.17	.23	.29	.37	.46	.55	.64	.71	.78	.82	.83	.82	.78	.71	.64	.55	.46	.37	.29	.23	.17	.12	.09	.06	.04	0	0		00000
28	0000	.74	1.0	1.3	1.8	2.3	2.8	3.4	3.9	4.4	4.7	4.8	4.7	4.4	3.9	3.4	2.8	2.3	1.8	1.3	1.0	.74	.52	.36	.24	.16	0	0		00000
29	0000	2.1	3.1	4.5	6.3	8.7	12	15	19	23	25	26	25	23	19	15	12	8.7	6.3	4.5	3.1	2.1	1.4	.99	.65	.42	0	0		00000
30	0000	3.9	5.9	9.0	14	21	30	43	57	72	82	86	82	72	57	43	30	21	14	9.0	5.9	3.9	2.5	1.6	1.0	.67	0	0		00000
31	0000	3.6	5.5	8.3	13	19	27	38	51	63	72	75	72	63	51	38	27	19	13	8.3	5.5	3.6	2.4	1.5	1.0	.64	0	0		00000
32	0000	1.8	2.6	3.7	5.1	7.0	9.2	12	15	17	19	19	19	17	15	12	9.2	7.0	5.1	3.7	2.6	1.8	1.2	.85	.56	.36	0	0		00000
33	0000	.58	.80	1.0	1.3	1.7	2.1	2.5	2.9	3.2	3.4	3.5	3.4	3.2	2.9	2.5	2.1	1.7	1.3	1.0	.80	.58	.41	.29	.19	.13	0	0		00000
34	0000	.12	.16	.21	.27	.33	.39	.45	.51	.55	.58	.59	.58	.55	.51	.45	.39	.33	.27	.21	.16	.12	.09	.06	.04	.03	0	0		00000
35	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		00000
36	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		00000
37	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		00000
38	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		00000
39	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		00000
40	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		00000
41	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		00000
42	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		00000
43	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		00000
44	000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000																													

CONCENTRATIONS ABOVE BACKGROUND OF CLAY (MG/L) IN THE CLOUD 2700.00 SECONDS AFTER DUMP

119.00 FT BELOW THE WATER SURFACE

...MULTIPLY DISPLAYED VALUES BY 10.00 (LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)

M N=	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30 31
2	000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000																												
3	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
4	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
5	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
6	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
7	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
8	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
9	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
10	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
11	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
12	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
13	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
14	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
15	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
16	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
17	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
18	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
19	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
20	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
21	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
22	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
23	0000	+	+	+	.01	.01	.01	.01	.01	.01	.01	.01	.01	.01	.01	.01	.01	.01	.01	+	+	+	+	+	+	+	0	0	00000
24	0000	.05	.07	.08	.09	.11	.12	.13	.14	.15	.16	.16	.16	.15	.14	.13	.12	.11	.09	.08	.07	.05	.04	.03	.02	.02	0	0	00000
25	0000	.40	.49	.58	.68	.78	.87	.95	1.0	1.0	1.1	1.1	1.1	1.0	1.0	.95	.87	.78	.68	.58	.49	.40	.32	.25	.19	.15	0	0	00000
26	0000	2.0	2.4	2.9	3.4	3.9	4.3	4.8	5.1	5.4	5.6	5.6	5.6	5.4	5.1	4.8	4.3	3.9	3.4	2.9	2.4	2.0	1.6	1.2	.99	.75	0	0	00000
27	0000	7.3	8.9	11	12	14	16	17	19	20	20	21	20	20	19	17	16	14	12	11	8.9	7.3	5.9	4.6	3.6	2.7	0	0	00000
28	0000	19	23	28	32	37	41	45	49	51	53	54	53	51	49	45	41	37	32	28	23	19	15	12	9.3	7.1	0	0	00000
29	0000	36	43	52	60	69	77	85	91	96	99	100	99	96	91	85	77	69	60	52	43	36	29	23	18	13	0	0	00000
30	0000	48	58	70	81	93	104	115	123	130	134	136	134	130	123	115	104	93	81	70	58	48	39	31	24	18	0	0	00000
31	0000	46	57	67	79	90	101	111	119	126	130	131	130	126	119	111	101	90	79	67	57	46	37	30	23	17	0	0	00000
32	0000	32	39	47	55	62	70	77	83	87	90	91	90	87	83	77	70	62	55	47	39	32	26	21	16	12	0	0	00000
33	0000	16	20	23	27	31	35	38	41	43	45	45	45	43	41	38	35	31	27	23	20	16	13	10	7.9	6.0	0	0	00000
34	0000	5.8	7.0	8.4	10	11	13	14	15	16	16	16	16	16	15	14	13	11	10	8.4	7.0	5.8	4.6	3.6	2.8	2.1	0	0	00000
35	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
36	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
37	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
38	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
39	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
40	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
41	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
42	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
43	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
44	000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000																												

SMALL CLOUDS AT 2700.00 SECONDS ELAPSED TIME FOR CLAY

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID	LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	2940.	300.0	24.29	0.0000E+00	237.6	0.0000E+00	120.0	0.340000E-04
2	2941.	300.0	21.43	0.0000E+00	265.5	0.0000E+00	120.0	0.340000E-04
3	2941.	300.0	29.71	0.0000E+00	314.4	0.0000E+00	120.0	0.340000E-04
4	2941.	300.0	37.68	0.0000E+00	414.1	0.0000E+00	120.0	0.340000E-04
5	2941.	300.0	16.37	0.0000E+00	486.9	0.0000E+00	120.0	0.340000E-04
6	2941.	300.0	7.644	0.0000E+00	531.1	0.0000E+00	120.0	0.340000E-04
7	2941.	300.0	4.425	0.0000E+00	560.3	0.0000E+00	120.0	0.340000E-04
8	2940.	300.0	3.103	0.0000E+00	582.6	0.0000E+00	120.0	0.340000E-04
9	2940.	300.0	2.432	0.0000E+00	601.2	0.0000E+00	120.0	0.340000E-04
10	2940.	300.0	1721.	0.0000E+00	617.3	111.4	8.554	0.316242E-02

SUMMARY OF CLAY DISTRIBUTIONS AFTER 3000.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 1868.4
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 0.00000E+00

SUMMARY OF CLAY DISTRIBUTIONS AFTER 3300.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 1868.4
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 0.00000E+00

SUMMARY OF CLAY DISTRIBUTIONS AFTER 3600.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 1868.4
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 0.00000E+00

CONCENTRATIONS ABOVE BACKGROUND OF CLAY   (MG/L) IN THE CLOUD   3600.00 SECONDS AFTER DUMP

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                  60.00 FT BELOW THE WATER SURFACE
...MULTIPLY DISPLAYED VALUES BY   1.000         (LEGEND... + = .LT. .01   . = .LT. .0001   0 = .LT. .000001)
M N=  2   3   4   5   6   7   8   9  10  11  12  13  14  15  16  17  18  19  20  21  22  23  24  25  26  27  28  29  30  31
 2 000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000
 3 0000   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   00000
 4 0000   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   00000
 5 0000   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   00000
 6 0000   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   00000
 7 0000   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   00000
 8 0000   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   00000
 9 0000   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   00000
10 0000   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   00000
11 0000   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   00000
12 0000   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   00000
13 0000   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   00000
14 0000   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   00000
15 0000   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   00000
16 0000   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   00000
17 0000   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   00000
18 0000   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   00000
19 0000   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   00000
20 0000   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   00000
21 0000   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   00000
22 0000   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   00000
23 0000   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   00000
24 0000   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   00000
25 0000   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   00000
26 0000   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   00000
27 0000   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   00000
28 0000   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   00000
29 0000   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   00000
30 0000   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   00000
31 0000   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   .   .   .0000
32 0000   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +0000
33 0000 .01 .01 .01 .02 .02 .02 .03 .03 .03 .03 .03 .03 .03 .03 .03 .02 .02 .02 .01 .01 .01 .01   +   +   +   +   +   +0000
34 0000 .07 .08 .10 .12 .13 .15 .17 .18 .19 .20 .20 .20 .19 .18 .17 .15 .13 .12 .10 .08 .07 .05 .04 .03 .02 .02 .01 .010000
35 0000 .30 .38 .46 .54 .63 .72 .80 .88 .93 .97 .98 .97 .93 .88 .80 .72 .63 .54 .46 .38 .30 .24 .19 .14 .11 .08 .06 .040000
36 0000 1.0 1.3 1.6 2.0 2.4 2.8 3.3 3.6 3.9 4.1 4.2 4.1 3.9 3.6 3.3 2.8 2.4 2.0 1.6 1.3 1.0 .81 .62 .46 .34 .25 .17 .120000
37 0000 2.8 3.7 4.9 6.4 8.0  10  12  14  15  16  16  16  15  14  12  10 8.0 6.4 4.9 3.7 2.8 2.1 1.5 1.1 .81 .57 .40 .270000
38 0000 5.5 7.6  10  14  19  24  29  35  39  42  43  42  39  35  29  24  19  14  10 7.6 5.5 3.9 2.7 1.9 1.3 .95 .65 .440000
39 0000 6.5 9.1  13  17  23  30  37  45  51  55  56  55  51  45  37  30  23  17  13 9.1 6.5 4.6 3.2 2.2 1.5 1.0 .73 .500000
40 0000 4.5 6.2 8.3  11  14  18  22  26  29  32  32  32  29  26  22  18  14  11 8.3 6.2 4.5 3.2 2.3 1.6 1.1 .82 .57 .390000
41 0000 2.0 2.6 3.4 4.3 5.3 6.4 7.5 8.5 9.4  10  10  10 9.4 8.5 7.5 6.4 5.3 4.3 3.4 2.6 2.0 1.5 1.1 .84 .61 .43 .30 .210000
42 0000 .69 .86 1.0 1.2 1.5 1.7 1.9 2.1 2.3 2.4 2.4 2.4 2.3 2.1 1.9 1.7 1.5 1.2 1.0 .86 .69 .53 .41 .31 .23 .17 .12 .080000
43 0000 .18 .22 .27 .32 .37 .42 .46 .50 .53 .55 .55 .55 .53 .50 .46 .42 .37 .32 .27 .22 .18 .14 .11 .08 .06 .05 .03 .020000
44 0000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000
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CONCENTRATIONS ABOVE BACKGROUND OF CLAY (MG/L) IN THE CLOUD 3600.00 SECONDS AFTER DUMP

119.00 FT BELOW THE WATER SURFACE

...MULTIPLY DISPLAYED VALUES BY 1.000 (LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)

M N=	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30 31
2	OOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOO																												
3	OOOO	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
4	OOOO	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
5	OOOO	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
6	OOOO	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
7	OOOO	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
8	OOOO	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
9	OOOO	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
10	OOOO	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
11	OOOO	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
12	OOOO	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
13	OOOO	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
14	OOOO	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
15	OOOO	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
16	OOOO	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
17	OOOO	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
18	OOOO	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
19	OOOO	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
20	OOOO	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
21	OOOO	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
22	OOOO	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
23	OOOO	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
24	OOOO	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
25	OOOO	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
26	OOOO	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
27	OOOO	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
28	OOOO	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
29	OOOO	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
30	OOOO	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
31	OOOO	.30	.35	.39	.44	.48	.52	.56	.59	.61	.62	.63	.62	.61	.59	.56	.52	.48	.44	.39	.35	.30	.26	.22	.18	.15	.12	.09	.070000
32	OOOO	1.6	1.9	2.1	2.4	2.6	2.9	3.1	3.2	3.3	3.4	3.4	3.4	3.3	3.2	3.1	2.9	2.6	2.4	2.1	1.9	1.6	1.4	1.2	1.0	.83	.67	.53	.420000
33	OOOO	7.3	8.4	10	11	12	13	14	14	15	15	15	15	15	14	14	13	12	11	10	8.4	7.3	6.3	5.3	4.4	3.6	2.9	2.3	1.80000
34	OOOO	26	29	33	37	41	44	47	50	51	53	53	53	51	50	47	44	41	37	33	29	26	22	18	15	13	10	8.1	6.40000
35	OOOO	70	80	91	102	112	121	129	136	141	144	145	144	141	136	129	121	112	102	91	80	70	60	51	42	35	28	22	180000
36	OOOO	152	174	197	220	242	263	280	295	306	313	315	313	306	295	280	263	242	220	197	174	152	130	110	91	75	61	48	380000
37	OOOO	260	299	339	378	416	451	482	507	526	538	542	538	526	507	482	451	416	378	339	299	260	223	189	157	129	104	83	650000
38	OOOO	353	406	460	514	566	614	656	691	717	734	739	734	717	691	656	614	566	514	460	406	353	303	256	213	175	141	113	890000
39	OOOO	380	437	495	553	608	660	706	743	772	789	795	789	772	743	706	660	608	553	495	437	380	325	275	229	188	152	121	950000
40	OOOO	323	371	420	469	516	560	598	630	654	669	674	669	654	630	598	560	516	469	420	371	323	277	234	195	160	129	103	810000
41	OOOO	217	249	282	315	347	376	401	423	438	448	451	448	438	423	401	376	347	315	282	249	217	186	157	131	107	87	69	540000
42	OOOO	115	133	150	168	184	200	213	225	233	238	240	238	233	225	213	200	184	168	150	133	115	99	84	70	57	46	37	290000
43	OOOO	49	56	63	71	78	84	90	95	98	100	101	100	98	95	90	84	78	71	63	56	49	42	35	29	24	19	16	120000
44	OOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOO																												

SMALL CLOUDS AT 3600.00 SECONDS ELAPSED TIME FOR CLAY

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID	LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	3781.	300.0	24.29	0.0000E+00	322.9	0.0000E+00	120.0	0.340000E-04
2	3781.	300.0	21.43	0.0000E+00	353.8	0.0000E+00	120.0	0.340000E-04
3	3782.	300.0	29.71	0.0000E+00	407.5	0.0000E+00	120.0	0.340000E-04
4	3782.	300.0	37.68	0.0000E+00	515.6	0.0000E+00	120.0	0.340000E-04
5	3782.	300.0	16.37	0.0000E+00	593.8	0.0000E+00	120.0	0.340000E-04
6	3782.	300.0	7.644	0.0000E+00	641.0	0.0000E+00	120.0	0.340000E-04
7	3781.	300.0	4.425	0.0000E+00	672.2	0.0000E+00	120.0	0.340000E-04
8	3781.	300.0	3.103	0.0000E+00	695.9	0.0000E+00	120.0	0.340000E-04
9	3781.	300.0	2.432	0.0000E+00	715.6	0.0000E+00	120.0	0.340000E-04
10	3781.	300.0	1721.	0.0000E+00	732.7	110.3	9.716	0.165815E-02

BEGIN LONG TERM SIMULATION OF FATE OF FLUID

SUMMARY OF FLUID DISTRIBUTIONS AFTER 300.00 SEC

TOTAL FLUID FRACTION VOLUME FROM DISPOSAL (CU FT) = 5066.6

SMALL CLOUDS AT 300.00 SECONDS ELAPSED TIME FOR FLUID

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID	LOCATION OF CLOUD CENTROID DISTANCE FROM LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	697.8	300.0	5067.	0.0000E+00	344.8	90.14	29.86	0.000000E+00

SUMMARY OF FLUID DISTRIBUTIONS AFTER 600.00 SEC

TOTAL FLUID FRACTION VOLUME FROM DISPOSAL (CU FT) = 5066.6

SMALL CLOUDS AT 600.00 SECONDS ELAPSED TIME FOR FLUID

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID	LOCATION OF CLOUD CENTROID DISTANCE FROM LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	978.0	300.0	5067.	0.0000E+00	375.8	62.76	57.24	0.000000E+00

SUMMARY OF FLUID DISTRIBUTIONS AFTER 900.00 SEC

TOTAL FLUID FRACTION VOLUME FROM DISPOSAL (CU FT) = 5066.6

CONCENTRATIONS ABOVE BACKGROUND OF FLUID (VOLUMETRIC RATIO OF DUMP FLUID TO AMBIENT WATER) IN THE CLOUD 900.00 SECONDS AFTER DUMP

60.00 FT BELOW THE WATER SURFACE

...MULTIPLY DISPLAYED VALUES BY 0.1000E-03 (LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)

M N=	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31
2	000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000																													
3	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
4	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
5	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
6	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
7	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
8	0000	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0	0	0	00000	
9	0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	0	0	0	0	0	0	00000	
10	0000	+	+	.01	.01	.02	.03	.04	.05	.05	.06	.06	.06	.05	.05	.04	.03	.02	.01	.01	+	+	0	0	0	0	0	0	00000	
11	0000	.06	.09	.14	.20	.27	.36	.44	.52	.59	.63	.65	.63	.59	.52	.44	.36	.27	.20	.14	.09	.06	0	0	0	0	0	0	00000	
12	0000	.29	.46	.69	.98	1.3	1.7	2.1	2.5	2.8	3.0	3.1	3.0	2.8	2.5	2.1	1.7	1.3	.98	.69	.46	.29	0	0	0	0	0	0	00000	
13	0000	.67	1.0	1.5	2.2	3.0	3.9	4.8	5.7	6.4	6.9	7.1	6.9	6.4	5.7	4.8	3.9	3.0	2.2	1.5	1.0	.67	0	0	0	0	0	0	00000	
14	0000	.71	1.1	1.6	2.3	3.2	4.2	5.1	6.1	6.9	7.4	7.5	7.4	6.9	6.1	5.1	4.2	3.2	2.3	1.6	1.1	.71	0	0	0	0	0	0	00000	
15	0000	.35	.56	.83	1.1	1.6	2.1	2.6	3.0	3.4	3.7	3.7	3.7	3.4	3.0	2.6	2.1	1.6	1.1	.83	.56	.35	0	0	0	0	0	0	00000	
16	0000	.08	.13	.19	.28	.38	.49	.61	.72	.81	.87	.89	.87	.81	.72	.61	.49	.38	.28	.19	.13	.08	0	0	0	0	0	0	00000	
17	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
18	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
19	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
20	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
21	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
22	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
23	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
24	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
25	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
26	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
27	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
28	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
29	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
30	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
31	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
32	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
33	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
34	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
35	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
36	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
37	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
38	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
39	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
40	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
41	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
42	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
43	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
44	000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000																													

CONCENTRATIONS ABOVE BACKGROUND OF FLUID (VOLUMETRIC RATIO OF DUMP FLUID TO AMBIENT WATER) IN THE CLOUD 900.00 SECONDS AFTER DUMP

119.00 FT BELOW THE WATER SURFACE

...MULTIPLY DISPLAYED VALUES BY 0.1000E-03 (LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)

M N=	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30 31
2	000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000																												
3	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
4	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
5	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
6	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
7	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
8	0000	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0	0	0	00000
9	0000	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	0	0	0	0	0	0	00000
10	0000	+	+	+	+	+	+	+	.01	.01	.01	.01	.01	.01	.01	+	+	+	+	+	+	+	0	0	0	0	0	0	00000
11	0000	.01	.02	.03	.04	.05	.07	.09	.11	.12	.13	.13	.13	.12	.11	.09	.07	.05	.04	.03	.02	.01	0	0	0	0	0	0	00000
12	0000	.06	.09	.14	.20	.28	.36	.45	.53	.60	.64	.66	.64	.60	.53	.45	.36	.28	.20	.14	.09	.06	0	0	0	0	0	0	00000
13	0000	.14	.22	.33	.47	.64	.83	1.0	1.2	1.3	1.4	1.5	1.4	1.3	1.2	1.0	.83	.64	.47	.33	.22	.14	0	0	0	0	0	0	00000
14	0000	.15	.23	.35	.50	.68	.88	1.0	1.2	1.4	1.5	1.5	1.5	1.4	1.2	1.0	.88	.68	.50	.35	.23	.15	0	0	0	0	0	0	00000
15	0000	.07	.11	.17	.25	.34	.44	.54	.64	.72	.78	.79	.78	.72	.64	.54	.44	.34	.25	.17	.11	.07	0	0	0	0	0	0	00000
16	0000	.01	.02	.04	.05	.08	.10	.12	.15	.17	.18	.18	.18	.17	.15	.12	.10	.08	.05	.04	.02	.01	0	0	0	0	0	0	00000
17	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
18	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
19	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
20	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
21	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
22	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
23	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
24	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
25	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
26	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
27	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
28	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
29	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
30	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
31	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
32	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
33	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
34	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
35	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
36	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
37	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
38	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
39	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
40	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
41	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
42	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
43	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
44	000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000																												

CONCENTRATIONS ABOVE BACKGROUND OF FLUID   (VOLUMETRIC RATIO OF DUMP FLUID TO AMBIENT WATER) IN THE CLOUD   900.00 SECONDS AFTER DUMP

THESE CONCENTRATIONS ARE THE MAXIMUM OCCURING IN THE WATER COLUMN AT THIS TIME

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 ...MULTIPLY DISPLAYED VALUES BY  0.1000E-02     (LEGEND... + = .LT. .01   . = .LT. .0001   0 = .LT. .000001)
 M N=  2   3   4   5   6   7   8   9  10  11  12  13  14  15  16  17  18  19  20  21  22  23  24  25  26  27  28  29  30  31
  2 OOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOO
  3 OOOO   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   OOOOO
  4 OOOO   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   OOOOO
  5 OOOO   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   OOOOO
  6 OOOO   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   OOOOO
  7 OOOO   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   OOOOO
  8 OOOO   0   .   .   .   .   .   .   .   .   .   .   .   .   .   .   .   .   .   .   .   .   0   0   0   0   0   0   0   OOOOO
  9 OOOO   .   .   .   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   .   .   .   0   0   0   0   0   0   OOOOO
 10 OOOO   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   0   0   0   0   0   0   OOOOO
 11 OOOO   + .01 .02 .02 .03 .05 .06 .07 .08 .09 .09 .09 .08 .07 .06 .05 .03 .02 .02 .01   +   0   0   0   0   0   0   OOOOO
 12 OOOO .04 .06 .09 .14 .19 .24 .30 .36 .40 .43 .44 .43 .40 .36 .30 .24 .19 .14 .09 .06 .04   0   0   0   0   0   0   OOOOO
 13 OOOO .09 .14 .22 .31 .43 .55 .69 .81 .91 .98 1.0 .98 .91 .81 .69 .55 .43 .31 .22 .14 .09   0   0   0   0   0   0   OOOOO
 14 OOOO .10 .15 .23 .33 .45 .59 .73 .86 .97 1.0 1.0 1.0 .97 .86 .73 .59 .45 .33 .23 .15 .10   0   0   0   0   0   0   OOOOO
 15 OOOO .05 .07 .11 .16 .22 .29 .36 .43 .48 .52 .53 .52 .48 .43 .36 .29 .22 .16 .11 .07 .05   0   0   0   0   0   0   OOOOO
 16 OOOO .01 .01 .02 .03 .05 .07 .08 .10 .11 .12 .12 .12 .11 .10 .08 .07 .05 .03 .02 .01 .01   0   0   0   0   0   0   OOOOO
 17 OOOO   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   OOOOO
 18 OOOO   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   OOOOO
 19 OOOO   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   OOOOO
 20 OOOO   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   OOOOO
 21 OOOO   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   OOOOO
 22 OOOO   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   OOOOO
 23 OOOO   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   OOOOO
 24 OOOO   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   OOOOO
 25 OOOO   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   OOOOO
 26 OOOO   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   OOOOO
 27 OOOO   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   OOOOO
 28 OOOO   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   OOOOO
 29 OOOO   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   OOOOO
 30 OOOO   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   OOOOO
 31 OOOO   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   OOOOO
 32 OOOO   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   OOOOO
 33 OOOO   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   OOOOO
 34 OOOO   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   OOOOO
 35 OOOO   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   OOOOO
 36 OOOO   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   OOOOO
 37 OOOO   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   OOOOO
 38 OOOO   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   OOOOO
 39 OOOO   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   OOOOO
 40 OOOO   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   OOOOO
 41 OOOO   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   OOOOO
 42 OOOO   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   OOOOO
 43 OOOO   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   OOOOO
 44 OOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOO
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SMALL CLOUDS AT 900.00 SECONDS ELAPSED TIME FOR FLUID

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID	LOCATION OF CLOUD CENTROID DISTANCE FROM LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	1258.	300.0	5067.	0.0000E+00	407.8	35.37	84.63	0.000000E+00

SUMMARY OF FLUID DISTRIBUTIONS AFTER 1200.00 SEC

TOTAL FLUID FRACTION VOLUME FROM DISPOSAL (CU FT) = 5066.6

SMALL CLOUDS AT 1200.00 SECONDS ELAPSED TIME FOR FLUID

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID	LOCATION OF CLOUD CENTROID DISTANCE FROM LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	1539.	300.0	5067.	0.0000E+00	440.7	7.986	112.0	0.000000E+00

SUMMARY OF FLUID DISTRIBUTIONS AFTER 1500.00 SEC

TOTAL FLUID FRACTION VOLUME FROM DISPOSAL (CU FT) = 5066.6

SMALL CLOUDS AT 1500.00 SECONDS ELAPSED TIME FOR FLUID

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID	LOCATION OF CLOUD CENTROID DISTANCE FROM LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	1819.	300.0	5067.	0.0000E+00	474.4	0.0000E+00	120.0	0.000000E+00

SUMMARY OF FLUID DISTRIBUTIONS AFTER 1800.00 SEC

TOTAL FLUID FRACTION VOLUME FROM DISPOSAL (CU FT) = 5066.6

CONCENTRATIONS ABOVE BACKGROUND OF FLUID (VOLUMETRIC RATIO OF DUMP FLUID TO AMBIENT WATER) IN THE CLOUD 1800.00 SECONDS AFTER DUMP

60.00 FT BELOW THE WATER SURFACE

...MULTIPLY DISPLAYED VALUES BY 0.1000E-03 (LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)

M N=	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	0	0	0	0	0	0
17	+	+	+	+	+	+	+	+	.01	.01	.01	.01	.01	.01	.01	+	+	+	+	+	+	+	+	+	0	0	0	0	0	0
18	.02	.03	.04	.05	.06	.07	.08	.09	.10	.10	.10	.10	.10	.10	.09	.08	.07	.06	.05	.04	.03	.02	.01	.01	0	0	0	0	0	0
19	.13	.17	.22	.28	.34	.40	.46	.51	.55	.58	.59	.58	.55	.51	.46	.40	.34	.28	.22	.17	.13	.09	.06	0	0	0	0	0	0	0
20	.43	.58	.75	.94	1.1	1.3	1.5	1.7	1.8	1.9	1.9	1.9	1.8	1.7	1.5	1.3	1.1	.94	.75	.58	.43	.31	.22	0	0	0	0	0	0	0
21	.90	1.2	1.5	1.9	2.3	2.8	3.2	3.5	3.8	4.0	4.1	4.0	3.8	3.5	3.2	2.8	2.3	1.9	1.5	1.2	.90	.65	.46	0	0	0	0	0	0	0
22	1.1	1.5	1.9	2.4	3.0	3.5	4.0	4.5	4.8	5.1	5.2	5.1	4.8	4.5	4.0	3.5	3.0	2.4	1.9	1.5	1.1	.83	.58	0	0	0	0	0	0	0
23	.89	1.1	1.5	1.9	2.3	2.7	3.1	3.5	3.8	4.0	4.0	4.0	3.8	3.5	3.1	2.7	2.3	1.9	1.5	1.1	.89	.64	.45	0	0	0	0	0	0	0
24	.42	.57	.74	.92	1.1	1.3	1.5	1.7	1.8	1.9	1.9	1.9	1.8	1.7	1.5	1.3	1.1	.92	.74	.57	.42	.31	.22	0	0	0	0	0	0	0
25	.12	.16	.21	.27	.33	.39	.45	.50	.54	.56	.57	.56	.54	.50	.45	.39	.33	.27	.21	.16	.12	.09	.06	0	0	0	0	0	0	0
26	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
27	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
28	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
29	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
30	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
31	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
32	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
33	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
34	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
35	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
36	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
37	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
38	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
39	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
40	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
41	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
42	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
43	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
44	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0

CONCENTRATIONS ABOVE BACKGROUND OF FLUID (VOLUMETRIC RATIO OF DUMP FLUID TO AMBIENT WATER) IN THE CLOUD 1800.00 SECONDS AFTER DUMP

119.00 FT BELOW THE WATER SURFACE

...MULTIPLY DISPLAYED VALUES BY 0.1000E-04 (LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)

M N=	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	0	0	0	0	0	0	0
17	+	+	+	+	.01	.01	.01	.01	.01	.01	.01	.01	.01	.01	.01	.01	.01	.01	+	+	+	+	+	+	0	0	0	0	0	0
18	.03	.04	.05	.07	.09	.10	.12	.13	.14	.15	.15	.15	.14	.13	.12	.10	.09	.07	.05	.04	.03	.02	.01	0	0	0	0	0	0	0
19	.18	.25	.32	.40	.49	.58	.67	.74	.80	.84	.85	.84	.80	.74	.67	.58	.49	.40	.32	.25	.18	.13	.09	0	0	0	0	0	0	0
20	.63	.84	1.0	1.3	1.6	1.9	2.2	2.5	2.7	2.8	2.8	2.8	2.7	2.5	2.2	1.9	1.6	1.3	1.0	.84	.63	.45	.32	0	0	0	0	0	0	0
21	1.3	1.7	2.2	2.8	3.4	4.0	4.6	5.1	5.5	5.8	5.9	5.8	5.5	5.1	4.6	4.0	3.4	2.8	2.2	1.7	1.3	.94	.66	0	0	0	0	0	0	0
22	1.6	2.2	2.8	3.5	4.3	5.1	5.9	6.5	7.0	7.4	7.5	7.4	7.0	6.5	5.9	5.1	4.3	3.5	2.8	2.2	1.6	1.2	.84	0	0	0	0	0	0	0
23	1.2	1.7	2.2	2.7	3.4	4.0	4.6	5.1	5.5	5.7	5.8	5.7	5.5	5.1	4.6	4.0	3.4	2.7	2.2	1.7	1.2	.93	.66	0	0	0	0	0	0	0
24	.61	.82	1.0	1.3	1.6	1.9	2.2	2.4	2.6	2.7	2.8	2.7	2.6	2.4	2.2	1.9	1.6	1.3	1.0	.82	.61	.45	.31	0	0	0	0	0	0	0
25	.18	.24	.31	.39	.48	.57	.65	.72	.78	.82	.83	.82	.78	.72	.65	.57	.48	.39	.31	.24	.18	.13	.09	0	0	0	0	0	0	0
26	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
27	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
28	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
29	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
30	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
31	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
32	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
33	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
34	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
35	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
36	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
37	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
38	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
39	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
40	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
41	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
42	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
43	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
44	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0

CONCENTRATIONS ABOVE BACKGROUND OF FLUID (VOLUMETRIC RATIO OF DUMP FLUID TO AMBIENT WATER) IN THE CLOUD 1800.00 SECONDS AFTER DUMP

THESE CONCENTRATIONS ARE THE MAXIMUM OCCURING IN THE WATER COLUMN AT THIS TIME

...MULTIPLY DISPLAYED VALUES BY 0.1000E-03 (LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)

M N=	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30 31
2	000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000																												
3	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
4	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
5	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
6	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
7	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
8	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
9	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
10	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
11	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
12	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
13	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
14	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
15	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
16	0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	0	0	0	0	00000
17	0000	+	+	+	+	+	+	+	.01	.01	.01	.01	.01	.01	.01	+	+	+	+	+	+	+	+	+	0	0	0	0	00000
18	0000	.02	.03	.04	.05	.06	.07	.08	.09	.10	.10	.10	.10	.10	.09	.08	.07	.06	.05	.04	.03	.02	.01	.01	0	0	0	0	00000
19	0000	.13	.17	.22	.28	.34	.40	.46	.51	.55	.58	.59	.58	.55	.51	.46	.40	.34	.28	.22	.17	.13	.09	.06	0	0	0	0	00000
20	0000	.43	.58	.75	.94	1.1	1.3	1.5	1.7	1.8	1.9	1.9	1.9	1.8	1.7	1.5	1.3	1.1	.94	.75	.58	.43	.31	.22	0	0	0	0	00000
21	0000	.90	1.2	1.5	1.9	2.3	2.8	3.2	3.5	3.8	4.0	4.1	4.0	3.8	3.5	3.2	2.8	2.3	1.9	1.5	1.2	.90	.65	.46	0	0	0	0	00000
22	0000	1.1	1.5	1.9	2.4	3.0	3.5	4.0	4.5	4.8	5.1	5.2	5.1	4.8	4.5	4.0	3.5	3.0	2.4	1.9	1.5	1.1	.83	.58	0	0	0	0	00000
23	0000	.89	1.1	1.5	1.9	2.3	2.7	3.1	3.5	3.8	4.0	4.0	4.0	3.8	3.5	3.1	2.7	2.3	1.9	1.5	1.1	.89	.64	.45	0	0	0	0	00000
24	0000	.42	.57	.74	.92	1.1	1.3	1.5	1.7	1.8	1.9	1.9	1.9	1.8	1.7	1.5	1.3	1.1	.92	.74	.57	.42	.31	.22	0	0	0	0	00000
25	0000	.12	.16	.21	.27	.33	.39	.45	.50	.54	.56	.57	.56	.54	.50	.45	.39	.33	.27	.21	.16	.12	.09	.06	0	0	0	0	00000
26	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
27	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
28	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
29	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
30	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
31	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
32	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
33	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
34	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
35	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
36	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
37	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
38	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
39	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
40	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
41	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
42	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
43	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
44	000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000																												

SMALL CLOUDS AT 1800.00 SECONDS ELAPSED TIME FOR FLUID

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID	LOCATION OF CLOUD CENTROID DISTANCE FROM LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	2099.	300.0	5067.	0.0000E+00	508.9	0.0000E+00	120.0	0.000000E+00

SUMMARY OF FLUID DISTRIBUTIONS AFTER 2100.00 SEC

TOTAL FLUID FRACTION VOLUME FROM DISPOSAL (CU FT) = 5066.6

SMALL CLOUDS AT 2100.00 SECONDS ELAPSED TIME FOR FLUID

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID	LOCATION OF CLOUD CENTROID DISTANCE FROM LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	2379.	300.0	5067.	0.0000E+00	544.2	0.0000E+00	120.0	0.000000E+00

SUMMARY OF FLUID DISTRIBUTIONS AFTER 2400.00 SEC

TOTAL FLUID FRACTION VOLUME FROM DISPOSAL (CU FT) = 5066.6

SMALL CLOUDS AT 2400.00 SECONDS ELAPSED TIME FOR FLUID

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID	LOCATION OF CLOUD CENTROID DISTANCE FROM LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	2660.	300.0	5067.	0.0000E+00	580.4	0.0000E+00	120.0	0.000000E+00

SUMMARY OF FLUID DISTRIBUTIONS AFTER 2700.00 SEC

TOTAL FLUID FRACTION VOLUME FROM DISPOSAL (CU FT) = 5066.6

CONCENTRATIONS ABOVE BACKGROUND OF FLUID (VOLUMETRIC RATIO OF DUMP FLUID TO AMBIENT WATER) IN THE CLOUD 2700.00 SECONDS AFTER DUMP

60.00 FT BELOW THE WATER SURFACE

...MULTIPLY DISPLAYED VALUES BY 0.1000E-03 (LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)

M N=	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31
2	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O
3	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
18	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
19	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
20	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
21	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
22	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
23	O	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	0	0	0	0
24	O	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	0	0	0	0
25	O	.01	.01	.01	.01	.02	.02	.02	.02	.02	.02	.02	.02	.02	.02	.02	.02	.02	.01	.01	.01	.01	+	+	+	+	0	0	0	0
26	O	.05	.06	.07	.08	.10	.11	.12	.13	.13	.14	.14	.14	.13	.13	.12	.11	.10	.08	.07	.06	.05	.04	.03	.02	.01	0	0	0	0
27	O	.18	.22	.27	.31	.36	.40	.44	.48	.50	.52	.52	.52	.50	.48	.44	.40	.36	.31	.27	.22	.18	.15	.11	.09	.06	0	0	0	0
28	O	.48	.59	.70	.82	.94	1.0	1.1	1.2	1.3	1.3	1.3	1.3	1.3	1.2	1.1	1.0	.94	.82	.70	.59	.48	.39	.31	.24	.18	0	0	0	0
29	O	.91	1.1	1.3	1.5	1.7	1.9	2.1	2.3	2.4	2.5	2.5	2.5	2.4	2.3	2.1	1.9	1.7	1.5	1.3	1.1	.91	.73	.58	.44	.34	0	0	0	0
30	O	1.2	1.4	1.7	2.0	2.3	2.6	2.9	3.1	3.3	3.4	3.4	3.4	3.3	3.1	2.9	2.6	2.3	2.0	1.7	1.4	1.2	.99	.78	.60	.45	0	0	0	0
31	O	1.1	1.4	1.7	2.0	2.2	2.5	2.8	3.0	3.1	3.2	3.3	3.2	3.1	3.0	2.8	2.5	2.2	2.0	1.7	1.4	1.1	.95	.75	.58	.44	0	0	0	0
32	O	.82	1.0	1.1	1.3	1.5	1.7	1.9	2.1	2.2	2.2	2.3	2.2	2.2	2.1	1.9	1.7	1.5	1.3	1.1	1.0	.82	.66	.52	.40	.30	0	0	0	0
33	O	.41	.50	.59	.69	.79	.89	.98	1.0	1.1	1.1	1.1	1.1	1.1	1.0	.98	.89	.79	.69	.59	.50	.41	.33	.26	.20	.15	0	0	0	0
34	O	.14	.18	.21	.25	.28	.32	.35	.37	.39	.41	.41	.41	.39	.37	.35	.32	.28	.25	.21	.18	.14	.11	.09	.07	.05	0	0	0	0
35	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
36	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
37	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
38	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
39	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
40	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
41	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
42	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
43	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
44	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O

CONCENTRATIONS ABOVE BACKGROUND OF FLUID (VOLUMETRIC RATIO OF DUMP FLUID TO AMBIENT WATER) IN THE CLOUD 2700.00 SECONDS AFTER DUMP

119.00 FT BELOW THE WATER SURFACE

...MULTIPLY DISPLAYED VALUES BY 0.1000E-04 (LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)

M N=	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31
2	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O
3	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
4	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
5	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
6	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
7	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
8	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
9	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
10	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
11	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
12	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
13	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
14	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
15	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
16	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
17	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
18	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
19	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
20	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
21	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
22	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
23	O	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	0	0	0	O
24	O	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	0	0	0	O
25	O	.01	.01	.02	.02	.02	.03	.03	.03	.04	.04	.04	.04	.04	.03	.03	.03	.02	.02	.02	.01	.01	.01	+	+	+	0	0	0	O
26	O	.07	.09	.10	.12	.14	.16	.17	.19	.20	.20	.21	.20	.20	.19	.17	.16	.14	.12	.10	.09	.07	.06	.04	.03	.02	0	0	0	O
27	O	.27	.33	.39	.45	.52	.58	.64	.69	.73	.75	.76	.75	.73	.69	.64	.58	.52	.45	.39	.33	.27	.21	.17	.13	.10	0	0	0	O
28	O	.70	.85	1.0	1.1	1.3	1.5	1.6	1.8	1.9	1.9	1.9	1.9	1.9	1.8	1.6	1.5	1.3	1.1	1.0	.85	.70	.56	.44	.34	.26	0	0	0	O
29	O	1.3	1.6	1.9	2.2	2.5	2.8	3.1	3.3	3.5	3.6	3.7	3.6	3.5	3.3	3.1	2.8	2.5	2.2	1.9	1.6	1.3	1.0	.84	.64	.49	0	0	0	O
30	O	1.7	2.1	2.5	3.0	3.4	3.8	4.2	4.5	4.7	4.9	4.9	4.9	4.7	4.5	4.2	3.8	3.4	3.0	2.5	2.1	1.7	1.4	1.1	.87	.66	0	0	0	O
31	O	1.7	2.0	2.4	2.9	3.3	3.7	4.0	4.3	4.6	4.7	4.8	4.7	4.6	4.3	4.0	3.7	3.3	2.9	2.4	2.0	1.7	1.3	1.0	.84	.63	0	0	0	O
32	O	1.1	1.4	1.7	2.0	2.3	2.5	2.8	3.0	3.2	3.3	3.3	3.3	3.2	3.0	2.8	2.5	2.3	2.0	1.7	1.4	1.1	.96	.75	.58	.44	0	0	0	O
33	O	.59	.72	.86	1.0	1.1	1.2	1.4	1.5	1.6	1.6	1.6	1.6	1.6	1.5	1.4	1.2	1.1	1.0	.86	.72	.59	.48	.37	.29	.22	0	0	0	O
34	O	.21	.26	.31	.36	.41	.46	.51	.54	.57	.59	.60	.59	.57	.54	.51	.46	.41	.36	.31	.26	.21	.17	.13	.10	.07	0	0	0	O
35	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
36	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
37	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
38	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
39	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
40	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
41	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
42	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
43	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O
44	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O	O

CONCENTRATIONS ABOVE BACKGROUND OF FLUID (VOLUMETRIC RATIO OF DUMP FLUID TO AMBIENT WATER) IN THE CLOUD 2700.00 SECONDS AFTER DUMP

THESE CONCENTRATIONS ARE THE MAXIMUM OCCURING IN THE WATER COLUMN AT THIS TIME

...MULTIPLY DISPLAYED VALUES BY 0.1000E-03 (LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)

M	N= 2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31
2	000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000																													
3	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
4	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
5	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
6	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
7	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
8	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
9	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
10	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
11	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
12	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
13	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
14	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
15	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
16	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
17	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
18	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
19	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
20	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
21	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
22	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
23	0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	0	0	00000	
24	0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	0	0	00000	
25	0000	.01	.01	.01	.01	.02	.02	.02	.02	.02	.02	.02	.02	.02	.02	.02	.02	.02	.01	.01	.01	.01	+	+	+	+	0	0	00000	
26	0000	.05	.06	.07	.08	.10	.11	.12	.13	.13	.14	.14	.14	.13	.13	.12	.11	.10	.08	.07	.06	.05	.04	.03	.02	.01	0	0	00000	
27	0000	.18	.22	.27	.31	.36	.40	.44	.48	.50	.52	.52	.52	.50	.48	.44	.40	.36	.31	.27	.22	.18	.15	.11	.09	.06	0	0	00000	
28	0000	.48	.59	.70	.82	.94	1.0	1.1	1.2	1.3	1.3	1.3	1.3	1.3	1.2	1.1	1.0	.94	.82	.70	.59	.48	.39	.31	.24	.18	0	0	00000	
29	0000	.91	1.1	1.3	1.5	1.7	1.9	2.1	2.3	2.4	2.5	2.5	2.5	2.4	2.3	2.1	1.9	1.7	1.5	1.3	1.1	.91	.73	.58	.44	.34	0	0	00000	
30	0000	1.2	1.4	1.7	2.0	2.3	2.6	2.9	3.1	3.3	3.4	3.4	3.4	3.3	3.1	2.9	2.6	2.3	2.0	1.7	1.4	1.2	.99	.78	.60	.45	0	0	00000	
31	0000	1.1	1.4	1.7	2.0	2.2	2.5	2.8	3.0	3.1	3.2	3.3	3.2	3.1	3.0	2.8	2.5	2.2	2.0	1.7	1.4	1.1	.95	.75	.58	.44	0	0	00000	
32	0000	.82	1.0	1.1	1.3	1.5	1.7	1.9	2.1	2.2	2.2	2.3	2.2	2.2	2.1	1.9	1.7	1.5	1.3	1.1	1.0	.82	.66	.52	.40	.30	0	0	00000	
33	0000	.41	.50	.59	.69	.79	.89	.98	1.0	1.1	1.1	1.1	1.1	1.1	1.0	.98	.89	.79	.69	.59	.50	.41	.33	.26	.20	.15	0	0	00000	
34	0000	.14	.18	.21	.25	.28	.32	.35	.37	.39	.41	.41	.41	.39	.37	.35	.32	.28	.25	.21	.18	.14	.11	.09	.07	.05	0	0	00000	
35	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
36	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
37	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
38	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
39	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
40	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
41	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
42	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
43	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000	
44	000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000																													

SMALL CLOUDS AT 2700.00 SECONDS ELAPSED TIME FOR FLUID

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID	LOCATION OF CLOUD CENTROID DISTANCE FROM LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	2940.	300.0	5067.	0.0000E+00	617.3	0.0000E+00	120.0	0.000000E+00

SUMMARY OF FLUID DISTRIBUTIONS AFTER 3000.00 SEC

TOTAL FLUID FRACTION VOLUME FROM DISPOSAL (CU FT) = 5066.6

SMALL CLOUDS AT 3000.00 SECONDS ELAPSED TIME FOR FLUID

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID	LOCATION OF CLOUD CENTROID DISTANCE FROM LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	3220.	300.0	5067.	0.0000E+00	655.1	0.0000E+00	120.0	0.000000E+00

SUMMARY OF FLUID DISTRIBUTIONS AFTER 3300.00 SEC

TOTAL FLUID FRACTION VOLUME FROM DISPOSAL (CU FT) = 5066.6

SMALL CLOUDS AT 3300.00 SECONDS ELAPSED TIME FOR FLUID

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID	LOCATION OF CLOUD CENTROID DISTANCE FROM LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	3500.	300.0	5067.	0.0000E+00	693.5	0.0000E+00	120.0	0.000000E+00

SUMMARY OF FLUID DISTRIBUTIONS AFTER 3600.00 SEC

TOTAL FLUID FRACTION VOLUME FROM DISPOSAL (CU FT) = 5066.6

CONCENTRATIONS ABOVE BACKGROUND OF FLUID (VOLUMETRIC RATIO OF DUMP FLUID TO AMBIENT WATER) IN THE CLOUD 3600.00 SECONDS AFTER DUMP

60.00 FT BELOW THE WATER SURFACE

...MULTIPLY DISPLAYED VALUES BY 0.1000E-03 (LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)

M N=	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
18	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
19	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
20	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
21	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
22	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
23	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
24	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
25	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
26	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
27	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
28	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
29	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
30	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
31	0	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+
32	0	+	+	+	+	+	+	+	.01	.01	.01	.01	.01	.01	.01	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+
33	0	.02	.02	.03	.03	.03	.04	.04	.04	.04	.04	.04	.04	.04	.04	.04	.04	.03	.03	.03	.02	.02	.02	.01	.01	.01	+	+	+	+
34	0	.08	.09	.10	.11	.12	.14	.14	.15	.16	.16	.16	.16	.16	.15	.14	.14	.12	.11	.10	.09	.08	.06	.05	.04	.04	.03	.02	.02	0
35	0	.22	.25	.28	.32	.35	.38	.41	.43	.44	.45	.46	.45	.44	.43	.41	.38	.35	.32	.28	.25	.22	.19	.16	.13	.10	.08	.07	.05	0
36	0	.48	.55	.62	.69	.76	.83	.88	.93	.97	.99	.99	.99	.97	.93	.88	.83	.76	.69	.62	.55	.48	.41	.34	.29	.23	.19	.15	.12	0
37	0	.82	.94	1.0	1.1	1.3	1.4	1.5	1.6	1.6	1.7	1.7	1.7	1.6	1.6	1.5	1.4	1.3	1.1	1.0	.94	.82	.70	.59	.49	.40	.33	.26	.20	0
38	0	1.1	1.2	1.4	1.6	1.7	1.9	2.0	2.1	2.2	2.3	2.3	2.3	2.2	2.1	2.0	1.9	1.7	1.6	1.4	1.2	1.1	.96	.81	.67	.55	.44	.35	.28	0
39	0	1.2	1.3	1.5	1.7	1.9	2.0	2.2	2.3	2.4	2.4	2.4	2.4	2.4	2.3	2.2	2.0	1.9	1.7	1.5	1.3	1.2	1.0	.87	.72	.59	.48	.38	.30	0
40	0	1.0	1.1	1.3	1.4	1.6	1.7	1.8	1.9	2.0	2.1	2.1	2.1	2.0	1.9	1.8	1.7	1.6	1.4	1.3	1.1	1.0	.87	.74	.61	.50	.40	.32	.25	0
41	0	.68	.79	.89	.99	1.0	1.1	1.2	1.3	1.3	1.4	1.4	1.4	1.3	1.3	1.2	1.1	1.0	.99	.89	.79	.68	.58	.49	.41	.34	.27	.21	.17	0
42	0	.36	.42	.47	.53	.58	.63	.67	.71	.73	.75	.76	.75	.73	.71	.67	.63	.58	.53	.47	.42	.36	.31	.26	.22	.18	.14	.11	.09	0
43	0	.15	.17	.20	.22	.24	.26	.28	.29	.31	.31	.32	.31	.31	.29	.28	.26	.24	.22	.20	.17	.15	.13	.11	.09	.07	.06	.04	.03	0
44	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0

CONCENTRATIONS ABOVE BACKGROUND OF FLUID (VOLUMETRIC RATIO OF DUMP FLUID TO AMBIENT WATER) IN THE CLOUD 3600.00 SECONDS AFTER DUMP

119.00 FT BELOW THE WATER SURFACE

...MULTIPLY DISPLAYED VALUES BY 0.1000E-04 (LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)

M N=	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
18	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
19	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
20	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
21	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
22	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
23	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
24	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
25	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
26	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
27	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
28	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
29	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
30	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
31	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+
32	+	+	.01	.01	.01	.01	.01	.01	.01	.01	.01	.01	.01	.01	.01	.01	.01	.01	.01	.01	+	+	+	+	+	+	+	+	+	+
33	.03	.03	.04	.04	.05	.05	.06	.06	.06	.06	.07	.06	.06	.06	.06	.05	.05	.04	.04	.03	.03	.02	.02	.02	.01	.01	.01	+	0	0
34	.11	.13	.15	.16	.18	.20	.21	.22	.23	.24	.24	.24	.23	.22	.21	.20	.18	.16	.15	.13	.11	.10	.08	.07	.05	.04	.03	.02	0	0
35	.32	.36	.41	.46	.51	.55	.59	.62	.64	.66	.66	.66	.64	.62	.59	.55	.51	.46	.41	.36	.32	.27	.23	.19	.15	.12	.10	.08	0	0
36	.69	.79	.90	1.0	1.1	1.2	1.2	1.3	1.4	1.4	1.4	1.4	1.4	1.3	1.2	1.2	1.1	1.0	.90	.79	.69	.59	.50	.41	.34	.27	.22	.17	0	0
37	1.1	1.3	1.5	1.7	1.9	2.0	2.2	2.3	2.4	2.4	2.4	2.4	2.4	2.3	2.2	2.0	1.9	1.7	1.5	1.3	1.1	1.0	.86	.71	.59	.47	.38	.29	0	0
38	1.6	1.8	2.1	2.3	2.5	2.8	2.9	3.1	3.2	3.3	3.3	3.3	3.2	3.1	2.9	2.8	2.5	2.3	2.1	1.8	1.6	1.3	1.1	.97	.80	.64	.51	.40	0	0
39	1.7	1.9	2.2	2.5	2.7	3.0	3.2	3.3	3.5	3.5	3.6	3.5	3.5	3.3	3.2	3.0	2.7	2.5	2.2	1.9	1.7	1.4	1.2	1.0	.86	.69	.55	.43	0	0
40	1.4	1.6	1.9	2.1	2.3	2.5	2.7	2.8	2.9	3.0	3.0	3.0	2.9	2.8	2.7	2.5	2.3	2.1	1.9	1.6	1.4	1.2	1.0	.89	.73	.59	.47	.37	0	0
41	.99	1.1	1.2	1.4	1.5	1.7	1.8	1.9	2.0	2.0	2.0	2.0	2.0	1.9	1.8	1.7	1.5	1.4	1.2	1.1	.99	.85	.72	.59	.49	.39	.31	.24	0	0
42	.52	.60	.68	.76	.84	.91	.97	1.0	1.0	1.0	1.0	1.0	1.0	1.0	.97	.91	.84	.76	.68	.60	.52	.45	.38	.31	.26	.21	.16	.13	0	0
43	.22	.25	.28	.32	.35	.38	.41	.43	.44	.45	.46	.45	.44	.43	.41	.38	.35	.32	.28	.25	.22	.19	.16	.13	.11	.08	.07	.05	0	0
44	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0

CONCENTRATIONS ABOVE BACKGROUND OF FLUID (VOLUMETRIC RATIO OF DUMP FLUID TO AMBIENT WATER) IN THE CLOUD 3600.00 SECONDS AFTER DUMP

THESE CONCENTRATIONS ARE THE MAXIMUM OCCURING IN THE WATER COLUMN AT THIS TIME

...MULTIPLY DISPLAYED VALUES BY 0.1000E-03 (LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)

M N=	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
18	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
19	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
20	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
21	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
22	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
23	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
24	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
25	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
26	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
27	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
28	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
29	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
30	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
31	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+
32	+	+	+	+	+	+	+	.01	.01	.01	.01	.01	.01	.01	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+
33	.02	.02	.03	.03	.03	.04	.04	.04	.04	.04	.04	.04	.04	.04	.04	.04	.03	.03	.03	.02	.02	.02	.01	.01	.01	+	+	+	+	+
34	.08	.09	.10	.11	.12	.14	.14	.15	.16	.16	.16	.16	.16	.15	.14	.14	.12	.11	.10	.09	.08	.06	.05	.04	.04	.03	.02	.02	0	0
35	.22	.25	.28	.32	.35	.38	.41	.43	.44	.45	.46	.45	.44	.43	.41	.38	.35	.32	.28	.25	.22	.19	.16	.13	.10	.08	.07	.05	0	0
36	.48	.55	.62	.69	.76	.83	.88	.93	.97	.99	.99	.99	.97	.93	.88	.83	.76	.69	.62	.55	.48	.41	.34	.29	.23	.19	.15	.12	0	0
37	.82	.94	1.0	1.1	1.3	1.4	1.5	1.6	1.6	1.7	1.7	1.7	1.6	1.6	1.5	1.4	1.3	1.1	1.0	.94	.82	.70	.59	.49	.40	.33	.26	.20	0	0
38	1.1	1.2	1.4	1.6	1.7	1.9	2.0	2.1	2.2	2.3	2.3	2.3	2.2	2.1	2.0	1.9	1.7	1.6	1.4	1.2	1.1	.96	.81	.67	.55	.44	.35	.28	0	0
39	1.2	1.3	1.5	1.7	1.9	2.0	2.2	2.3	2.4	2.4	2.4	2.4	2.4	2.3	2.2	2.0	1.9	1.7	1.5	1.3	1.2	1.0	.87	.72	.59	.48	.38	.30	0	0
40	1.0	1.1	1.3	1.4	1.6	1.7	1.8	1.9	2.0	2.1	2.1	2.1	2.0	1.9	1.8	1.7	1.6	1.4	1.3	1.1	1.0	.87	.74	.61	.50	.40	.32	.25	0	0
41	.68	.79	.89	.99	1.0	1.1	1.2	1.3	1.3	1.4	1.4	1.4	1.3	1.3	1.2	1.1	1.0	.99	.89	.79	.68	.58	.49	.41	.34	.27	.21	.17	0	0
42	.36	.42	.47	.53	.58	.63	.67	.71	.73	.75	.76	.75	.73	.71	.67	.63	.58	.53	.47	.42	.36	.31	.26	.22	.18	.14	.11	.09	0	0
43	.15	.17	.20	.22	.24	.26	.28	.29	.31	.31	.32	.31	.31	.29	.28	.26	.24	.22	.20	.17	.15	.13	.11	.09	.07	.06	.04	.03	0	0
44	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0

CONCENTRATIONS ABOVE BACKGROUND OF FLUID   (VOLUMETRIC RATIO OF DUMP FLUID TO AMBIENT WATER) IN THE CLOUD   3600.00 SECONDS AFTER DUMP

THESE CONCENTRATIONS ARE THE MAXIMUM THAT EVER OCCURRED IN THE WATER COLUMN DURING THE SIMULATION

```
...MULTIPLY DISPLAYED VALUES BY  0.1000E-02     (LEGEND... + = .LT. .01   . = .LT. .0001   0 = .LT. .000001)
M N=  2   3   4   5   6   7   8   9  10  11  12  13  14  15  16  17  18  19  20  21  22  23  24  25  26  27  28  29  30  31
 2 0000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000
 3 0000   0   0   .   .   .   .   .   .   .   .   .   .   .   .   .   .   .   .   .   0   0   0   0   0   0   0   0   00000
 4 0000   .   .   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   0   0   0   0   0   0   0   0   00000
 5 0000   +   +   +   + .01 .01 .02 .03 .03 .04 .04 .04 .03 .03 .02 .01 .01   +   +   0   0   0   0   0   0   0   0   00000
 6 0000 .02 .03 .06 .11 .17 .25 .33 .42 .50 .55 .57 .55 .50 .42 .33 .25 .17 .11 .06   .   0   0   0   0   0   0   0   00000
 7 0000 .10 .18 .33 .54 .83 1.2 1.6 2.0 2.4 2.6 2.7 2.6 2.4 2.0 1.6 1.2 .83 .54 .33   +   0   0   0   0   0   0   0   00000
 8 0000 .16 .31 .54 .90 1.3 1.9 2.6 3.3 3.9 4.4 4.5 4.4 3.9 3.3 2.6 1.9 1.3 .90 .54   +   0   0   0   0   0   0   0   00000
 9 0000 .09 .18 .31 .51 .79 1.1 1.5 1.9 2.2 2.5 2.6 2.5 2.2 1.9 1.5 1.1 .79 .51 .31 .05   .   0   0   0   0   0   0   00000
10 0000 .09 .16 .25 .39 .56 .76 .97 1.1 1.3 1.4 1.5 1.4 1.3 1.1 .97 .76 .56 .39 .25 .16   +   0   0   0   0   0   0   00000
11 0000 .12 .20 .33 .50 .71 .97 1.2 1.5 1.7 1.9 1.9 1.9 1.7 1.5 1.2 .97 .71 .50 .33 .20   +   0   0   0   0   0   0   00000
12 0000 .06 .10 .17 .26 .37 .51 .66 .80 .92 1.0 1.0 1.0 .92 .80 .66 .51 .37 .26 .17 .10 .04   0   0   0   0   0   0   00000
13 0000 .09 .14 .22 .31 .43 .55 .69 .81 .91 .98 1.0 .98 .91 .81 .69 .55 .43 .31 .22 .14 .09   .   0   0   0   0   0   00000
14 0000 .10 .15 .23 .33 .45 .59 .73 .86 .97 1.0 1.0 1.0 .97 .86 .73 .59 .45 .33 .23 .15 .10   .   0   0   0   0   0   00000
15 0000 .05 .07 .11 .16 .22 .29 .36 .43 .48 .52 .53 .52 .48 .43 .36 .29 .22 .16 .11 .07 .05   +   0   0   0   0   0   00000
16 0000 .09 .13 .19 .26 .34 .42 .51 .59 .65 .69 .70 .69 .65 .59 .51 .42 .34 .26 .19 .13 .09   +   .   0   0   0   0   00000
17 0000 .08 .12 .18 .24 .31 .39 .47 .54 .60 .64 .65 .64 .60 .54 .47 .39 .31 .24 .18 .12 .08 .01   +   0   0   0   0   00000
18 0000 .07 .09 .13 .17 .21 .26 .30 .34 .37 .39 .40 .39 .37 .34 .30 .26 .21 .17 .13 .09 .07 .04   +   .   0   0   0   00000
19 0000 .10 .14 .19 .25 .31 .38 .44 .50 .55 .58 .59 .58 .55 .50 .44 .38 .31 .25 .19 .14 .10 .07   +   .   0   0   0   00000
20 0000 .08 .12 .16 .21 .26 .32 .37 .42 .46 .48 .49 .48 .46 .42 .37 .32 .26 .21 .16 .12 .08 .06 .02   +   0   0   0   00000
21 0000 .09 .12 .15 .19 .23 .28 .32 .35 .38 .40 .41 .40 .38 .35 .32 .28 .23 .19 .15 .12 .09 .06 .04   +   .   0   0   00000
22 0000 .11 .15 .19 .24 .30 .35 .40 .45 .48 .51 .52 .51 .48 .45 .40 .35 .30 .24 .19 .15 .11 .08 .05   +   +   0   0   00000
23 0000 .08 .11 .15 .19 .23 .27 .31 .35 .38 .40 .40 .40 .38 .35 .31 .27 .23 .19 .15 .11 .08 .06 .04 .02   +   0   0   00000
24 0000 .10 .13 .17 .20 .24 .28 .32 .35 .37 .39 .39 .39 .37 .35 .32 .28 .24 .20 .17 .13 .10 .08 .05 .04   +   0   0   00000
25 0000 .11 .15 .19 .23 .27 .32 .36 .40 .42 .44 .45 .44 .42 .40 .36 .32 .27 .23 .19 .15 .11 .09 .06 .04 .01   0   0   00000
26 0000 .08 .11 .14 .17 .20 .23 .27 .29 .31 .32 .33 .32 .31 .29 .27 .23 .20 .17 .14 .11 .08 .06 .04 .03 .02   .   0   00000
27 0000 .11 .14 .17 .21 .24 .27 .31 .33 .35 .37 .37 .37 .35 .33 .31 .27 .24 .21 .17 .14 .11 .09 .06 .05 .03   +   0   00000
28 0000 .12 .15 .18 .21 .25 .28 .32 .34 .37 .38 .38 .38 .37 .34 .32 .28 .25 .21 .18 .15 .12 .09 .07 .05 .03   +   0   00000
29 0000 .09 .11 .13 .15 .18 .20 .22 .24 .26 .27 .27 .27 .26 .24 .22 .20 .18 .15 .13 .11 .09 .07 .05 .04 .03   +   .   00000
30 0000 .12 .14 .17 .20 .23 .26 .29 .31 .33 .34 .34 .34 .33 .31 .29 .26 .23 .20 .17 .14 .12 .09 .07 .06 .04   +   +   00000
31 0000 .11 .14 .17 .20 .22 .25 .28 .30 .31 .32 .33 .32 .31 .30 .28 .25 .22 .20 .17 .14 .11 .09 .07 .05 .04 .01   +   .0000
32 0000 .10 .12 .14 .16 .18 .20 .21 .23 .24 .25 .25 .25 .24 .23 .21 .20 .18 .16 .14 .12 .10 .08 .06 .05 .04 .03   +   +0000
33 0000 .12 .14 .17 .19 .22 .24 .26 .28 .30 .30 .31 .30 .30 .28 .26 .24 .22 .19 .17 .14 .12 .10 .08 .06 .05 .03 .01   +0000
34 0000 .11 .13 .15 .18 .20 .22 .24 .26 .27 .28 .28 .28 .27 .26 .24 .22 .20 .18 .15 .13 .11 .09 .07 .06 .04 .03 .02   +0000
35 0000 .10 .12 .14 .16 .18 .20 .21 .22 .23 .24 .24 .24 .23 .22 .21 .20 .18 .16 .14 .12 .10 .09 .07 .06 .04 .03 .03   +0000
36 0000 .12 .14 .16 .18 .20 .22 .24 .26 .27 .27 .28 .27 .27 .26 .24 .22 .20 .18 .16 .14 .12 .10 .08 .07 .05 .04 .03 .010000
37 0000 .10 .12 .14 .16 .18 .20 .21 .22 .23 .24 .24 .24 .23 .22 .21 .20 .18 .16 .14 .12 .10 .09 .07 .06 .04 .03 .03 .020000
38 0000 .11 .12 .14 .16 .17 .19 .20 .21 .22 .23 .23 .23 .22 .21 .20 .19 .17 .16 .14 .12 .11 .09 .08 .06 .05 .04 .03 .020000
39 0000 .12 .13 .15 .17 .19 .20 .22 .23 .24 .24 .24 .24 .24 .23 .22 .20 .19 .17 .15 .13 .12 .10 .08 .07 .05 .04 .03 .030000
40 0000 .10 .11 .13 .14 .16 .17 .18 .19 .20 .21 .21 .21 .20 .19 .18 .17 .16 .14 .13 .11 .10 .08 .07 .06 .05 .04 .03 .020000
41 0000 .06 .07 .08 .09 .10 .11 .12 .13 .13 .14 .14 .14 .13 .13 .12 .11 .10 .09 .08 .07 .06 .05 .04 .04 .03 .02 .02 .010000
42 0000 .03 .04 .04 .05 .05 .06 .06 .07 .07 .07 .07 .07 .07 .07 .06 .06 .05 .05 .04 .04 .03 .03 .02 .02 .01 .01 .01   +0000
43 0000 .01 .01 .02 .02 .02 .02 .02 .02 .03 .03 .03 .03 .03 .02 .02 .02 .02 .02 .02 .01 .01 .01 .01   +   +   +   +   +0000
44 0000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000
```

SMALL CLOUDS AT 3600.00 SECONDS ELAPSED TIME FOR FLUID

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID	LOCATION OF CLOUD CENTROID DISTANCE FROM LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	3781.	300.0	5067.	0.0000E+00	732.7	0.0000E+00	120.0	0.000000E+00

FINAL DISTRIBUTIONS OF TOTAL SETTLED MATERIAL FOLLOW.....

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TOTAL ACCUMULATED SOLID VOLUME ON BOTTOM (CU FT/GRID SQR),    3600.00 SECONDS AFTER DUMP
...MULTIPLY DISPLAYED VALUES BY   1.000         (LEGEND... + = .LT. .01   . = .LT. .0001   0 = .LT. .000001)
M N=  2   3   4   5   6   7   8   9  10  11  12  13  14  15  16  17  18  19  20  21  22  23  24  25  26  27  28  29  30  31
 2 000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000
 3 0000   .   .   .   .   .   .   +   +   +   +   +   +   +   +   +   .   .   .   .   .   .   .   .   0   0   0   0   00000
 4 0000   +   +   +   +   + .01 .01 .01 .02 .02 .02 .02 .02 .01 .01 .01   +   +   +   +   +   +   +   .   .   .   .   .0000
 5 0000 .03 .06 .11 .19 .29 .42 .57 .72 .85 .94 .98 .94 .85 .72 .57 .42 .29 .19 .11 .06 .03 .01   +   +   +   +   +   .0000
 6 0000 .49 .92 1.6 2.6 4.0 5.8 7.9  10  12  17  25  17  12  10 7.9 5.8 4.0 2.6 1.6 .92 .49 .24 .11 .05 .02   +   +   +0000
 7 0000 2.3 4.4 7.7  13  20  28  38  48  57  63  65  63  57  48  38  28  20  13 7.7 4.4 2.3 1.1 .55 .24 .09 .03 .01   +0000
 8 0000 4.0 7.5  13  22  33  48  64  82  97 108 113 108  97  82  64  48  33  22  13 7.5 4.0 2.0 .94 .41 .17 .06 .02   +0000
 9 0000 3.2 5.8  10  16  24  35  46  58  68  75  77  75  68  58  46  35  24  16  10 5.8 3.2 1.6 .81 .37 .16 .06 .02   +0000
10 0000 3.5 6.0  10  15  22  30  39  48  56  61  63  61  56  48  39  30  22  15  10 6.0 3.5 1.9 1.0 .50 .23 .10 .04 .010000
11 0000 4.2 7.2  12  18  25  34  44  54  62  69  73  69  62  54  44  34  25  18  12 7.2 4.2 2.4 1.2 .64 .30 .13 .06 .020000
12 0000 3.7 6.0 9.4  14  20  26  33  40  46  50  51  50  46  40  33  26  20  14 9.4 6.0 3.7 2.1 1.1 .62 .31 .14 .06 .020000
13 0000 4.1 6.5  10  14  20  25  32  38  43  46  47  46  43  38  32  25  20  14  10 6.5 4.1 2.5 1.4 .79 .41 .20 .09 .040000
14 0000 4.1 6.4  10  14  19  24  30  35  40  44  45  44  40  35  30  24  19  14  10 6.4 4.1 2.5 1.4 .80 .42 .21 .10 .040000
15 0000 2.3 3.6 5.4 7.7  10  13  17  19  22  23  24  23  22  19  17  13  10 7.7 5.4 3.6 2.3 1.4 .86 .48 .26 .13 .06 .030000
16 0000 1.1 1.7 2.5 3.5 4.7 6.0 7.3 8.6  10  11  11  11  10 8.6 7.3 6.0 4.7 3.5 2.5 1.7 1.1 .75 .46 .26 .15 .08 .04 .020000
17 0000 .72 1.0 1.5 2.0 2.6 3.3 4.0 4.7 5.3 5.8 6.0 5.8 5.3 4.7 4.0 3.3 2.6 2.0 1.5 1.0 .72 .47 .29 .17 .10 .05 .02 .010000
18 0000 .32 .48 .68 .92 1.2 1.5 1.8 2.0 2.3 2.4 2.5 2.4 2.3 2.0 1.8 1.5 1.2 .92 .68 .48 .32 .21 .13 .08 .04 .02 .01   +0000
19 0000 .08 .12 .17 .23 .30 .38 .49 .63 .85 1.0 1.1 1.0 .85 .63 .49 .38 .30 .23 .17 .12 .08 .05 .03 .02 .01   +   +   +0000
20 0000 .01 .01 .02 .03 .04 .05 .06 .09 .12 .16 .18 .16 .12 .09 .06 .05 .04 .03 .02 .01 .01   +   +   +   +   +   +   +0000
21 0000   +   +   +   +   +   +   + .01 .02 .03 .04 .03 .02 .01   +   +   +   +   +   +   +   +   +   +   +   .   .   .0000
22 0000   .   +   +   +   + .01 .03 .08 .17 .26 .30 .26 .17 .08 .03 .01   +   +   +   +   .   .   .   .   .   .   .   .0000
23 0000   .   .   +   +   +   +   + .01 .02 .03 .03 .03 .02 .01   +   +   +   +   +   .   .   .   .   .   .   .   .   00000
24 0000   .   .   +   +   +   + .01 .02 .03 .04 .05 .04 .03 .02 .01   +   +   +   +   .   .   .   .   .   .   .   .   .0000
25 0000   .   +   +   +   + .01 .02 .05 .09 .12 .14 .12 .09 .05 .02 .01   +   +   +   +   .   .   .   .   .   .   .   .0000
26 0000   .   .   +   +   +   +   +   + .01 .01 .01 .01 .01   +   +   +   +   +   +   .   .   .   .   .   .   .   .   .0000
27 0000   .   +   +   +   +   + .01 .02 .03 .04 .04 .04 .03 .02 .01   +   +   +   +   +   .   .   .   .   .   .   .   .0000
28 0000   .   +   +   +   +   + .01 .02 .04 .05 .06 .05 .04 .02 .01   +   +   +   +   +   .   .   .   .   .   .   .   .0000
29 0000   .   +   +   +   +   +   +   +   + .01 .01 .01   +   +   +   +   +   +   +   +   .   .   .   .   .   .   .   .0000
30 0000   +   +   +   +   +   + .01 .01 .02 .03 .03 .03 .02 .01 .01   +   +   +   +   +   +   .   .   .   .   .   .   .0000
31 0000   +   +   +   +   +   +   + .01 .02 .02 .02 .02 .02 .01   +   +   +   +   +   +   +   .   .   .   .   .   .   .0000
32 0000   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   .   .   .   .   .   .   .0000
33 0000   +   +   +   +   +   +   + .01 .01 .01 .01 .01 .01 .01   +   +   +   +   +   +   +   +   .   .   .   .   .   .0000
34 0000   +   +   +   +   +   +   +   +   + .01 .01 .01   +   +   +   +   +   +   +   +   +   +   .   .   .   .   .   .0000
35 0000   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   .   .   .   .   .   .0000
36 0000   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   .   .   .   .   .   .0000
37 0000   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   .   .   .   .   .   .0000
38 0000   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   .   .   .   .   .   .0000
39 0000   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   .   .   .   .   .   .0000
40 0000   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   .   .   .   .   .   .   .0000
41 0000   .   .   .   +   +   +   +   +   +   +   +   +   +   +   +   +   +   +   .   .   .   .   .   .   .   .   .   .0000
42 0000   .   .   .   .   .   .   .   .   .   .   .   .   .   .   .   .   .   .   .   .   .   .   .   .   .   .   .   .0000
43 0000   .   .   .   .   .   .   .   .   .   .   .   .   .   .   .   .   .   .   .   .   .   .   .   .   .   0   0   00000
44 000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000
```

TOTAL THICKNESS (FT) OF NEW MATERIAL ON BOTTOM,   3600.00 SECONDS AFTER DUMP
...MULTIPLY DISPLAYED VALUES BY   1.000   (LEGEND... + = .LT. .01   . = .LT. .0001   0 = .LT. .000001)

M N=	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31
2	000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000																													
3	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		00000
4	0000	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0	0		00000
5	0000	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	0		00000
6	0000	+	+	+	+	.01	.01	.01	.02	.02	.04	.06	.04	.02	.02	.01	.01	.01	+	+	+	+	+	+	+	.	.	.		.0000
7	0000	+	.01	.01	.03	.04	.06	.09	.11	.13	.15	.15	.15	.13	.11	.09	.06	.04	.03	.01	.01	+	+	+	+	+	.	.		.0000
8	0000	+	.01	.03	.05	.08	.11	.15	.20	.23	.26	.27	.26	.23	.20	.15	.11	.08	.05	.03	.01	+	+	+	+	+	+	.		.0000
9	0000	+	.01	.02	.03	.06	.08	.11	.14	.16	.18	.19	.18	.16	.14	.11	.08	.06	.03	.02	.01	+	+	+	+	+	+	.		.0000
10	0000	+	.01	.02	.03	.05	.07	.09	.11	.13	.14	.15	.14	.13	.11	.09	.07	.05	.03	.02	.01	+	+	+	+	+	+	+		.0000
11	0000	.01	.01	.02	.04	.06	.08	.10	.13	.15	.17	.17	.17	.15	.13	.10	.08	.06	.04	.02	.01	.01	+	+	+	+	+	+		.0000
12	0000	+	.01	.02	.03	.04	.06	.08	.09	.11	.12	.12	.12	.11	.09	.08	.06	.04	.03	.02	.01	+	+	+	+	+	+	+		.0000
13	0000	.01	.01	.02	.03	.04	.06	.07	.09	.10	.11	.11	.11	.10	.09	.07	.06	.04	.03	.02	.01	.01	+	+	+	+	+	+		+0000
14	0000	.01	.01	.02	.03	.04	.05	.07	.08	.09	.10	.11	.10	.09	.08	.07	.05	.04	.03	.02	.01	.01	+	+	+	+	+	+		+0000
15	0000	+	+	.01	.01	.02	.03	.04	.04	.05	.05	.05	.05	.05	.04	.04	.03	.02	.01	.01	+	+	+	+	+	+	+	+		.0000
16	0000	+	+	+	+	.01	.01	.01	.02	.02	.02	.02	.02	.02	.02	.01	.01	.01	+	+	+	+	+	+	+	+	+	+		.0000
17	0000	+	+	+	+	+	+	.01	.01	.01	.01	.01	.01	.01	.01	.01	+	+	+	+	+	+	+	+	+	+	+	.		.0000
18	0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.		.0000
19	0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.		.0000
20	0000	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.		00000
21	0000	.	.	.	.	.	.	.	.	.	.	+	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0	0		00000
22	0000	0	0	0	.	.	.	.	+	+	+	+	+	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0		00000
23	0000	0	0	0	0	.	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0	0	0	0	0	0	0		00000
24	0000	0	0	0	.	.	.	.	.	.	+	+	+	.	.	.	.	.	.	0	0	0	0	0	0	0	0	0		00000
25	0000	0	0	0	.	.	.	.	+	+	+	+	+	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0		00000
26	0000	0	0	0	0	.	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0	0	0	0	0	0	0		00000
27	0000	0	0	.	.	.	.	.	.	.	+	+	+	.	.	.	.	.	.	.	0	0	0	0	0	0	0	0		00000
28	0000	0	0	.	.	.	.	.	.	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0	0	0	0	0		00000
29	0000	0	0	0	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0	0	0	0	0	0		00000
30	0000	0	0	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0	0	0	0	0		00000
31	0000	0	0	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0	0	0	0	0		00000
32	0000	0	0	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0	0	0	0	0		00000
33	0000	0	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0	0	0	0		00000
34	0000	0	0	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0	0	0	0	0		00000
35	0000	0	0	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0	0	0	0	0		00000
36	0000	0	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0	0	0	0		00000
37	0000	0	0	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0	0	0	0	0		00000
38	0000	0	0	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0	0	0	0	0		00000
39	0000	0	0	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0	0	0	0	0		00000
40	0000	0	0	0	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0	0	0	0	0	0		00000
41	0000	0	0	0	0	0	0	0	0	0	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		00000
42	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		00000
43	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		00000
44	000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000000																													

INITIAL MIXING COMPUTATIONS RESULTS FOR GRAVEL :

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND ON ENTIRE GRID (MG/L)	X-LOC (FT)	Z-LOC (FT)	MAX CONC ABOVE BACKGROUND OUTSIDE MIXING ZONE (MG/L)
0.25	60.0	0.000E+00	0.	0.	0.000E+00
0.50	60.0	0.000E+00	0.	0.	0.000E+00
0.75	60.0	0.000E+00	0.	0.	0.000E+00
1.00	60.0	0.000E+00	0.	0.	0.000E+00
0.25	119.0	0.000E+00	0.	0.	0.000E+00
0.50	119.0	0.000E+00	0.	0.	0.000E+00
0.75	119.0	0.000E+00	0.	0.	0.000E+00
1.00	119.0	0.000E+00	0.	0.	0.000E+00

INITIAL MIXING COMPUTATIONS RESULTS FOR SAND :

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND ON ENTIRE GRID (MG/L)	X-LOC (FT)	Z-LOC (FT)	MAX CONC ABOVE BACKGROUND OUTSIDE MIXING ZONE (MG/L)
0.25	60.0	0.181E+02	1300.	300.	0.181E+02
0.50	60.0	0.275E+01	2100.	300.	0.275E+01
0.75	60.0	0.960E-01	2900.	300.	0.960E-01
1.00	60.0	0.236E-02	3800.	300.	0.236E-02
0.25	119.0	0.887E+01	1300.	300.	0.887E+01
0.50	119.0	0.212E+01	2100.	300.	0.212E+01
0.75	119.0	0.210E+00	2900.	300.	0.210E+00
1.00	119.0	0.270E-01	3800.	300.	0.270E-01

INITIAL MIXING COMPUTATIONS RESULTS FOR SILT :

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND ON ENTIRE GRID (MG/L)	X-LOC (FT)	Z-LOC (FT)	MAX CONC ABOVE BACKGROUND OUTSIDE MIXING ZONE (MG/L)
0.25	60.0	0.371E+03	1300.	300.	0.371E+03
0.50	60.0	0.581E+03	2100.	300.	0.581E+03
0.75	60.0	0.257E+03	2900.	300.	0.257E+03
1.00	60.0	0.168E+03	3800.	300.	0.168E+03
0.25	119.0	0.207E+03	1300.	300.	0.207E+03
0.50	119.0	0.865E+02	2100.	300.	0.865E+02
0.75	119.0	0.371E+02	2900.	300.	0.371E+02
1.00	119.0	0.243E+02	3800.	300.	0.243E+02

INITIAL MIXING COMPUTATIONS RESULTS FOR CLAY :

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND ON ENTIRE GRID (MG/L)	X-LOC (FT)	Z-LOC (FT)	MAX CONC ABOVE BACKGROUND OUTSIDE MIXING ZONE (MG/L)
0.25	60.0	0.227E+03	1300.	300.	0.227E+03
0.50	60.0	0.188E+03	2100.	300.	0.188E+03
0.75	60.0	0.860E+02	2900.	300.	0.860E+02
1.00	60.0	0.563E+02	3800.	300.	0.563E+02
0.25	119.0	0.527E+04	1300.	300.	0.527E+04
0.50	119.0	0.265E+04	2100.	300.	0.265E+04
0.75	119.0	0.136E+04	2900.	300.	0.136E+04
1.00	119.0	0.795E+03	3800.	300.	0.795E+03

INITIAL MIXING COMPUTATIONS RESULTS FOR FLUID :

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND ON ENTIRE GRID (PERCENT)	X-LOC (FT)	Z-LOC (FT)	MAX CONC ABOVE BACKGROUND OUTSIDE MIXING ZONE (PERCENT)
0.08	60.0	0.550E-08	700.	300.	0.482E-08
0.17	60.0	0.177E-01	1000.	300.	0.177E-01
0.25	60.0	0.759E-01	1300.	300.	0.759E-01
0.33	60.0	0.701E-01	1500.	300.	0.701E-01
0.42	60.0	0.593E-01	1800.	300.	0.593E-01
0.50	60.0	0.520E-01	2100.	300.	0.520E-01
0.58	60.0	0.451E-01	2400.	300.	0.451E-01
0.67	60.0	0.388E-01	2700.	300.	0.388E-01
0.75	60.0	0.345E-01	2900.	300.	0.345E-01
0.83	60.0	0.312E-01	3200.	300.	0.312E-01
0.92	60.0	0.280E-01	3500.	300.	0.280E-01
1.00	60.0	0.250E-01	3800.	300.	0.250E-01
0.08	119.0	0.799E-01	700.	300.	0.700E-01
0.17	119.0	0.304E-01	1000.	300.	0.304E-01
0.25	119.0	0.160E-01	1300.	300.	0.160E-01
0.33	119.0	0.103E-01	1500.	300.	0.103E-01
0.42	119.0	0.857E-02	1800.	300.	0.857E-02
0.50	119.0	0.752E-02	2100.	300.	0.752E-02
0.58	119.0	0.652E-02	2400.	300.	0.652E-02
0.67	119.0	0.561E-02	2700.	300.	0.561E-02
0.75	119.0	0.498E-02	2900.	300.	0.498E-02
0.83	119.0	0.451E-02	3200.	300.	0.451E-02
0.92	119.0	0.405E-02	3500.	300.	0.405E-02
1.00	119.0	0.361E-02	3800.	300.	0.361E-02
0.08	60.0	0.455E+00	700.	300.	0.399E+00
0.17	60.0	0.196E+00	1000.	300.	0.196E+00
0.25	60.0	0.108E+00	1300.	300.	0.108E+00
0.33	60.0	0.709E-01	1500.	300.	0.709E-01
0.42	60.0	0.593E-01	1800.	300.	0.593E-01
0.50	60.0	0.520E-01	2100.	300.	0.520E-01
0.58	60.0	0.451E-01	2400.	300.	0.451E-01
0.67	60.0	0.388E-01	2700.	300.	0.388E-01
0.75	60.0	0.345E-01	2900.	300.	0.345E-01
0.83	60.0	0.312E-01	3200.	300.	0.312E-01
0.92	60.0	0.280E-01	3500.	300.	0.280E-01
1.00	60.0	0.250E-01	3800.	300.	0.250E-01

RESULT: THE TOXICITY STANDARD FOR THE MIXING ZONE WAS NOT VIOLATED.

*** RUN COMPLETED ***